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MCR-70-457 (Vol I)

# FINAL REPORT

## SPIN VECTOR CONTROL FOR A SPINNING SPACE STATION

### VOLUME I: USER'S MANUAL

By:

T. Hendricks  
W. Guderian  
G. Johnson  
G. Haynes

November 1970

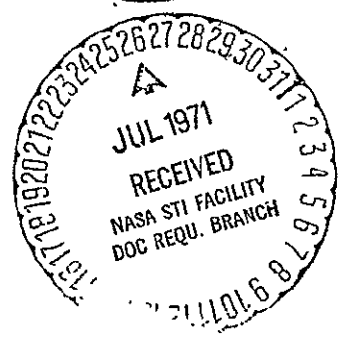
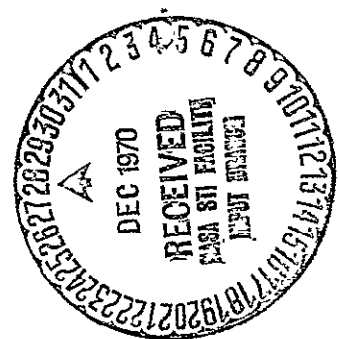
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NATIONAL AERONAUTICS AND SPACE ADMINISTRATION  
George C. Marshall Space Flight Center  
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### FOREWORD

This document represents Volume II of the final report on NASA Huntsville Contract entitled "Spin Vector Control for a Spinning Space Station". The report is prepared in two volumes:

Volume I - User's Manual

Volume II - Analytical Manual

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## FINAL REPORT

### SPIN VECTOR CONTROL OF A ROTATING SPACE STATION

#### VOLUME I: USER'S MANUAL

By: T. Hendricks, Walter Guderian, George Haynes, Gary Johnson

#### SUMMARY

This document presents the formulation, computational logic, input/output options, subroutine description and other pertinent information that should aid the user of the SPIN VECTOR CONTROL COMPUTER PROGRAM (MD246).

#### I. INTRODUCTION

This document is concerned with the design use and implementation of a digital computer program to facilitate the study of the dynamic behaviour and control of dual spin space vehicles. This volume is a companion to Volume II (analytical manual) of the final report under NASA-Huntsville Contract NAS8-25247.

The Spin Vector Control Program (MD246) is a Fortran Program that was written and checked out using the CDC 6400/6500 digital computer. To minimize possible system incompatibilities care has been exercised to assume that only the basic features of the system are used. Thus the program should be

operable on most digital machines with a FORTRAN 4 compiler.

The program is capable of solving the rotational dynamics of dual spin earth orbiting spacecraft. Several control options as well as spacecraft configurations are possible. Among the available control actuators are CMGs, reaction wheels, reaction jets and torque motors. This program is intended for but not restricted to attitude control studies of a rotating space station. The generalized spacecraft configuration along with geometrical definitions is shown in Figure 1. Figure 2 is a specific spacecraft configuration.

The remaining contents of this document discusses in varying degree of detail how to use the program. The first chapter Input Deck Construction describes those cards which are necessary when exercising the various program options. Chapter 2 Data Deck User's Guide presents a complete sequence and format description of all the data input cards. For a description and definition of the input variables refer to Appendix A.

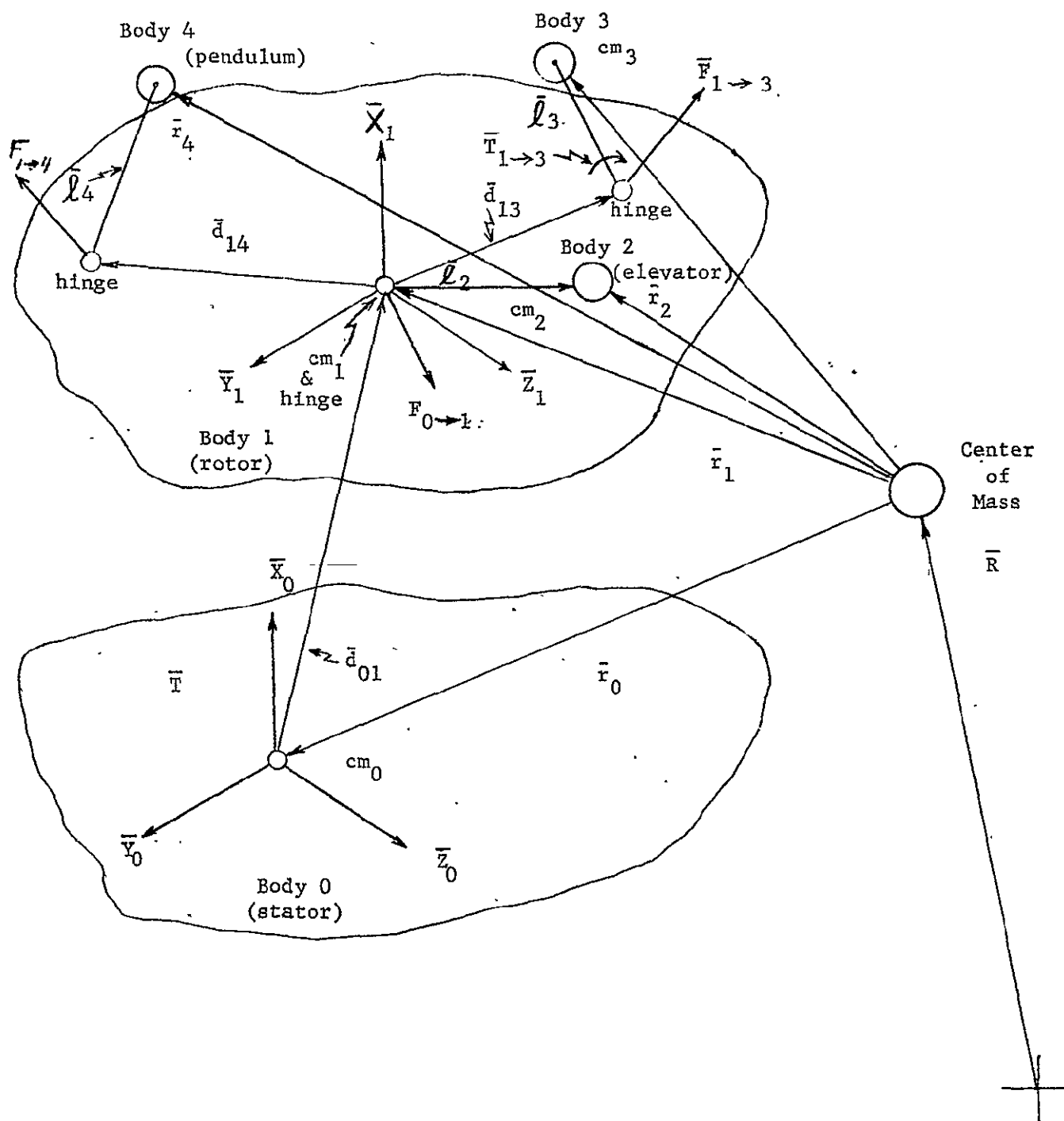


Figure 1 General Body Configuration

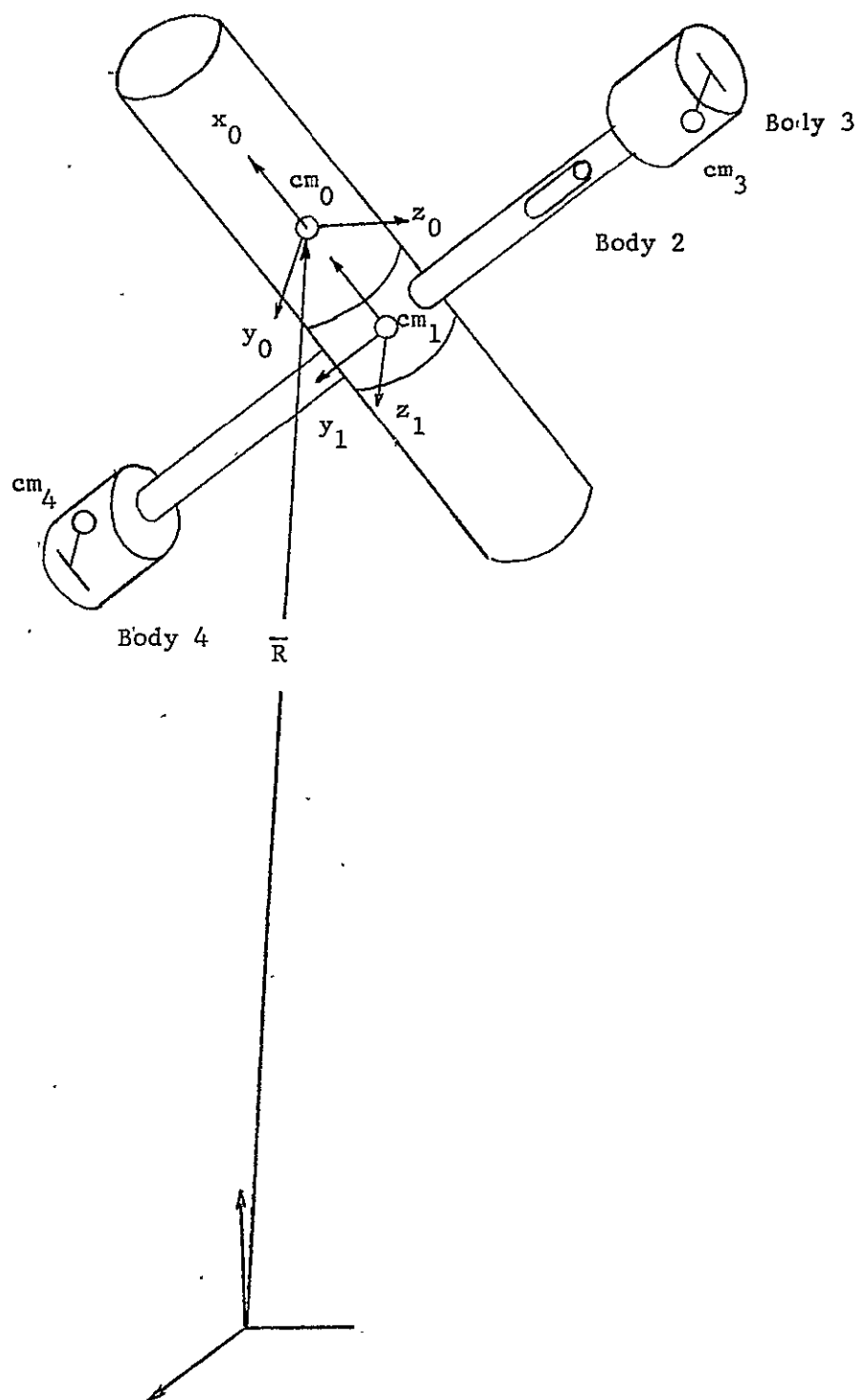


Figure 2 Spacecraft Body Configuration

# INPUT DECK CONSTRUCTION

The basic data deck for operating the program with essentially no designated options is as follows.

Card #	Variable	
1	NDECK = ____	
2	IPNDLM = 0	First card of run data
3	IPRINT = ____	
4	TSTART, TSTOP, DELTAT	
5	Alt.	
6-14	TIBOI(1,1) - TIBOI(3,3)	
15	WO(1), WO(2), WO(3)	
16	BOMASS	
17-25	BODYOI(1,1) - BODYOI(3,3)	
26	NUMCMG = 0	
225	IPROPF = 0 ____	
242	BLMASS	
243-251	BODYII(1,1) - BODYII(3,3)	
252	THETA1	
253	OMEGA1	
254	DO1(1), DO1(2), DO1(3)	
255	IB2F = 0	
282	SP	
283	NGAIN = 0	
294	IGRAVF = 0	
295	IDOCK = 0	

Note that the above is also a list of the cards that must always be present.

Some examples of data deck arrangements for various options will be given. All data decks consist of the basic data deck with changes indicated.

1. Pendulum

Card #2 IPNDLM = 1

Before card #282 add cards #268 through #281, the pendulum parameter and initial value data.

2. Two single DOF CMGs

Card #26 NUMCMG = 2

After card #26 add -

Card #27 IDOF(1) = 1

#28 - HW(1)

#29 - #37 AOCJ(1,1,1) - AOCJ(1,3,3)

#38 - #42 AII(1,1,1) - AII(1,3,3)

#47 - THATA(1)

#48 - THATAD(1)

#60 - IDOF(2) = 1

#61 - HW(2)

#62 - #70 AOCJ(2,1,1) - AOCJ(2,3,3)

#71 - #79 AII(2,1,1) - AII(2,3,3)

#80 - THATA(2)

#81 - THATAD(2)

Card #283 NGAIN = 5

After card #283 add cards #284 - #288

(Cards #287 is control gain for CMG #1 and  
card #288 is control gain for CMG #2 in the  
present subroutines)

3. Propulsion on Body 0 (no attitude control)

Card #225 IPROPF = 1

After card #225 add -

Card #226 IATTIF = 0

Card #230 AOJ(1) = (non-zero) CGAINO(1)

Card #231 AOJ(2) = (non-zero) CGAINO(2)

Card #232 AOJ(3) = (non-zero) CGAINO(3)

After card #259, if present, otherwise after card  
#255 add -

Card #260 ALJ(1) = (non-zero) CGAIN1(1) = 0

Card #261 ALJ(2) = (non-zero) CGAIN(2) = 0

4. Movable Mass

Card #255 IB2F = 1

After card #255 add cards #256 - #259 per-  
taining to movable mass

5. Attitude Control with Propulsion on Body 1

Card #225 IPROPF = 1

After card #225 add -

Card #226 IATT1F = 1

Card #227 CA(1), CA(2), CA(3)

Card #230 AOJ(1) = (non-zero) CGAIN(1) = 0

Card #231 AOJ(2) = (non-zero) CGAIN(2) = 0

Card #232 AOJ(3) = (non-zero) CGAIN(3) = 0

After card #259 if present, otherwise after card

#255 add -

Card #260 ALJ(1) = (non-zero) CGAIN1(1)

Card #261 ALJ(2) = (non-zero) CGAIN1(2)

6. Gravity Gradient

Card #294 IGRAVF = 1

7. Docking

Card #295 IDOCK = 1

After card #295 add cards #296 - #307 docking  
quantities.



# DATA DECK USER'S GUIDE

CARD: 5

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: ALT

FORMAT:  $\frac{+}{-}$  .  $E\frac{+}{-}$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 4

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLES: TSTART TSTOP DELTAT

FORMAT:  $\frac{+}{-}$  .  $\frac{+}{-}$  .  $\frac{+}{-}$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 3

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: IPRINT

FORMAT:

COLUMN: 2 3

CARD: 2

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: IPNDLM

FORMAT:

COLUMN: 3

CARD: 1

INSTRUCTION: THIS CARD GOES IN FRONT OF DATA DECK 1 ONLY.

VARIABLE: NDECK

FORMAT:

COLUMN: 2 1

CARD: 14  
VARIABLE: TIBOI (3,3)

CARD: 13  
VARIABLE: TIBOI (3,2)

CARD: 12  
VARIABLE: TIBOI (3,1)

CARD: 11  
VARIABLE: TIBOI (2,3)

CARD: 10  
VARIABLE: TIBOI (2,2)

CARD: 9  
VARIABLE: TIBOI (2,1)

CARD: 8  
VARIABLE: TIBOI (1,3)

CARD: 7  
VARIABLE: TIBOI (1,2)

CARD: 6  
INSTRUCTION: THE NEXT 9 CARDS MUST ALWAYS BE PRESENT.  
VARIABLE: TIBOI (1,1)  
FORMAT:  $\frac{+}{\cdot}$   
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 16

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: BOMASS

FORMAT:  $\pm$  . E $\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 15

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLES: WO(1)

WO(2)

WO(3)

FORMAT:  $\pm$  .

$\pm$  .

$\pm$  .

2 3 4 5 6 7 8 9 10 11 12

15 16 17 18 19 20 21 22 23 24 25

28 29 30 31 32 33 34 35 36 37 38

CARD: 25  
VARIABLE: BODYOI (3,3)

CARD: 24  
VARIABLE: BODYOI (3,2)

CARD: 23  
VARIABLE: BODYOI (3,1)

CARD: 22  
VARIABLE: BODYOI (2,3)

CARD: 21  
VARIABLE: BODYOI (2,2)

CARD: 20  
VARIABLE: BODYOI (2,1)

CARD: 19  
VARIABLE: BODYOI (1,3)

CARD: 18  
VARIABLE: BODYOI (1,2)

CARD: 17  
INSTRUCTION: THE NEXT 9 CARDS MUST ALWAYS BE PRESENT.  
VARIABLE: BODYOI (1,1)  
FORMAT:  $\pm$  .  $E\pm$   
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 28

INSTRUCTION: IF NUMCMG = 0, IGNORE THIS CARD.

VARIABLE: HW (1)

FORMAT:  $\pm$  . E $\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 27

INSTRUCTION: IF NUMCMG = 0, IGNORE THIS CARD.

VARIABLE: IDOF (1)

FORMAT:

COLUMN: 3

CARD: 26

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: NUMCMG

FORMAT:

COLUMN: 3

CARD: 37  
VARIABLE: AOCJ (1,3,3)

CARD: 36  
VARIABLE: AOCJ (1,3,2)

CARD: 35  
VARIABLE: AOCJ (1,3,1)

CARD: 34  
VARIABLE: AOCJ (1,2,3)

CARD: 33  
VARIABLE: AOCJ (1,2,2)

CARD: 32  
VARIABLE: AOCJ (1,2,1)

CARD: 31  
VARIABLE: AOCJ (1,1,3)

CARD: 30  
VARIABLE: AOCJ (1,1,2)

CARD: 29  
INSTRUCTION: IF NUMCMG = 0, IGNORE THE NEXT 9 CARDS.  
VARIABLE: AOCJ (1,1,1)  
FORMAT:  $\frac{+}{-}$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 46  
VARIABLE: AII (1,3,3)

CARD: 45  
VARIABLE: AII (1,3,2)

CARD: 44  
VARIABLE: AII (1,3,1)

CARD: 43  
VARIABLE: AII (1,2,3)

CARD: 42  
VARIABLE: AII (1,2,2)

CARD: 41  
VARIABLE: AII (1,2,1)

CARD: 40  
VARIABLE: AII (1,1,3)

CARD: 39  
VARIABLE: AII (1,1,2)

CARD: 38  
INSTRUCTION: IF NUMCMG OR IDOF (1) = 0, IGNORE THE NEXT 9 CARDS.  
VARIABLE: AII (1,1,1)  
FORMAT:  $\pm$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 48  
VARIABLE: THATAD (1)  
FORMAT:  $\pm$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 47  
INSTRUCTION: IF NUMCMG OR IDOF (1) = 0, IGNORE THE NEXT 2 CARDS.  
VARIABLE: THATA (1)  
FORMAT:  $\pm$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12



CARD: 57  
VARIABLE: AIO (1,3,3)

CARD: 56  
VARIABLE: AIO (1,3,2)

CARD: 55  
VARIABLE: AIO (1,3,1)

CARD: 54  
VARIABLE: AIO (1,2,3)

CARD: 53  
VARIABLE: AIO (1,2,2)

CARD: 52  
VARIABLE: AIO (1,2,1)

CARD: 51  
VARIABLE: AIO (1,1,3)

CARD: 50  
VARIABLE: AIO (1,1,2)

CARD: 49  
INSTRUCTION: IF NUMCMG = 0, OR IDOF (1) = 0, OR IDOF (1) = 1,  
                  IGNORE THE NEXT 9 CARDS.  
VARIABLE: AIO (1,1,1)  
FORMAT:    +       .  
COLUMN:    2,3,4,5,6,7,8,9,10,11,12,

CARD: 61

INSTRUCTION: IF NUMCMG < 2, IGNORE THIS CARD.

VARIABLE: HW (2)

FORMAT:  $\frac{+}{-}$  . E $\frac{+}{-}$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 60

INSTRUCTION: IF NUMCMG < 2, IGNORE THIS CARD.

VARIABLE: IDOF (2)

FORMAT:

COLUMN: 3

CARD: 59

VARIABLE: FEED (-1)

FORMAT:  $\frac{+}{-}$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 58

INSTRUCTION: IF NUMCMG = 0, OR IDOF (1) = 0, OR IDOF (1) = 1,  
IGNORE THE NEXT 2 CARDS.

VARIABLE: FEE (1)

FORMAT:  $\frac{+}{-}$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 70  
VARIABLE: AOCJ (2,3,3)

CARD: 69  
VARIABLE: AOCJ (2,3,2)

CARD: 68  
VARIABLE: AOCJ (2,3,1)

CARD: 67  
VARIABLE: AOCJ (2,2,3)

CARD: 66  
VARIABLE: AOCJ (2,2,2)

CARD: 65  
VARIABLE: AOCJ (2,2,1)

CARD: 64  
VARIABLE: AOCJ (2,1,3)

CARD: 63  
VARIABLE: AOCJ (2,1,2)

CARD: 62  
INSTRUCTION: IF NUMCMG < 2, IGNORE THE NEXT 9 CARDS.  
VARIABLE: AOCJ (2,1,1)  
FORMAT:  $\frac{+}{-}$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 79  
VARIABLE: AII (2,3,3)

CARD: 78  
VARIABLE: AII (2,3,2)

CARD: 77  
VARIABLE: AII (2,3,1)

CARD: 76  
VARIABLE: AII (2,2,3)

CARD: 75  
VARIABLE: AII (2,2,2)

CARD: 74  
VARIABLE: AII (2,2,1)

CARD: 73  
VARIABLE: AII (2,1,3)

CARD: 72  
VARIABLE: AII (2,1,2)

CARD: 71  
INSTRUCTION: IF NUMCMG < 2, OR IDOF (2) = 0,  
                  IGNORE THE NEXT 9 CARDS.  
VARIABLE: AII (2,1,1)  
FORMAT:   +       .  
COLUMN:    1 2 4 5 6 7 8 9 10 11 12

CARD: 81

INSTRUCTION: IF NUMCMG < 2, OR IDOF (2) = 0, IGNORE THIS CARD.

VARIABLE: THATAD (2)

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 80

INSTRUCTION: IF NUMCMG < 2, OR IDOF (2) = 0, IGNORE THIS CARD.

VARIABLE: THATA (2)

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 90  
VARIABLE: AIO (2,3,3)

CARD: 89  
VARIABLE: AIO (2,3,2)

CARD: 88  
VARIABLE: AIO (2,3,1)

CARD: 87  
VARIABLE: AIO (2,2,3)

CARD: 86  
VARIABLE: AIO (2,2,2)

CARD: 85  
VARIABLE: AIO (2,2,1)

CARD: 84  
VARIABLE: AIO (2,1,3)

CARD: 83  
VARIABLE: AIO (2,1,2)

CARD: 82  
INSTRUCTION: IF NUMCMG < 2, OR IDOF (2) = 0, OR IDOF (2) = 1,  
IGNORE THE NEXT 9 CARDS.  
VARIABLE: AIO (2,1,1)  
FORMAT:  $\pm$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 94  
INSTRUCTION: IF NUMCMG < 3, IGNORE THIS CARD.  
VARIABLE: HW (3)  
FORMAT:  $\frac{+}{-}$  . E+  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 93  
INSTRUCTION: IF NUMCMG < 3, IGNORE THIS CARD.  
VARIABLE: IDOF (3)  
FORMAT:  
COLUMN: 3

CARD: 92  
VARIABLE: FEED (2)

CARD: 91  
INSTRUCTION: IF NUMCMG < 2, OR IDOF (2) = 0, OR IDOF (2) = 1,  
IGNORE THE NEXT 2 CARDS.  
VARIABLE: FEE (2)  
FORMAT:  $\frac{+}{-}$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12,

CARD: 103  
VARIABLE: AOCJ (3,3,3)

CARD: 102  
VARIABLE: AOCJ (3,3,2)

CARD: 101  
VARIABLE: AOCJ (3,3,1)

CARD: 100  
VARIABLE: AOCJ (3,2,3)

CARD: 99  
VARIABLE: AOCJ (3,2,2)

CARD: 98  
VARIABLE: AOCJ (3,2,1)

CARD: 97  
VARIABLE: AOCJ (3,1,3)

CARD: 96  
VARIABLE: AOCJ (3,1,2)

CARD: 95  
INSTRUCTION: IF NUMCMG < 3, IGNORE THE NEXT 9 CARDS.  
VARIABLE: AOCJ (3,1,1)  
FORMAT:  $\frac{+}{-}$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12



CARD: 112  
VARIABLE: AII (3,3,3)

CARD: 111  
VARIABLE: AII (3,3,2)

CARD: 110  
VARIABLE: AII (3,3,1)

CARD: 109  
VARIABLE: AII (3,2,3)

CARD: 108  
VARIABLE: AII (3,2,2)

CARD: 107  
VARIABLE: AII (3,2,1)

CARD: 106  
VARIABLE: AII (3,1,3)

CARD: 105  
VARIABLE: AII (3,1,2)

CARD: 104  
INSTRUCTION: IF NUMCMG < 3, OR IDOF (3) = 0,  
                  IGNORE THE NEXT 9 CARDS.  
VARIABLE: AII (3,1,1)  
FORMAT:    +       .  
COLUMN:    2 3 4 5 6 7 8 9 10 11 12

CARD: 114

INSTRUCTION: IF NUMCMG  $< 3$ , OR IDOF (3) = 0, IGNORE THIS CARD.

VARIABLE: THATAD (3)

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 113

INSTRUCTION: IF NUMCMG  $< 3$ , OR IDOF (3) = 0, IGNORE THIS CARD.

VARIABLE: THATA (3)

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 123  
VARIABLE: AIO (3,3,3)

CARD: 122  
VARIABLE: AIO (3,3,2)

CARD: 121  
VARIABLE: AIO (3,3,1)

CARD: 120  
VARIABLE: AIO (3,2,3)

CARD: 119  
VARIABLE: AIO (3,2,2)

CARD: 118  
VARIABLE: AIO (3,2,1)

CARD: 117  
VARIABLE: AIO (3,1,3)

CARD: 116  
VARIABLE: AIO (3,1,2)

CARD: 115  
INSTRUCTION: IF NUMCMG < 3, OR IDOF (3) = 0, OR IDOF (3) = 1,  
IGNORE THE NEXT 9 CARDS.  
VARIABLE: AIO (3,1,1)  
FORMAT:  $\pm$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 127

INSTRUCTION: IF NUMCMG < 4, IGNORE THIS CARD.

VARIABLE: HW (4)

FORMAT:  $\pm$  .  $E\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 126

INSTRUCTION: IF NUMCMG < 4, IGNORE THIS CARD.

VARIABLE: IDOF (4)

FORMAT:

COLUMN: 3

CARD: 125

VARIABLE: FEED (3)

CARD: 124

INSTRUCTION: IF NUMCMG < 3, OR IDOF (3) = 0, OR IDOF (3) = 1,  
IGNORE THE NEXT 2 CARDS.

VARIABLE: FEE (3)

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 136  
VARIABLE: AOCJ (4,3,3)

CARD: 135  
VARIABLE: AOCJ (4,3,2)

CARD: 134  
VARIABLE: AOCJ (4,3,1)

CARD: 133  
VARIABLE: AOCJ (4,2,3)

CARD: 132  
VARIABLE: AOCJ (4,2,2)

CARD: 131  
VARIABLE: AOCJ (4,2,1)

CARD: 130  
VARIABLE: AOCJ (4,1,3)

CARD: 129  
VARIABLE: AOCJ (4,1,2)

CARD: 128  
INSTRUCTION: IF NUMCMG < 4, IGNORE THE NEXT 9 CARDS.  
VARIABLE: AOCJ (4,1,1)  
FORMAT:  $\frac{+}{-}$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 145  
VARIABLE: AII (4,3,3)

CARD: 144  
VARIABLE: AII (4,3,2)

CARD: 143  
VARIABLE: AII (4,3,1)

CARD: 142  
VARIABLE: AII (4,2,3)

CARD: 141  
VARIABLE: AII (4,2,2)

CARD: 140  
VARIABLE: AII (4,2,1)

CARD: 139  
VARIABLE: AII (4,1,3)

CARD: 138  
VARIABLE: AII (4,1,2)

CARD: 137  
INSTRUCTION: IF NUMCMG < 4, OR IDOF (4) = 0,  
              IGNORE THE NEXT 9 CARDS.  
VARIABLE: AII (4,1,1)  
FORMAT:   +       .  
COLUMN:    2 3 4 5 6 7 8 9 10 11 12

CARD: 147

INSTRUCTION: IF NUMCMG < 4, OR IDOF (4) = 0, IGNORE THIS CARD.

VARIABLE: THATA (4)

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 146

INSTRUCTION: IF NUMCMG < 4, OR IDOF (4) = 0, IGNORE THIS CARD.

VARIABLE: THATA (4)

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 156  
VARIABLE: AIO (4,3,3)

CARD: 155  
VARIABLE: AIO (4,3,2)

CARD: 154  
VARIABLE: AIO (4,3,1)

CARD: 153  
VARIABLE: AIO (4,2,3)

CARD: 152  
VARIABLE: AIO (4,2,2)

CARD: 151  
VARIABLE: AIO (4,2,1)

CARD: 150  
VARIABLE: AIO (4,1,3)

CARD: 149  
VARIABLE: AIO (4,1,2)

CARD: 148  
INSTRUCTION: IF NUMCMG < 4, OR IDOF (4) = 0, OR IDOF (4) = 1,  
                  IGNORE THE NEXT 9 CARDS.  
VARIABLE: AIO (4,1,1)  
FORMAT:    +       .  
COLUMN:    2 3 4 5 6 7 8 9 10 11 12



CARD: 160  
INSTRUCTION: IF NUMCMG < 5, IGNORE THIS CARD.  
VARIABLE: HW (5)  
FORMAT:  $\frac{+}{-}$  . E+  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 159  
INSTRUCTION: IF NUMCMG < 5, IGNORE THIS CARD.  
VARIABLE: IDOF (5)  
FORMAT:  
COLUMN: 3

CARD: 158  
VARIABLE: FEED (4)

CARD: 157  
INSTRUCTION: IF NUMCMG < 4, OR IDOF (4) = 0, OR IDOF (4) = 1,  
IGNORE THE NEXT 2 CARDS.  
VARIABLE: FEE (4)  
FORMAT:  $\frac{+}{-}$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 169  
VARIABLE: AOCJ (5,3,3)

CARD: 168  
VARIABLE: AOCJ (5,3,2)

CARD: 167  
VARIABLE: AOCJ (5,3,1)

CARD: 166  
VARIABLE: AOCJ (5,2,3)

CARD: 165  
VARIABLE: AOCJ (5,2,2)

CARD: 164  
VARIABLE: AOCJ (5,2,1)

CARD: 163  
VARIABLE: AOCJ (5,1,3)

CARD: 162  
VARIABLE: AOCJ (5,1,2)

CARD: 161  
INSTRUCTION: IF NUMCMG < 5, IGNORE THE NEXT 9 CARDS.  
VARIABLE: AOCJ (5,1,1)  
FORMAT:  $\pm$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 178  
VARIABLE: AII (5,3,3)

CARD: 177  
VARIABLE: AII (5,3,2)

CARD: 176  
VARIABLE: AII (5,3,1)

CARD: 175  
VARIABLE: AII (5,2,3)

CARD: 174  
VARIABLE: AII (5,2,2)

CARD: 173  
VARIABLE: AII (5,2,1)

CARD: 172  
VARIABLE: AII (5,1,3)

CARD: 171  
VARIABLE: AII (5,1,2)

CARD: 170  
INSTRUCTION: IF NUMCMG < 5, OR IDOF (5) = 0,  
                  IGNORE THE NEXT 9 CARDS.  
VARIABLE: AII (5,1,1)  
FORMAT:    +       .  
COLUMN:     2 3 4 5 6 7 8 9 10 11 12

CARD: 180

INSTRUCTION: IF NUMCMG < 5, OR IDOF (5) = 0, IGNORE THIS CARD.

VARIABLE: THATAD (5)

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 179

INSTRUCTION: IF NUMCMG < 5, OR IDOF (5) = 0, IGNORE THIS CARD.

VARIABLE: THATA (5)

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 189  
VARIABLE: AIO (5,3,3)

CARD: 188  
VARIABLE: AIO (5,3,2)

CARD: 187  
VARIABLE: AIO (5,3,1)

CARD: 186  
VARIABLE: AIO (5,2,3)

CARD: 185  
VARIABLE: AIO (5,2,2)

CARD: 184  
VARIABLE: AIO (5,2,1)

CARD: 183  
VARIABLE: AIO (5,1,3)

CARD: 182  
VARIABLE: AIO (5,1,2)

CARD: 181  
INSTRUCTION: IF NUMCMG < 5, OR IDOF (5) = 0, OR IDOF (5) = 1,  
IGNORE THE NEXT 9 CARDS.  
VARIABLE: AIO (5,1,1)  
FORMAT:  $\pm$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 193  
INSTRUCTION: IF NUMCMG < 6, IGNORE THIS CARD.  
VARIABLE: HW (6)  
FORMAT:  $\pm$  . E $\pm$   
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 192  
INSTRUCTION: IF NUMCMG < 6, IGNORE THIS CARD.  
VARIABLE: IDOF (6)  
FORMAT:  
COLUMN: 3

CARD: 191  
VARIABLE: FEED (5)

CARD: 190  
INSTRUCTION: IF NUMCMG < 5, OR IDOF (5) = 0, OR IDOF (5) = 1  
IGNORE THE NEXT 2 CARDS.  
VARIABLE: FEE (5)  
FORMAT:  $\pm$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 202  
VARIABLE: AOCJ (6,3,3)

CARD: 201  
VARIABLE: AOCJ (6,3,2)

CARD: 200  
VARIABLE: AOCJ (6,3,1)

CARD: 199  
VARIABLE: AOCJ (6,2,3)

CARD: 198  
VARIABLE: AOCJ (6,2,2)

CARD: 197  
VARIABLE: AOCJ (6,2,1)

CARD: 196  
VARIABLE: AOCJ (6,1,3)

CARD: 195  
VARIABLE: AOCJ (6,1,2)

CARD: 194  
INSTRUCTION: IF NUMCMG < 6, IGNORE THE NEXT 9 CARDS.  
VARIABLE: AOCJ (6,1,1)  
FORMAT:  $\pm$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 211  
VARIABLE: AII (6,3,3)

CARD: 210  
VARIABLE: AII (6,3,2)

CARD: 209  
VARIABLE: AII (6,3,1)

CARD: 208  
VARIABLE: AII (6,2,3)

CARD: 207  
VARIABLE: AII (6,2,2)

CARD: 206  
VARIABLE: AII (6,2,1)

CARD: 205  
VARIABLE: AII (6,1,3)

CARD: 204  
VARIABLE: AII (6,1,2)

CARD: 203  
INSTRUCTION: IF NUMCMG < 6, OR IDOF (6) = 0,  
IGNORE THE NEXT 9 CARDS.  
VARIABLE: AII (6,1,1)  
FORMAT:  $\frac{+}{-}$  .  
COLUMN: 2 3 4 5 6 7 8 9 10 11 12



CARD: 213

INSTRUCTION: IF NUMCMG < 6, OR IDOF (6) = 0, IGNORE THIS CARD.

VARIABLE: THATAD (6)

FORMAT:  $\frac{+}{.}$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 212

INSTRUCTION: IF NUMCMG < 6, OR IDOF (6) = 0, IGNORE THIS CARD.

VARIABLE: THATA (6)

FORMAT:  $\frac{+}{.}$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 222  
VARIABLE: AIO (6,3,3)

CARD: 221  
VARIABLE: AIO (6,3,2)

CARD: 220  
VARIABLE: AIO (6,3,1)

CARD: 219  
VARIABLE: AIO (6,2,3)

CARD: 218  
VARIABLE: AIO (6,2,2)

CARD: 217  
VARIABLE: AIO (6,2,1)

CARD: 216  
VARIABLE: AIO (6,1,3)

CARD: 215  
VARIABLE: AIO (6,1,2)

CARD: 214  
INSTRUCTION: IF NUMCMG < 6, OR IDOF (6) = 0, OR IDOF (6) = 1,  
                  IGNORE THE NEXT 9 CARDS.  
VARIABLE: AIO (6,1,1)  
FORMAT:   +       .  
COLUMN:    2 3 4 5 6 7 8 9 10 11 12

DUE TO MODIFICATIONS, THE NEXT DATA CARD  
HAS THE NUMBER 230.

CARD: 227

INSTRUCTION: IF IPROPF OR IATTIF = 0, IGNORE THIS CARD.

VARIABLES: CA(1) CA(2) CA(3)

FORMAT:  $\pm$  .  $\pm$  .  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 226

INSTRUCTION: IF IPROPF = 0, IGNORE THIS CARD.

VARIABLE: IATTIF

FORMAT:

COLUMN: 1

CARD: 225

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: IPROPF

FORMAT:

COLUMN: 1

CARD: 224

VARIABLE: FEED (6)

CARD: 223

INSTRUCTION: IF NUMCMG < 6, OR IDOF (6) = 0, OR IDOF (6) = 1,  
IGNORE THE NEXT 2 CARDS.

VARIABLE: FEE (6)

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

DUE TO MODIFICATIONS, THE NEXT DATA CARD  
HAS THE NUMBER 242.

CARD: 232

VARIABLES: AOJ (3)

CGAINO (3)

CARD: 231

VARIABLES: AOJ (2)

CGAINO (2)

CARD: 230

INSTRUCTION: IF IPROP = 0, IGNORE THE NEXT 3 CARDS.

VARIABLES: AOJ(1)

CGAINO(1)

FORMAT:  $\pm$  . E $\pm$

$\pm$  . E $\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

1 15 17 18 19 20 21 22 23 24 25

PRECEDING PAGE BLANK NOT FILMED

CARD: 251  
VARIABLE: BODYII (3,3)

CARD: 250  
VARIABLE: BODYII (3,2)

CARD: 249  
VARIABLE: BODYII (3,1)

CARD: 248  
VARIABLE: BODYII (2,3)

CARD: 247  
VARIABLE: BODYII (2,2)

CARD: 246  
VARIABLE: BODYII (2,1)

CARD: 245  
VARIABLE: BODYII (1,3)

CARD: 244  
VARIABLE: BODYII (1,2)

CARD: 243  
INSTRUCTION: THE NEXT 9 CARDS MUST ALWAYS BE PRESENT.  
VARIABLE: BODYII (1,1)  
FORMAT:  $\pm$  .  $E\pm$   
COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 255

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: IB2F

FORMAT:

COLUMN: 3

CARD: 254

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLES: DO1(1) DO1(2) DO1(3)

FORMAT:  $\pm$  .  $\pm$  .  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 253

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: OMEGA1

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 252

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: THETA1

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 259  
 INSTRUCTION: IF IB2F = 0, IGNORE THIS CARD.  
 VARIABLES: S SDOT  
 FORMAT:  $\frac{+}{-}$  .  $\frac{+}{-}$  .  
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25

CARD: 258  
 INSTRUCTION: IF IB2F = 0, IGNORE THIS CARD.  
 VARIABLES: S2(1) S2(2) S2(3)  
 FORMAT:  $\frac{+}{-}$  .  $\frac{+}{-}$  .  $\frac{+}{-}$  .  
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 257  
 INSTRUCTION: IF IB2F = 0, IGNORE THIS CARD.  
 VARIABLES: D12(1) D12(2) D12(3)  
 FORMAT:  $\frac{+}{-}$  .  $\frac{+}{-}$  .  $\frac{+}{-}$  .  
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 256  
 INSTRUCTION: IF IB2F = 0, IGNORE THIS CARD.  
 VARIABLE: B2MASS  
 FORMAT:  $\frac{+}{-}$  . E $\frac{+}{-}$   
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12

DUE TO MODIFICATIONS, THE NEXT DATA CARD  
HAS THE NUMBER 268.

CARD: 261

VARIABLES: ALJ(2)

CGAIN1(2)

CARD: 260

INSTRUCTION: IF IPROFF = 0, IGNORE THE NEXT 2 CARDS.

VARIABLES: ALJ(1)

CGAIN1(1)

FORMAT:  $\pm$  . . E $\pm$

$\pm$  . . E $\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

15 16 17 18 19 20 21 22 23 24 25



CARD: 271  
 INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.  
 VARIABLES: D13(1) D13(2) D13(3)  
 FORMAT:  $\pm$  .  $\pm$  .  $\pm$  .  
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 270  
 INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.  
 VARIABLE: B3MASS  
 FORMAT:  $\pm$  . E $\pm$   
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 269  
 INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.  
 VARIABLE: CP2  
 FORMAT:  $\pm$  . E $\pm$   
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 268  
 INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.  
 VARIABLE: CP1  
 FORMAT:  $\pm$  . E $\pm$   
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 279

INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.

VARIABLE: PEND4L

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 278

INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.

VARIABLES: S4(1) S4(2) S4(3)

FORMAT:  $\pm$  .  $\pm$  .  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 277

INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.

VARIABLES: D14(1) D14(2) D14(3)

FORMAT:  $\pm$  .  $\pm$  .  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 276

INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.

VARIABLE: B4MASS

FORMAT:  $\pm$  . E $\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 275

INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.

VARIABLE: OMEGA3

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 274

INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.

VARIABLE: THETA3

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 273

INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.

VARIABLE: PEND3L

FORMAT:  $\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 272

INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.

VARIABLES: S3(1)

S3(2)

S3(3)

FORMAT:  $\pm$  .

$\pm$  .

$\pm$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

15 16 17 18 19 20 21 22 23 24 25

26 27 28 29 30 31 32 33 34 35 36 37 38

CARD: 283

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: NGAIN

FORMAT:

COLUMN: 2 3

CARD: 282

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: SP

FORMAT:  $\frac{+}{-}$  .

2 3 4 5 6 7 8 9 10 11 12

CARD: 281

INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD

VARIABLE: OMEGA4

FORMAT:  $\frac{+}{-}$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 280

INSTRUCTION: IF IPNDLM = 0, IGNORE THIS CARD.

VARIABLE: THETA4

FORMAT:  $\frac{+}{-}$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 288

INSTRUCTION: IF NGAIN < 5, IGNORE THIS CARD.

VARIABLE: GAIN (5)

FORMAT:  $\frac{+}{-}$  .  $\frac{E+}{-}$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 287

INSTRUCTION: IF NGAIN < 4, IGNORE THIS CARD.

VARIABLE: GAIN (4)

FORMAT:  $\frac{+}{-}$  .  $\frac{E+}{-}$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 286

INSTRUCTION: IF NGAIN < 3, IGNORE THIS CARD.

VARIABLE: GAIN (3)

FORMAT:  $\frac{+}{-}$  .  $\frac{E+}{-}$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 285

INSTRUCTION: IF NGAIN < 2, IGNORE THIS CARD.

VARIABLE: GAIN (2)

FORMAT:  $\frac{+}{-}$  .  $\frac{E+}{-}$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 284

INSTRUCTION: IF NGAIN = 0, IGNORE THIS CARD.

VARIABLE: GAIN (1)

FORMAT:  $\frac{+}{-}$  .  $\frac{E+}{-}$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 293

INSTRUCTION: IF NGAIN < 10, IGNORE THIS CARD.

VARIABLE: GAIN (10)

FORMAT:  $\pm$  .  $E\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 292

INSTRUCTION: IF NGAIN < 9, IGNORE THIS CARD.

VARIABLE: GAIN (9)

FORMAT:  $\pm$  .  $E\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 291

INSTRUCTION: IF NGAIN < 8, IGNORE THIS CARD.

VARIABLE: GAIN (8)

FORMAT:  $\pm$  .  $E\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 290

INSTRUCTION: IF NGAIN < 7, IGNORE THIS CARD.

VARIABLE: GAIN (7)

FORMAT:  $\pm$  .  $E\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 289

INSTRUCTION: IF NGAIN < 6, IGNORE THIS CARD.

VARIABLE: GAIN (6)

FORMAT:  $\pm$  .  $E\pm$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 297

INSTRUCTION: IF IDOCK = 0, IGNORE THIS CARD.

VARIABLE: BDMASS

FORMAT:  $\frac{+}{-}$  . E $\frac{+}{-}$

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 296

INSTRUCTION: IF IDOCK = 0, IGNORE THIS CARD.

VARIABLE: DTIME

FORMAT:  $\frac{+}{-}$  .

COLUMN: 2 3 4 5 6 7 8 9 10 11 12

CARD: 295

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: IDOCK

FORMAT:

COLUMN: 3

CARD: 294

INSTRUCTION: THIS CARD MUST ALWAYS BE PRESENT.

VARIABLE: IGRAVF

FORMAT:

COLUMN: 3

CARD: 306  
VARIABLE: BODYDI (3,3)

CARD: 305  
VARIABLE: BODYDI (3,2)

CARD: 304  
VARIABLE: BODYDI (3,1)

CARD: 303  
VARIABLE: BODYDI (2,3)

CARD: 302  
VARIABLE: BODYDI (2,2)

CARD: 301  
VARIABLE: BODYDI (2,1)

CARD: 300  
VARIABLE: BODYDI (1,3)

CARD: 299  
VARIABLE: BODYDI (1,2)

CARD: 298  
INSTRUCTION: IF IDOCK = 0, IGNORE THE NEXT 9 CARDS.  
VARIABLE: BODYDI (1,1)  
FORMAT:  $\pm$  . E $\pm$   
COLUMN: 2 3 4 5 6 7 8 9 10 11 12



CARD: 308  
 INSTRUCTION: IF IDOCK = 0, IGNORE THIS CARD.  
 VARIABLES: DD01(1) DD01(2) DD01(3)  
 FORMAT: + . + . + .  
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

CARD: 307  
 INSTRUCTION: IF IDOCK = 0, IGNORE THIS CARD.  
 VARIABLES: DTI(1) DTI(2) DTI(3)  
 FORMAT: + . + . + .  
 COLUMN: 2 3 4 5 6 7 8 9 10 11 12 15 16 17 18 19 20 21 22 23 24 25 28 29 30 31 32 33 34 35 36 37 38

## APPENDIX A, DEFINITIONS AND REFERENCES FOR INPUT VARIABLES

This appendix is in two parts. The first part contains a list of all input variables in alphabetical order. The second part contains the input variables in categories and the input variables in each category are alphabetized.

AII(J,M,N):

$$[AII(J,M,N)] = [II_J] = \begin{bmatrix} AII(J,1,1) & AII(J,1,2) & AII(J,1,3) \\ AII(J,2,1) & AII(J,2,2) & AII(J,2,3) \\ AII(J,3,1) & AII(J,3,2) & AII(J,3,3) \end{bmatrix}$$

This array is the inertia matrix for the inner gimbal of the Jth control moment gyro aboard the stator. A maximum of six CMGs may be used. (i.e. J = 1,6) All CMGs are also constrained to be located at the center of mass on the stator, body 0. If the Jth CMG has one or two degrees of freedom, it will have an inner gimbal. (Refer to the write up on CMGs for further discussion.)

UNITS: (slug-ft<sup>2</sup>)

FORMAT: # 5006 = (1X, F11.5)

AIO(J,M,N):

$$[AIO(J,M,N)] = [IO_J] = \begin{bmatrix} AIO(J,1,1) & AIO(J,1,2) & AIO(J,1,3) \\ AIO(J,2,1) & AIO(J,2,2) & AIO(J,2,3) \\ AIO(J,3,1) & AIO(J,3,2) & AIO(J,3,3) \end{bmatrix}$$

This array is the inertia matrix for the outer gimbal of the Jth control moment gyro aboard the stator. A maximum of six CMGs may be used. (i.e. J = 1,6) All CMGs are constrained to be located at the center of mass on the stator, body 0. The

Jth CMG will have an outer gimbal only if it has two degrees of freedom. (Refer to the write up on CMGs for further discussion.)

UNITS: (slug-ft<sup>2</sup>)

FORMAT: # 5006 = (1X, F11.5)

ALT:

ALT is altitude of the center of mass of the space station configuration measured from the surface of the earth. All orbits are constrained to be circular with no oblateness effects. Therefore, altitude is the only pertinent orbit parameter.

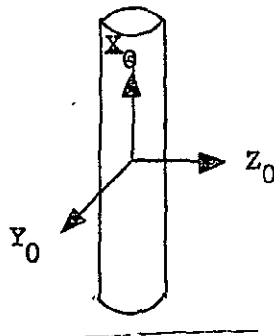
UNITS: (miles)

FORMAT: # 5004 = (1X, E11.4)

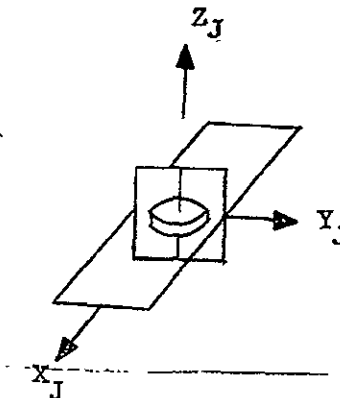
AOCJ(J,M,N):

$$[AOCJ(J,M,N)] = [O,C_J] = \begin{bmatrix} AOCJ(J,1,1) & AOCJ(J,1,2) & AOCJ(J,1,3) \\ AOCJ(J,2,1) & AOCJ(J,2,2) & AOCJ(J,2,3) \\ AOCJ(J,3,1) & AOCJ(J,3,2) & AOCJ(J,3,3) \end{bmatrix}$$

This array is the coordinate transformation matrix from the CMG null gimbal coordinate frame to the coordinate frame of body 0, the stator. (Refer to the coordinate transformation appendix.) For example, consider the two coordinate systems shown below:



Body 0 Frame



Jth Null Gimbal Frame

For the above situation:

$$[AOCJ(J,M,N)] = \begin{bmatrix} 0. & 0. & 1. \\ 1. & 0. & 0. \\ 0. & 1. & 0. \end{bmatrix}$$

UNITS: (None)

FORMAT: # 5006 = (1X, F11.5)

AOJ(M):

AOJ(1) is the distance between the jets of the pure couple producing the torque around the X axis of body 0.

AOJ(2) is the distance between the jets of the pure couple producing the torque around the Y axis of body 0.

AOJ(3) is the distance between the jets of the pure couple producing the torque around the Z axis of body 0.

Note: The variables CGAIN0(1), CGAIN0(2), and CGAIN0(3) are also read on the same data cards as AOJ(1), AOJ(2), and AOJ(3). Punch the values of AOJ(1), AOJ(2), and AOJ(3) in columns 2 through 12 of the data cards. Non-zero values should be read in for AOJ(M). Control on an axis can be disabled by reading zero for the CGAIN0.

UNITS: (feet)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

AIJ(M):

AIJ(1) is the distance between the jets of the pure couple producing the torque around the X axis of body 1.

AIJ(2) is the distance between the jets of the pure couple producing the torque around the Y axis of body 1.

Note: The variables CGAIN1(1) and CGAIN1(2) are also read on the same data cards as AIJ(1) and AIJ(2). Punch the values of AIJ(1) and AIJ(2) in columns 2 through 12 of the data cards. Non-zero values should

be read in for ALJ(M). Control on an axis can be disabled by reading zero for the CGAIN1.

UNITS: (feet)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

BDMASS:

BDMASS is the sum of the mass of body 0, the stator, and the mass of the docking vehicle. The docking vehicle is constrained to dock on body 0, the stator.  $BDMASS = m_D$

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

BODYDI (M,N):

$$[BODYDI(M,N)] = [I_D] = \begin{bmatrix} BODYDI(1,1) & BODYDI(1,2) & BODYDI(1,3) \\ BODYDI(2,1) & BODYDI(2,2) & BODYDI(2,3) \\ BODYDI(3,1) & BODYDI(3,2) & BODYDI(3,3) \end{bmatrix}$$

This array is the inertia matrix of the docked body which consists of the docking vehicle connected to the stator.

UNITS: (slug-ft<sup>2</sup>)

FORMAT: # 5004 = (1X, E11.4)

BODYOI (M,N):

$$[BODYOI(M,N)] = [I_0] = \begin{bmatrix} BODYOI(1,1) & BODYOI(1,2) & BODYOI(1,3) \\ BODYOI(2,1) & BODYOI(2,2) & BODYOI(2,3) \\ BODYOI(3,1) & BODYOI(3,2) & BODYOI(3,3) \end{bmatrix}$$

This array is the inertia matrix of body 0, the stator.

UNITS: (slug-ft<sup>2</sup>).

FORMAT: # 5004 = (1X, E11.4)

BODY1I(M,N):

$$[BODY1I(M,N)] = [I_1] = \begin{bmatrix} BODY1I(1,1) & BODY1I(1,2) & BODY1I(1,3) \\ BODY1I(2,1) & BODY1I(2,2) & BODY1I(2,3) \\ BODY1I(3,1) & BODY1I(3,2) & BODY1I(3,3) \end{bmatrix}$$

This array is the inertia matrix for body 1, the rotor.

UNITS: (slug-ft<sup>2</sup>)

FORMAT: # 5004 = (1X, E11.4)

BOMASS:

BOMASS is the mass of body 0, the stator. BOMASS = m<sub>0</sub>

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

B1MASS:

B1MASS is the mass of body 1, the rotor. B1MASS = m<sub>1</sub>

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

B2MASS:

B2MASS is the mass of body 2, the elevator. B2MASS = m<sub>2</sub>

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

B3MASS:

B3MASS is the mass of body 3, a pendulum.  $B3MASS = m_3$

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

B4MASS:

B4MASS is the mass of body 4, a pendulum.  $B4MASS = m_4$

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

CA(M):

CA(1), CA(2), and CA(3) are the three direction cosines of the desired attitude reference direction in the inertial frame.

UNITS: (None)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

CGAINO(M):

CGAINO(1) equals the control gain of all four reaction jets in the pure force couples producing torque around the X axis of body 0.

CGAINO(2) equals the control gain of all four reaction jets in the pure force couples producing torque around the Y axis of body 0.

CGAINO(3) equals the control gain of all four reaction jets in the pure force couples producing torque around the Z axis of body 0.

Note: The variables AOJ(1), AOJ(2), and AOJ(3) are also read in on the same data cards as CGAINO(1), CGAINO(2), and CGAINO(3). Punch the values of CGAINO(1), CGAINO(2), and CGAINO(3) in columns 15 through 25 of the data cards.

UNITS: (lb/radians/second)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

#### CGAIN1(M):

CGAIN1(1) equals the control gain of all four reaction jets in the pure force couples producing torque around the X axis of body 1.

CGAIN1(2) equals the control gain of all four reaction jets in the pure force couples producing torque around the Y axis of body 1.

Note: The variables ALJ(1) and ALJ(2) are also read in on the same data cards as CGAIN1(1) and CGAIN1(2). Punch the values of CGAIN1(1) and CGAIN1(2) in columns 15 through 25 of the data cards.

UNITS: (lb/radians/second)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

#### CP1 and CP2:

CP1 and CP2 are parameters used in determining the stiffness and the resonant frequency of the pendulums. For example, the control laws which are governed by the parameters are:

$$T13 = - CP1 * OMEGA3 - CP2 * THETA3$$

$$T14 = - CP1 * OMEGA4 - CP2 * (THETA4 - \pi)$$

Note: These variables are read on separate data cards.

UNITS: (none)

FORMAT: # 5004 = (1X, E11.4)



DD01(M):

DD01(1), DD01(2), and DD01(3) are the X, Y, and Z components of the vector from the center of mass of the docked body to the hinge line of body 1, the rotor. The vector is expressed in body 0 coordinates. The docked body shall be defined as the configuration of the docking vehicle attached to body 0.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

DELTAT:

DELTAT =  $\Delta t$

DELTAT is the time increment used in the integration algorithm which solves the rotational equations of motion. When "TIME" is updated we have:

TIME = TIME + DELTAT

Note: Punch the value of DELTAT in columns 28 through 38

UNITS: (seconds)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

D01(M):

D01(1), D01(2), and D01(3) are the X, Y, and Z components of the vector from the center of mass of body 0 to the hinge line of body 1, the rotor. The vector is expressed in body 0 coordinates. D01(1) should in most cases be zero.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

DTI(M):

DTI(1), DTI(2) and DTI(3) are the X, Y, and Z components of the docking torque impulse.

UNITS: 1b-ft-sec

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

DTIME:

DTIME is the time when docking occurs. (i.e. "Docking Time")  
The restrictions placed on DTIME are as follows:

- a)  $T_{\text{start}} < \text{DTIME} < T_{\text{stop}}$
- b) DTIME must be an integer multiple of  $\Delta t$ .

UNITS: (seconds)

FORMAT: # 5006 = (1X, F11.5)

D12(M):

D12(1), D12(2) and D12(3) are the X, Y and Z components of a fixed vector locating the starting position of the movable mass, the elevator. The vector equation that describes the motion of the movable mass is  $\vec{r}_2 = \vec{d}_{12} + \vec{s}_2 s$ . Where  $\vec{s}_2$  is a unit vector which defines the direction in which the movable mass travels and  $s$  is a scalar prespecified function of time. For most cases  $s(t_0 = 0) = 0$  so that  $\vec{d}_{12}$  specifies the initial starting position of the movable mass. The elevator is known alternately as the movable mass or body 2. D12 is expressed in body 1 coordinates. For example, if the elevator were constrained to travel along the X axis, then  $\vec{d}_{12}$  could have the following values: D12(1) = 1., D12(2) = 0., D12(3) = 0.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

D13(M):

D13(1), D13(2), and D13(3) are the X, Y, and Z components of the vector from the center of mass of body 1 to the hinge line of body 3. D13 is expressed in body 1 coordinates.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

D14(M):

D14(1), D14(2), and D14(3) are the X, Y, and Z components of the vector from the center of mass of body 1 to the hinge line of body 4.

D14 is expressed in body 1 coordinates.

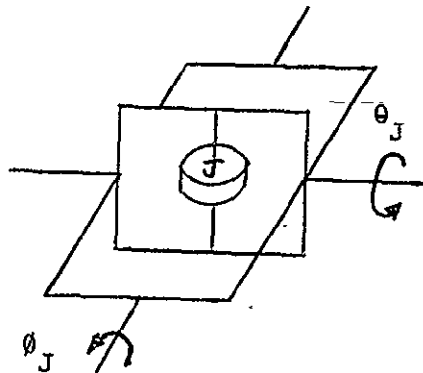
UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

FEE(J):

$$FEE(J) = \phi_J$$

FEE(J) is the outer gimbal angle of a two degree of freedom control moment gyro as shown pictorially below:



The subscript J refers to the number assigned to the CMG. (Refer to the write up on CMGs for further discussion.)

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{start}$

FEED(J):

$$FEED(J) = \dot{\theta}_J$$

FEED(J) is the outer gimbal rate of a two degree of freedom control moment gyro. The subscript J refers to the number assigned to the CMG. (Refer to the write up on CMGs for further discussion.)

UNITS: (radians/second)

FORMAT: # 5006 = (1X, F11.5)

GAIN(M):

GAIN(M) is an array of numbers the dimension of which is determined by another input variable NGAIN. These numbers, once read in, are stored in common and can be used for a variety of purposes. In many CMG control laws it is necessary to have control gains. GAIN(M) can be used for this purpose among others.

UNITS: (None)

FORMAT: # 5004 = (1X, E11.4)

HW(J):

HW(J) is the angular momentum of the wheel associated with the Jth momentum device. (Refer to the write up on CMGs for further discussion.)

UNITS: (slug-ft<sup>2</sup>/second)

FORMAT: # 5004 = (1X, E11.4)

IATTIF:

IATTIF is the attitude flag.

IATTIF = 1 implies an attempt to change attitude will be made.

IATCIF = 0 implies an attempt to change attitude will not be made.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IB2F:

IB2F is the body 2 flag. (i.e. the elevator flag)

IB2F = 1 implies body 2 will be present.

IB2F = 0 implies body 2 will not be present.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IDOCK:

IDOCK is the docking flag.

IDOCK = 1 implies docking will occur.

IDOCK = 0 implies docking will not occur.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IDOF(J):

IDOF(J) = 0 implies the Jth controller aboard body 0 is a reaction wheel.

IDOF(J) = 1 implies the Jth controller aboard body 0 is a one degree of freedom control moment gyro.

IDOF(J) = 2 implies the Jth controller aboard body 0 is a two degree of freedom control moment gyro.

SPECIAL INSTRUCTIONS: Punch a 0, 1, or a 2 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, 12)

IGRAVF:

IGRAVF is the gravity gradient flag.

IGRAVF = 1 implies gravity gradient torques will be present.

IGRAVF = 0 implies gravity gradient torques will not be present.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, 12)

IPNDLM:

IPNDLM is the pendulum flag.

IPNDLM = 1 implies body 3 and body 4, the pendulums, will be present.

IPNDLM = 0 implies body 3 and body 4, the pendulums, will not be present.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, 12)

IPRINT:

IPRINT is an integer variable used to determine how often output data is printed. Data is printed in time increments of IPRINT \* DELTAT. For example, if IPRINT = 50 and DELTAT = .2, then data will be printed when time = 10, 20, 30, 40, 50, . . . .

SPECIAL INSTRUCTIONS: If IPRINT has a value less than 10, punch the integer in column 3 of the data card. If IPRINT has a value greater than 9, punch the integer in columns 2 and 3.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IPROPF:

IPROPF is the propulsion flag.

IPROPF = 1 implies propulsion forces will be considered.

IPROPF = 0 implies propulsion forces will not be considered.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

NDECK:

NDECK is an integer variable equal to the number of data decks present at run time.

SPECIAL INSTRUCTIONS: This variable goes in front of the first data deck only. If NDECK has a value less than 10, punch the integer in column 3 of the data card. If NDECK has a value greater than 9, punch the integer in columns 2 and 3.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

#### NGAIN:

NGAIN is an integer variable and refers to the number of arbitrary gains which are input. If  $NGAIN = 3$  then values for  $GAIN(1)$ ,  $GAIN(2)$  and  $GAIN(3)$  will be input. The maximum value of NGAIN is 10.

SPECIAL INSTRUCTIONS: If NGAIN has a value less than 10, punch the integer in column 3 of the data card. Otherwise, use columns 2 and 3.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

#### NUMCMG:

NUMCMG is the number of controllers aboard body 0. A maximum of 6 controllers may be used.

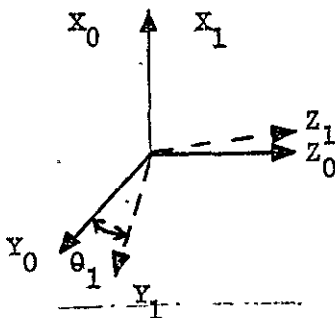
SPECIAL INSTRUCTIONS: Punch the integer in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

#### OMEGA1:

OMEGA1 is the initial relative angular velocity measure about the spin axis between bodies 0 and 1. Another definition of OMEGA1 can be visualized by referring to the sketch shown below showing the orthogonal coordinate systems located on bodies 0 and 1.





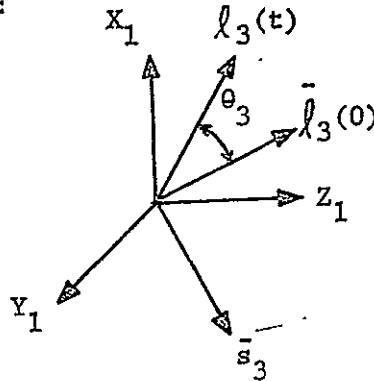
Implicit in this sketch is the hinge line between the stator and rotor is aligned parallel to both the  $\bar{X}_0$  and  $\bar{X}_1$  axes. Therefore, the orientation of the stator and the rotor differ only in a rotation  $\theta_1 = \text{THETA1}$  and  $\text{OMEGA1} = \dot{\theta}_1$ .

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

#### OMEGA3:

OMEGA3 is the angular velocity of body 3 about the hinge line  $\bar{s}_3$ . OMEGA3 is also the time derivative of THETA3 when the datum for the angle THETA3 will be the  $\bar{Y}_1, \bar{Z}_1$  plane as illustrated below:



In other words,  $\bar{s}_3$  determines the positive direction of rotation by the right hand rule and the positive  $Y_1 - Z_1$  plane determines the starting position.

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{\text{start}}$

#### OMEGA4:

OMEGA4 is the angular velocity of body 4 about the hinge line  $\bar{s}_4$ . OMEGA4 is also the time derivative of THETA4 where the datum for the angle THETA4 is the same as THETA3. (See OMEGA3)

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{\text{start}}$

PEND3L:

PEND3L is the scalar distance from the hinge line,  $\bar{s}_3$ , to the center of mass of body 3. (i.e. the length of pendulum 3)

UNITS: (feet)

FORMAT: # 5006 = (1X, F11.5)

PEND4L:

PEND4L is the scalar distance from the hinge line,  $\bar{s}_4$ , to the center of mass of body 4. (i.e. the length of pendulum 4)

UNITS: (feet)

FORMAT: # 5006 = (1X, F11.5)

S:

S is a scalar parameter used in defining the position of body 2. S defines the magnitude of displacement of body 2 from the zero position.

Note: Punch the value of S in columns 2 through 12.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

INITIAL VALUE AT TIME =  $T_{\text{start}}$

SDOT:

SDOT defines the magnitude of the velocity vector of body 2.

Note: Punch the value of SDOT in columns 15 through 25.

UNITS: (feet per second)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

INITIAL VALUE AT TIME =  $T_{\text{start}}$

SP:

SP is the desired spin magnitude of body 1 relative to body 0.

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

S2(M):

S2(1), S2(2), and S2(3) are the X, Y, and Z components of a unit vector defining the direction of travel of body 2.  $\bar{s}_2$  is expressed in body 1 coordinates.

UNITS: (none)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

S3(M):

S3(1), S3(2), and S3(3) are the X, Y, and Z components of a unit vector which defines the hinge line of body 3.  $\bar{s}_3$  is expressed in body 1 coordinates. S3(1) must always be zero.

UNITS: (none)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

S4(M):

S4(1), S4(2), and S4(3) are the X, Y, and Z components of a unit vector which defines the hinge line of body 4.  $\bar{s}_4$  is expressed in body 1 coordinates. S4(1) must always be zero.

UNITS: (none)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

### THATA(J):

THATA(J) is the gimbal angle of the Jth controller aboard body 0 assuming this controller is either a one or two degree of freedom control moment gyro. If it is a two degree of freedom CMG, then this variable refers to the inner gimbal angle. J may have a maximum value of 6.

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{start}$

### THATAD(J):

THATAD(J) is the gimbal rate associated with THATA(J).

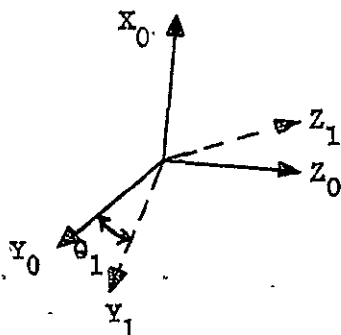
UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{start}$

### THETA1:

THETA1 is the relative angular displacement measured about the spin axis, between bodies 0 and 1.



UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{start}$

THETA3:

THETA3 is the angle between pendulum 3 and the Y, Z, plane. The axis about which THETA3 rotates is the hinge line  $s_3$ . For an explanation of the THETA3 datum refer to the discussion of OMEGA3.

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{start}$

THETA4:

THETA4 is the angle between pendulum 4 and the Y, Z, plane. The axis about which THETA4 rotates is the hinge line  $s_4$ . The datum for THETA4 is the same as for THETA3.

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{start}$

TIBOI(M,N):

$$[TIBOI(M,N)] = \begin{bmatrix} TIBOI(1,1) & TIBOI(1,2) & TIBOI(1,3) \\ TIBOI(2,1) & TIBOI(2,2) & TIBOI(2,3) \\ TIBOI(3,1) & TIBOI(3,2) & TIBOI(3,3) \end{bmatrix}$$

This array is the initial transformation matrix of the body 0 coordinate system to the inertial coordinate system. If initially body 0 is aligned with the inertial system, TIBOI(M,N) would be the identity matrix. Refer to the coordinate transformation appendix for further details.

UNITS: (none)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUES AT TIME =  $T_{start}$

TSTART:

TSTART is the time at which you wish the program to start calculating the equations of motion. Except for restarting, TSTART is usually set to zero.

SPECIAL INSTRUCTIONS: Punch the value of TSTART in columns 2 through 12.

UNITS: (seconds)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

TSTOP:

TSTOP is the time at which you wish the program to stop calculating.

SPECIAL INSTRUCTIONS: Punch the value of TSTOP in columns 15 through 25.

UNITS: (seconds)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

WO(M):

WO(1), WO(2), and WO(3) are the X, Y, and Z components of the angular velocity vector of body 0.

UNITS: (radians per second)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

INITIAL VALUES AT TIME =  $T_{\text{start}}$

## GENERAL INPUT VARIABLES

### ALT:

ALT is altitude of the center of mass of the space station configuration measured from the surface of the earth. All orbits are constrained to be circular with no oblateness effects. Therefore, altitude is the only pertinent orbit parameter.

UNITS: (miles)

FORMAT: # 5004 = (1X, E11.4)

### BDMASS:

BDMASS is the sum of the mass of body 0, the stator, and the mass of the docking vehicle. The docking vehicle is constrained to dock on body 0, the stator.  $BDMASS = m_D$

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

### BODYDI(M,N):

$$[BODYDI(M,N)] = [I_D] = \begin{bmatrix} BODYDI(1,1) & BODYDI(1,2) & BODYDI(1,3) \\ BODYDI(2,1) & BODYDI(2,2) & BODYDI(2,3) \\ BODYDI(3,1) & BODYDI(3,2) & BODYDI(3,3) \end{bmatrix}$$

This array is the inertia matrix of the docked body which consists of the docking vehicle connected to the stator.

UNITS: (slug-ft<sup>2</sup>)

FORMAT: # 5004 = (1X, E11.4)

CA(M):

CA(1), CA(2), and CA(3) are the three direction cosines of the desired attitude reference direction in the inertial frame.

UNITS: (None)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

CP1 and CP2:

CP1 and CP2 are parameters used in determining the stiffness and the resonant frequency of the pendulums. For example, the control laws which are governed by the parameters are:

$$T13 = - CP1 * OMEGA3 - CP2 * THETA3$$

$$T14 = - CP1 * OMEGA4 - CP2 * (THETA4 - \pi)$$

Note: These variables are read on separate data cards.

UNITS: (none)

FORMAT: # 5004 = (1X, E11.4)

DD01(M):

DD01(1), DD01(2), and DD01(3) are the X, Y, and Z components of the vector from the center of mass of the docked body to the hinge line of body 1, the rotor. The vector is expressed in body 0 coordinates. The docked body shall be defined as the configuration of the docking vehicle attached to body 0.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))



DELTAT:

$$\text{DELTAT} = \Delta t$$

DELTAT is the time increment used in the integration algorithm which solves the rotational equations of motion. When "TIME" is updated we have:

$$\text{TIME} = \text{TIME} + \text{DELTAT}$$

Note: Punch the value of DELTAT in columns 28 through 38.

UNITS: (seconds)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

DTI(M):

DTI(1), DTI(2) and DTI(3) are the X, Y, and Z components of the docking torque impulse.

UNITS: lb-ft-sec

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

DTIME:

DTIME is the time when docking occurs. (i.e. "Docking Time"). The restrictions placed on DTIME are as follows:

a)  $T_{\text{start}} < \text{DTIME} < T_{\text{stop}}$

b) DTIME must be an integer multiple of  $\Delta t$ .

UNITS: (seconds)

FORMAT: # 5006 = (1X, F11.5)

GAIN(M):

GAIN(M) is an array of numbers the dimension of which is determined by another input variable NGAIN. These numbers, once read in, are stored in common and can be used for a variety of purposes. In many CMG control laws it is necessary to have control gains. GAIN(M) can be used for this purpose among others.

UNITS: (None)

FORMAT: # 5004 = (1X, E11.4)

IATTIF:

IATTIF is the attitude flag.

IATTIF = 1 implies an attempt to change attitude will be made.

IATTIF = 0 implies an attempt to change attitude will not be made.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IB2F:

IB2F is the body 2 flag. (i.e. the elevator flag)

IB2F = 1 implies body 2 will be present.

IB2F = 0 implies body 2 will not be present.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IDOCK:

IDOCK is the docking flag.

IDOCK = 1 implies docking will occur.

IDOCK = 0 implies docking will not occur.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IGRAVF:

IGRAVF is the gravity gradient flag.

IGRAVF = 1 implies gravity gradient torques will be present.

IGRAVF = 0 implies gravity gradient torques will not be present.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IPNDLM:

IPNDLM is the pendulum flag.

IPNDLM = 1 implies body 3 and body 4, the pendulums, will be present.

IPNDLM = 0 implies body 3 and body 4, the pendulums, will not be present.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IPRINT:

IPRINT is an integer variable used to determine how often output data is printed. Data is printed in time increments of  $IPRINT * DELTAT$ . For example, if  $IPRINT = 50$  and  $DELTAT = .2$ , then data will be printed when time = 10, 20, 30, 40, 50, . . . .

SPECIAL INSTRUCTIONS: If IPRINT has a value less than 10, punch the integer in column 3 of the data card. If IPRINT has a value greater than 9, punch the integer in columns 2 and 3.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

IPROPF:

IPROPF is the propulsion flag.

IPROPF = 1 implies propulsion forces will be considered.

IPROPF = 0 implies propulsion forces will not be considered.

SPECIAL INSTRUCTIONS: Punch a 0 or a 1 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

NDECK:

NDECK is an integer variable equal to the number of data decks present at run time.

SPECIAL INSTRUCTIONS: This variable goes in front of the first data deck only. If NDECK has a value less than 10, punch the integer in column 3 of the data card. If NDECK has a value greater than 9, punch the integer in columns 2 and 3.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

### NGAIN:

NGAIN is an integer variable and refers to the number of arbitrary gains which are input. If NGAIN = 3 then values for GAIN(1), GAIN(2) and GAIN(3) will be input. The maximum value of NGAIN is 10.

SPECIAL INSTRUCTIONS: If NGAIN has a value less than 10, punch the integer in column 3 of the data card. Otherwise, use columns 2 and 3.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

### TSTART:

TSTART is the time at which you wish the program to start calculating the equations of motion. Except for restarting, TSTART is usually set to zero.

SPECIAL INSTRUCTIONS: Punch the value of TSTART in columns 2 through 12.

UNITS: (seconds)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

### TSTOP:

TSTOP is the time at which you wish the program to stop calculating.

SPECIAL INSTRUCTIONS: Punch the value of TSTOP in columns 15 through 25.

UNITS: (seconds)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

# BODY 0 INPUT VARIABLES

AII(J,M,N):

$$[AII(J,M,N)] = [II_J] = \begin{bmatrix} AII(J,1,1) & AII(J,1,2) & AII(J,1,3) \\ AII(J,2,1) & AII(J,2,2) & AII(J,2,3) \\ AII(J,3,1) & AII(J,3,2) & AII(J,3,3) \end{bmatrix}$$

This array is the inertia matrix for the inner gimbal of the Jth control moment gyro aboard the stator. A maximum of six CMGs may be used. (i.e. J = 1,6) All CMGs are also constrained to be located at the center of mass on the stator, body 0. If the Jth CMG has one or two degrees of freedom, it will have an inner gimbal. (Refer to the write up on CMGs for further discussion.)

UNITS: (slug-ft<sup>2</sup>).

FORMAT: # 5006 = (1X, F11.5)

AIO(J,M,N):

$$[AIO(J,M,N)] = [IO_J] = \begin{bmatrix} AIO(J,1,1) & AIO(J,1,2) & AIO(J,1,3) \\ AIO(J,2,1) & AIO(J,2,2) & AIO(J,2,3) \\ AIO(J,3,1) & AIO(J,3,2) & AIO(J,3,3) \end{bmatrix}$$

This array is the inertia matrix for the outer gimbal of the Jth control moment gyro aboard the stator. A maximum of six CMGs may be used. (i.e. J = 1,6) All CMGs are constrained to be located at the center of mass on the stator, body 0. The Jth CMG will have an outer gimbal only if it has two degrees of freedom. (Refer to the write up on CMGs for further discussion.)

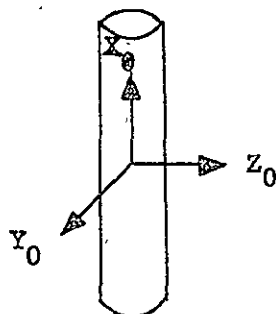
UNITS: (slug-ft<sup>2</sup>)

FORMAT: # 5006 = (1X, F11.5)

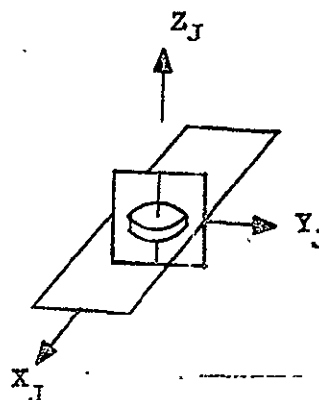
AOCJ(J,M,N):

$$[AOCJ(J,M,N)] = [O, C_J] = \begin{bmatrix} AOCJ(J,1,1) & AOCJ(J,1,2) & AOCJ(J,1,3) \\ AOCJ(J,2,1) & AOCJ(J,2,2) & AOCJ(J,2,3) \\ AOCJ(J,3,1) & AOCJ(J,3,2) & AOCJ(J,3,3) \end{bmatrix}$$

This array is the coordinate transformation matrix from the CMG null gimbal coordinate frame to the coordinate frame of body 0, the stator. (Refer to the coordinate transformation appendix.) For example, consider the two coordinate systems shown below:



Body 0 Frame



Jth Null Gimbal Frame

For the above situation:

$$[AOCJ(J,M,N)] = \begin{bmatrix} 0. & 0. & 1. \\ 1. & 0. & 0. \\ 0. & 1. & 0. \end{bmatrix}$$

UNITS: (None)

FORMAT: # 5006 = (1X, F11.5)

AOJ(M):

AOJ(1) is the distance between the jets of the pure couple producing the torque around the X axis of body 0.

AOJ(2) is the distance between the jets of the pure couple producing the torque around the Y axis of body 0.

AOJ(3) is the distance between the jets of the pure couple producing the torque around the Z axis of body 0.

Note: The variables CGAINO(1), CGAINO(2), and CGAINO(3) are also read on the same data cards as AOJ(1), AOJ(2), and AOJ(3). Punch the values of AOJ(1), AOJ(2), and AOJ(3) in columns 2 through 12 of the data cards.

UNITS: (feet)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

BODYOI(M,N):

$$[BODYOI(M,N)] = [I_0] = \begin{bmatrix} BODYOI(1,1) & BODYOI(1,2) & BODYOI(1,3) \\ BODYOI(2,1) & BODYOI(2,2) & BODYOI(2,3) \\ BODYOI(3,1) & BODYOI(3,2) & BODYOI(3,3) \end{bmatrix}$$

This array is the inertia matrix of body 0, the stator.

UNITS: (slug-ft<sup>2</sup>)

FORMAT: # 5004 = (1X, E11.4)

BOMASS:

BOMASS is the mass of body 0, the stator. BOMASS = m<sub>0</sub>

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)



CGAINO(M):

CGAINO(1) equals the control gain of all four reaction jets in the pure force couples producing torque around the X axis of body 0.

CGAINO(2) equals the control gain of all four reaction jets in the pure force couples producing torque around the Y axis of body 0.

CGAINO(3) equals the control gain of all four reaction jets in the pure force couples producing torque around the Z axis of body 0.

Note: The variables AOJ(1), AOJ(2), and AOJ(3) are also read in on the same data cards as CGAINO(1), CGAINO(2), and CGAINO(3). Punch the values of CGAINO(1), CGAINO(2), and CGAINO(3) in columns 15 through 25 of the data cards.

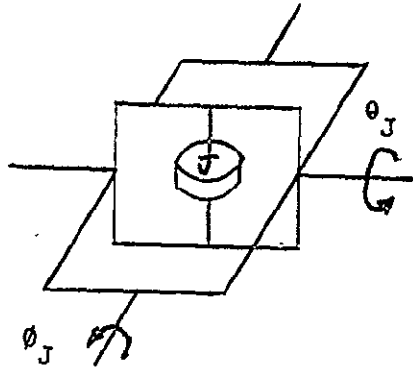
UNITS: (lb/radians/second)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

FEE(J):

$$FEE(J) = \theta_J$$

FEE(J) is the outer gimbal angle of a two degree of freedom control moment gyro as shown pictorially below:



The subscript J refers to the number assigned to the CMG. (Refer to the write up on CMGs for further discussion.)

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{start}$

FEED(J):

$$\text{FEED}(J) = \dot{\theta}_J$$

FEED(J) is the outer gimbal rate of a two degree of freedom control moment gyro. The subscript J refers to the number assigned to the CMG. (Refer to the write up on CMGs for further discussion.)

UNITS: (radians/second)

FORMAT: # 5006 = (1X, F11.5)

HW(J):

HW(J) is the angular momentum of the wheel associated with the Jth momentum device. (Refer to the write up on CMGs for further discussion.)

UNITS: (slug-ft<sup>2</sup>/second)

FORMAT: # 5004 = (1X, E11.4)

IDOF(J):

IDOF(J) = 0 implies the Jth controller aboard body 0 is a reaction wheel.

IDOF(J) = 1 implies the Jth controller aboard body 0 is a one degree of freedom control moment gyro.

IDOF(J) = 2 implies the Jth controller aboard body 0 is a two degree of freedom control moment gyro.

SPECIAL INSTRUCTIONS: Punch a 0, 1, or a 2 in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

NUMCMG:

NUMCMG is the number of controllers aboard body 0. A maximum of 6 controllers may be used.

SPECIAL INSTRUCTIONS: Punch the integer in column 3 of the data card.

UNITS: (none)

FORMAT: # 5000 = (1X, I2)

THATA(J):

THAT(J) is the gimbal angle of the Jth controller aboard body 0 assuming this controller is either a one or two degree of freedom control moment gyro. If it is a two degree of freedom CMG, then this variable refers to the inner gimbal angle. J may have a maximum value of 6.

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{start}$

THATAD(J):

THATAD(J) is the gimbal rate associated with THATA(J).

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{start}$

TIBOI(M,N):

$$[TIBOI(M,N)] = \begin{bmatrix} TIBOI(1,1) & TIBOI(1,2) & TIBOI(1,3) \\ TIBOI(2,1) & TIBOI(2,2) & TIBOI(2,3) \\ TIBOI(3,1) & TIBOI(3,2) & TIBOI(3,3) \end{bmatrix}$$

This array is the initial transformation matrix of the body 0 coordinate system to the inertial coordinate system. If initially body 0 is aligned with the inertial system, TIBOI(M,N) would be the identity matrix. Refer to the coordinate transformation appendix for further details.

UNITS: (none)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUES AT TIME =  $T_{start}$

WO(M):

WO(1), WO(2), and WO(3) are the X, Y, and Z components of the angular velocity vector of body 0.

UNITS: (radians per second)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

INITIAL VALUES AT TIME =  $T_{start}$

## BODY 1 INPUT VARIABLES

### AIJ(M):

AIJ(1) is the distance between the jets of the pure couple producing the torque around the X axis of body 1.

AIJ(2) is the distance between the jets of the pure couple producing the torque around the Y axis of body 1.

Note: The variables CGAIN1(1) and CGAIN1(2) are also read on the same data cards as AIJ(1) and AIJ(2).  
Punch the values of AIJ(1) and AIJ(2) in columns 2 through 12 of the data cards.

UNITS: (feet)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

### BODY1I(M,N):

$$[ \text{BODY1I}(M,N) ] = [ I_1 ] = \begin{bmatrix} \text{BODY1I}(1,1) & \text{BODY1I}(1,2) & \text{BODY1I}(1,3) \\ \text{BODY1I}(2,1) & \text{BODY1I}(2,2) & \text{BODY1I}(2,3) \\ \text{BODY1I}(3,1) & \text{BODY1I}(3,2) & \text{BODY1I}(3,3) \end{bmatrix}$$

This array is the inertia matrix for body 1, the rotor.

UNITS: (slug-ft<sup>2</sup>)

FORMAT: # 5004 = (1X, E11.4)

### BLMASS:

BLMASS is the mass of body 1, the rotor. BLMASS =  $m_1$

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

CGAIN1(M):

CGAIN1(1) equals the control gain of all four reaction jets in the pure force couples producing torque around the X axis of body 1.

CGAIN1(2) equals the control gain of all four reaction jets in the pure force couples producing torque around the Y axis of body 1.

Note: The variables ALJ(1) and ALJ(2) are also read in on the same data cards as CGAIN1(1) and CGAIN1(2). Punch the values of CGAIN1(1) and CGAIN1(2) in columns 15 through 25 of the data cards.

UNITS: (lb/radians/second)

FORMAT: # 5008 = (1X, E11.4, 2X, E11.4)

D01(M):

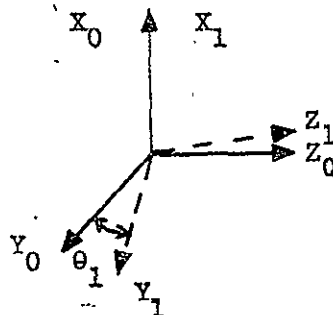
D01(1), D01(2), and D01(3) are the X, Y, and Z components of the vector from the center of mass of body 0 to the hinge line of body 1, the rotor. The vector is expressed in body 0 coordinates. D01(1) should in most cases be zero.

UNITS: (feet)     s

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

OMEGA1:

OMEGA1 is the initial relative angular velocity measure about the spin axis between bodies 0 and 1. Another definition of OMEGA1 can be visualized by referring to the sketch shown below showing the orthogonal coordinate systems located on bodies 0 and 1.



Implicit in this sketch is the hinge line between the stator and rotor is aligned parallel to both the  $\bar{X}_0$  and  $\bar{X}_1$  axes. Therefore, the orientation of the stator and the rotor differ only in a rotation  $\theta_1 = \text{THETA1}$  and  $\text{OMEGA1} = \dot{\theta}_1$ .

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

#### SP:

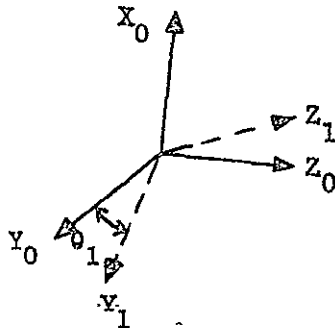
SP is the desired spin magnitude of body 1 relative to body 0.

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

#### THETA1:

THETA1 is the relative angular displacement measured about the spin axis, between bodies 0 and 1.



UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{\text{start}}$

## BODY 2 INPUT VARIABLES

### B2MASS:

B2MASS is the mass of body 2, the elevator.  $B2MASS = m_2$

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

### D12(M):

D12(1), D12(2) and D12(3) are the X, Y and Z components of a fixed vector locating the starting position of the movable mass, the elevator. The vector equation that describes the motion of the movable mass is  $\vec{l}_2 = \vec{d}_{12} + \vec{s}_2 s$ . Where  $\vec{s}_2$  is a unit vector which defines the direction in which the movable mass travels and  $s$  is a scalar prespecified function of time. For most cases  $s(t_0 = 0) = 0$  so that  $\vec{d}_{12}$  specifies the initial starting position of the movable mass. The elevator is known alternately as the movable mass or body 2. D12 is expressed in body 1 coordinates. For example, if the elevator were constrained to travel along the X axis, then  $\vec{d}_{12}$  could have the following values: D12(1) = 1., D12(2) = 0., D12(3) = 0.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

### S:

S is a scalar parameter used in defining the position of body 2. S defines the magnitude of displacement of body 2 from the zero position.

Note: Punch the value of S in columns 2 through 12.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

INITIAL VALUE AT TIME =  $T_{start}$



SDOT:

SDOT defines the magnitude of the velocity vector of body 2.

Note: Punch the value of SDOT in columns 15 through 25.

UNITS: (feet per second)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

INITIAL VALUE AT TIME =  $T_{start}$

S2(M):

S2(1), S2(2), and S2(3) are the X, Y, and Z components of a unit vector defining the direction of travel of body 2.  $\bar{s}_2$  is expressed in body 1 coordinates.

UNITS: (none)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

# BODY 3 INPUT VARIABLES

## B3MASS:

B3MASS is the mass of body 3, a pendulum.  $B3MASS = m_3$

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

## D13(M):

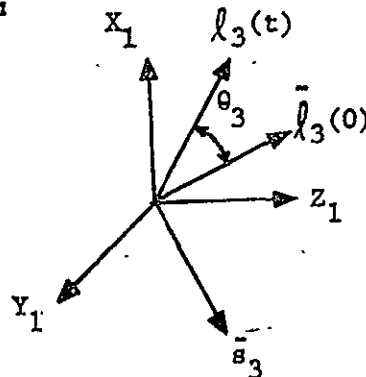
D13(1), D13(2), and D13(3) are the X, Y, and Z components of the vector from the center of mass of body 1 to the hinge line of body 3.  $\bar{D13}$  is expressed in body 1 coordinates.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

## OMEGA3:

OMEGA3 is the angular velocity of body 3 about the hinge line  $\bar{s}_3$ . OMEGA3 is also the time derivative of THETA3 when the datum for the angle THETA3 will be the  $\bar{Y}_1, \bar{Z}_1$  plane as illustrated below:



In other words,  $\bar{s}_3$  determines the positive direction of rotation by the right hand rule and the positive  $Y_1 - Z_1$  plane determines to starting position.

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{start}$

PEND3L:

PEND3L is the scalar distance from the hinge line,  $\bar{s}_2$ , to the center of mass of body 3. (i.e. the length of pendulum 3)

UNITS: (feet)

FORMAT: # 5006 = (1X, F11.5)

S3(M):

S3(1), S3(2), and S3(3) are the X, Y, and Z components of a unit vector which defines the hinge line of body 3.  $\bar{s}_3$  is expressed in body 1 coordinates. S3(1) must always be zero.

UNITS: (none)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

THETA3:

THETA3 is the angle between pendulum 3 and the Y, Z, plane. The axis about which THETA3 rotates is the hinge line  $\bar{s}_2$ . For an explanation of the THETA3 datum refer to the discussion of OMEGA3.

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{start}$

#### BODY 4 INPUT VARIABLES

##### B4MASS:

B4MASS is the mass of body 4, a pendulum.  $B4MASS = m_4$

UNITS: (slugs)

FORMAT: # 5004 = (1X, E11.4)

##### D14(M):

D14(1), D14(2), and D14(3) are the X, Y, and Z components of the vector from the center of mass of body 1 to the hinge line of body 4.

D14 is expressed in body 1 coordinates.

UNITS: (feet)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

##### OMEGA4:

OMEGA4 is the angular velocity of body 4 about the hinge line  $\bar{s}_4$ . OMEGA4 is also the time derivative of THETA4 where the datum for the angle THETA4 is the same as THETA3. (See OMEGA3)

UNITS: (radians per second)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{start}$

##### PEND4L:

PEND4L is the scalar distance from the hinge line,  $\bar{s}_4$ , to the center of mass of body 4. (i.e. the length of pendulum 4)

UNITS: (feet)

FORMAT: # 5006 = (1X, F11.5)

S4(M):

S4(1), S4(2), and S4(3) are the X, Y, and Z components of a unit vector which defines the hinge line of body 4.  $\vec{s}_4$  is expressed in body 1 coordinates. S4(1) must always be zero.

UNITS: (none)

FORMAT: # 5002 = (1X, 3(F11.5, 2X))

THETA4:

THETA4 is the angle between pendulum 4 and the Y, Z, plane. The axis about which THETA4 rotates is the hinge line  $s_4$ . The datum for THETA4 is the same as for THETA3.

UNITS: (radians)

FORMAT: # 5006 = (1X, F11.5)

INITIAL VALUE AT TIME =  $T_{start}$

## APPENDIX B, COORDINATE TRANSFORMATIONS

The following pages contain a pictorial guide to aid the user in computing the initial transformation matrix from one right hand orthogonal coordinate system to another. The transformation matrix from coordinate system B to coordinate A shall be denoted  $[A,B]$ .

$$\text{Mathematically: } \begin{bmatrix} X_A \\ Y_A \\ Z_A \end{bmatrix} = [A,B] \begin{bmatrix} X_B \\ Y_B \\ Z_B \end{bmatrix}$$

$$\text{i.e. } X_A = AB(1,1) * X_B + AB(1,2) * Y_B + AB(1,3) * Z_B$$

$$Y_A = AB(2,1) * X_B + AB(2,2) * Y_B + AB(2,3) * Z_B$$

$$Z_A = AB(3,1) * X_B + AB(3,2) * Y_B + AB(3,3) * Z_B$$

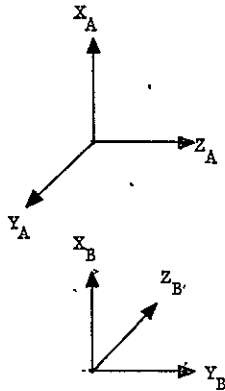
For simplicity, the coordinate systems in the following illustrations are orthogonal to each other in one way or another. i.e. There are not small offsetting rotations. Hence, the components of  $A,B$  may assume only certain values. The components may be  $\pm 1.$ ,  $0.$ ,  $\pm \sin\emptyset$ ,  $\pm \cos\emptyset$ ,  $\pm \sin\theta$ ,  $\pm \cos\theta$ ,  $\pm \sin\psi$ , or  $\pm \cos\psi$  where  $\emptyset$ ,  $\theta$ , and  $\psi$  are angles of rotation about the  $X$ ,  $Y$ ,  $Z$  axes respectively.

# FLOW CHART & BLOCK DIAGRAM

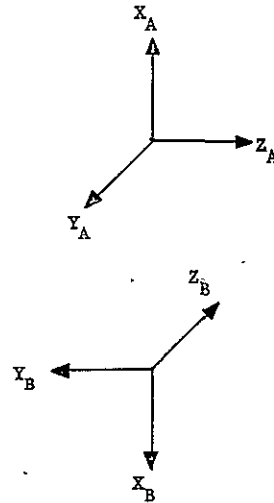
FORM DEN 1103-01 (4-64)

Application \_\_\_\_\_ Date \_\_\_\_\_ Page \_\_\_\_\_ of \_\_\_\_\_

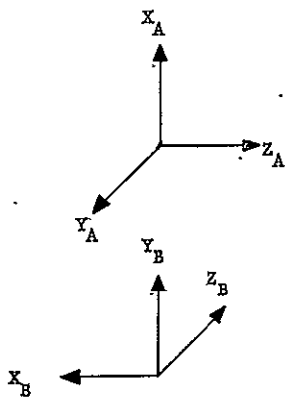
Procedure \_\_\_\_\_ Drawn By \_\_\_\_\_



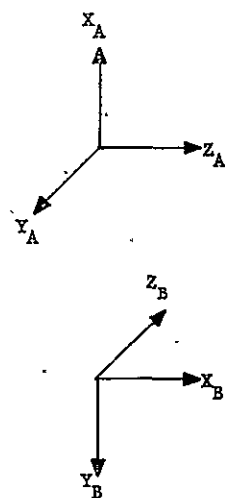
$$[A, B] = \begin{bmatrix} 1. & 0. & 0. \\ 0. & 0. & -1. \\ 0. & 1. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} -1. & 0. & 0. \\ 0. & 0. & -1. \\ 0. & -1. & 0. \end{bmatrix}$$



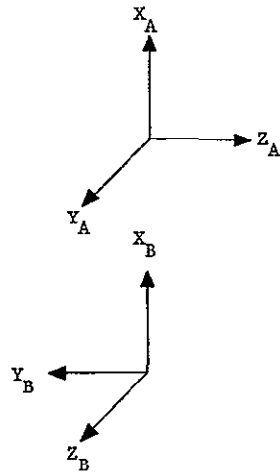
$$[A, B] = \begin{bmatrix} 0. & 1. & 0. \\ 0. & 0. & -1. \\ -1. & 0. & 0. \end{bmatrix}$$



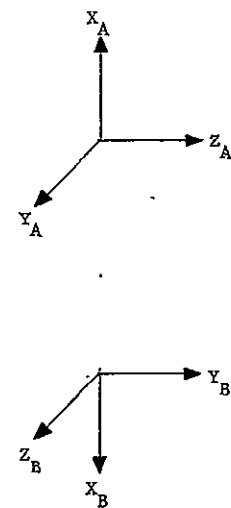
$$[A, B] = \begin{bmatrix} 0. & -1. & 0. \\ 0. & 0. & -1. \\ 1. & 0. & 0. \end{bmatrix}$$

# FLOW-CHART & BLOCK DIAGRAM

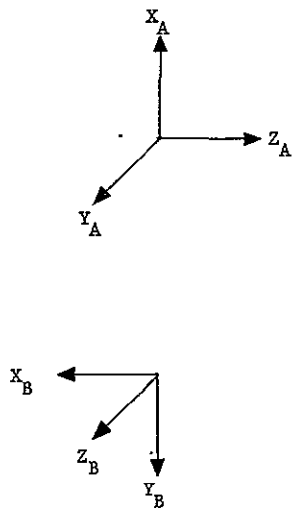
Application \_\_\_\_\_ Date \_\_\_\_\_ Page \_\_\_\_\_ of \_\_\_\_\_  
 Procedure \_\_\_\_\_ Drawn By \_\_\_\_\_



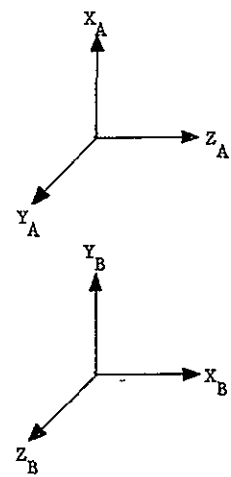
$$[A, B] = \begin{bmatrix} 1. & 0. & 0. \\ 0. & 0. & 1. \\ 0. & -1. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} -1. & 0. & 0. \\ 0. & 0. & 1. \\ 0. & 1. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & -1. & 0. \\ 0. & 0. & 1. \\ -1. & 0. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 1. & 0. \\ 0. & 0. & 1. \\ 1. & 0. & 0. \end{bmatrix}$$

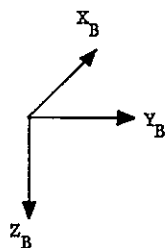
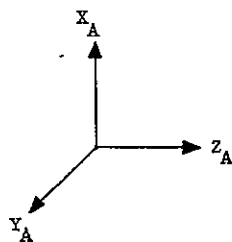


# FLOW CHART & BLOCK DIAGRAM

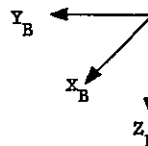
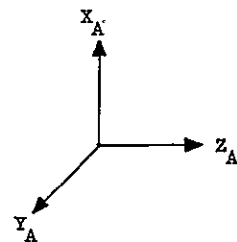
FORM DEN 1103-01 (1-6-1)

Application \_\_\_\_\_ Date \_\_\_\_\_ Page \_\_\_\_\_ of \_\_\_\_\_

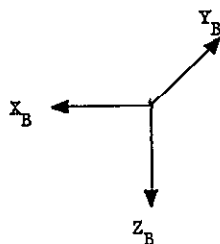
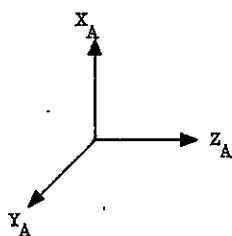
Procedure \_\_\_\_\_ Drawn By \_\_\_\_\_



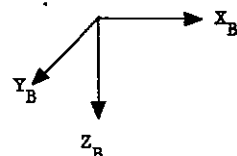
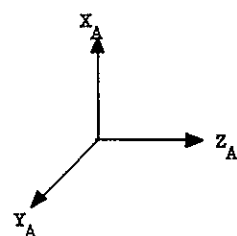
$$[A, B] = \begin{bmatrix} 0. & 0. & -1. \\ -1. & 0. & 0. \\ 0. & 1. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 0. & -1. \\ 1. & 0. & 0. \\ 0. & -1. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 0. & -1. \\ 0. & -1. & 0. \\ -1. & 0. & 0. \end{bmatrix}$$

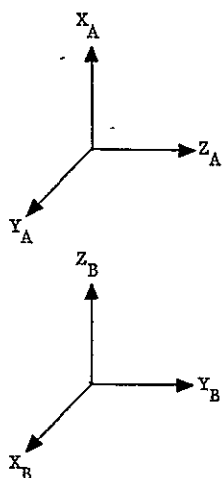


$$[A, B] = \begin{bmatrix} 0. & 0. & -1. \\ 0. & 1. & 0. \\ 1. & 0. & 0. \end{bmatrix}$$

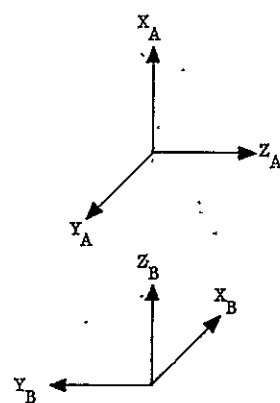
# FLOW CHART & BLOCK DIAGRAM

Application \_\_\_\_\_ Date \_\_\_\_\_ Page \_\_\_\_\_ of \_\_\_\_\_

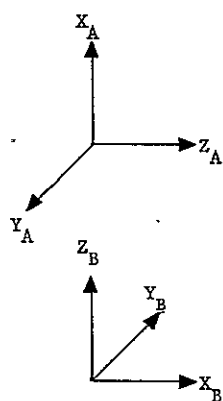
Procedure \_\_\_\_\_ Drawn By \_\_\_\_\_



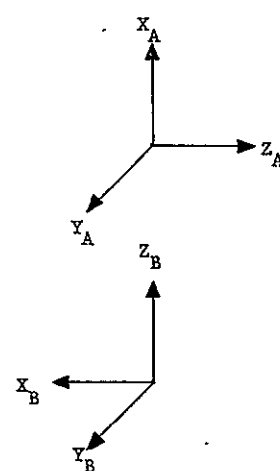
$$[A, B] = \begin{bmatrix} 0. & 0. & 1. \\ 1. & 0. & 0. \\ 0. & 1. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 0. & 1. \\ -1. & 0. & 0. \\ 0. & -1. & 0. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 0. & 1. \\ 0. & -1. & 0. \\ 1. & 0. & 0. \end{bmatrix}$$



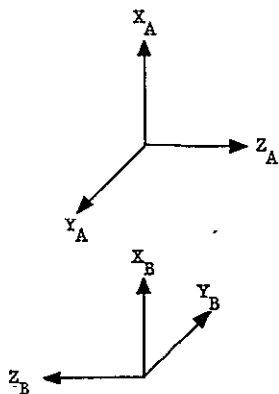
$$[A, B] = \begin{bmatrix} 0. & 0. & 1. \\ 0. & 1. & 0. \\ -1. & 0. & 0. \end{bmatrix}$$

# FLOW CHART & BLOCK DIAGRAM

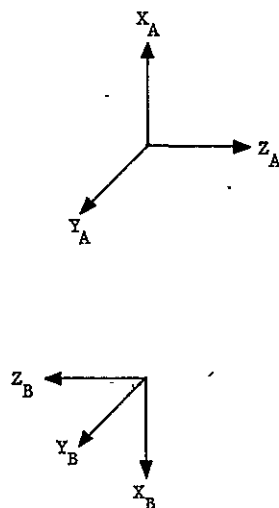
FORM DEN 1103-D1 (2-62)

Application \_\_\_\_\_ Date \_\_\_\_\_ Page \_\_\_\_\_ of \_\_\_\_\_

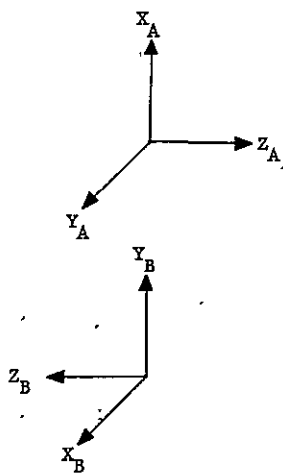
Procedure \_\_\_\_\_ Drawn By \_\_\_\_\_



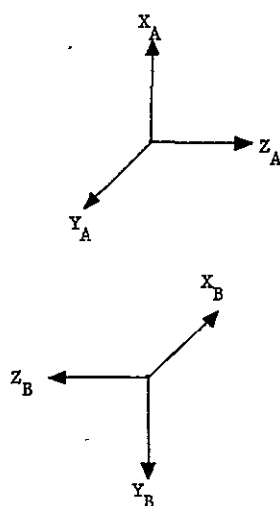
$$[A, B] = \begin{bmatrix} 1. & 0. & 0. \\ 0. & -1. & 0. \\ 0. & 0. & -1. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} -1. & 0. & 0. \\ 0. & 1. & 0. \\ 0. & 0. & -1. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 1. & 0. \\ 1. & 0. & 0. \\ 0. & 0. & -1. \end{bmatrix}$$

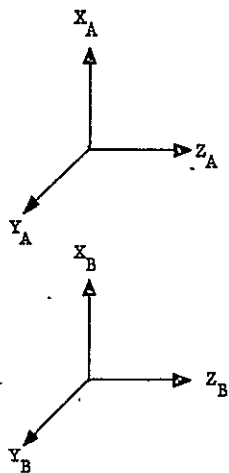


$$[A, B] = \begin{bmatrix} 0. & -1. & 0. \\ -1. & 0. & 0. \\ 0. & 0. & -1. \end{bmatrix}$$

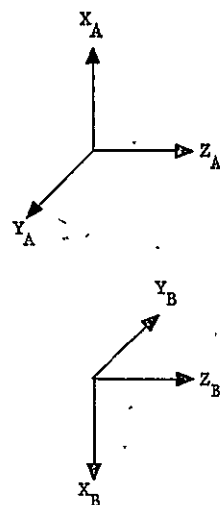
# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-D1 (4-64)

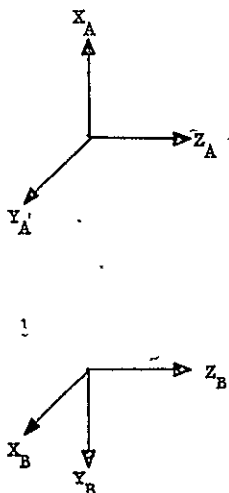
Application \_\_\_\_\_ Date \_\_\_\_\_ Page \_\_\_\_\_ of \_\_\_\_\_  
 Procedure \_\_\_\_\_ Drawn By \_\_\_\_\_



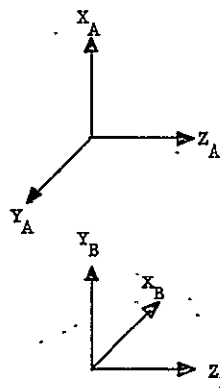
$$[A, B] = \begin{bmatrix} 1. & 0. & 0. \\ 0. & 1. & 0. \\ 0. & 0. & 1. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} -1. & 0. & 0. \\ 0. & -1. & 0. \\ 0. & 0. & 1. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & -1. & 0. \\ 1. & 0. & 0. \\ 0. & 0. & 1. \end{bmatrix}$$



$$[A, B] = \begin{bmatrix} 0. & 1. & 0. \\ -1. & 0. & 0. \\ 0. & 0. & 1. \end{bmatrix}$$

CHARGE. 03 MD246 2070000603744524 8947 56665

P.HENDRICKS2284

MAP.  
 RUN24(P,,,,,37777,,1)  
 LGO.  
 EXIT.  
 DMP.  
 DMP(0,150000)

PROGRAM MD246(INPUT,OUTPUT,TAPES=INPUT,TAPE=OUTPUT,FILMPL)

C  
 C  
 C  
 C

```

*****
COMMON      A(3)          9      AE(5)          9      AED(5)          9      COMMC
*            AF0UR(2)      9      AII(6,3,3)      9      COMMC
*            AIO(6,3,3)    9      AJ1(3)          9      ALT          9      COMMC
*            AOCJ(6,3,3)   9      AOJ(3)          9      AONE(7)       9      COMMC
*            ATCPT2(3,3)   9      ATHREE(5)      9      ATWO(4)       9      COMMC
*            A1(3,3)       9      A1J(2)          9      COMMC
COMMON      BDMASS        9      BFOUR(2)        9      BMOM          9      COMMC
*            BODYOI(3,3)   9      BODYOI(3,3)    9      BODY11(3,3)   9      COMMC
*            BOMASS        9      BONE(7)         9      BTHREE(5)     9      COMMC
*            BTWO(4)       9      B1MASS          9      B2MASS         9      COMMC
*            B3MASS        9      B4MASS          9      COMMC
COMMON      CA(3)         9      CB(3)           9      CGAIN0(3)     9      COMMC
*            CGAIN1(2)     9      COMMC
*            COSFEJ        9      COSTIJ          9      COSTT0        9      COMMC
*            COSTT1        9      COSTT3          9      COSTT4        9      COMMC
*            CO2T          9      CP1             9      CP2           9      COMMC
*            CST           9      C1              9      COMMC
COMMON      DB(3)         9      DD01(3)         9      COMMC
*            DELTAT        9      D01(3)          9      D01D0T(3)     9      COMMC
*            DTI(3)        9      COMMC
*            DTIME         9      D12(3)          9      D13(3)         9      COMMC
*            D13D0T(3)     9      D13YCS          9      D13YSN         9      COMMC
*            D13ZCS        9      D13ZSN          9      D14(3)         9      COMMC
*            D14D0T(3)     9      D14YCS          9      D14YSN         9      COMMC
*            D14ZCS        9      D14ZSN          9      COMMC
COMMON      EEE(3,3)      9      EEJ(3,3)        9      EL2(3)         9      COMMC
*            EL2D0T(3)     9      EL2YCS          9      EL2YSN         9      COMMC
*            EL2ZCS        9      EL2ZSN          9      ELB(3)         9      COMMC
*            EL3D0T(3)     9      EL3YCS          9      ELBYSN         9      COMMC
*            EL3ZCS        9      EL3ZSN          9      EL4(3)         9      COMMC
*            EL4D0T(3)     9      EL4YCS          9      EL4YSN         9      COMMC
*            EL4ZCS        9      EL4ZSN          9      EMI(6,6)      9      COMMC
COMMON      FAT(8)        9      COMMC
*            FEE(6)        9      FEED(6)         9      FFF(3)         9      COMMC
*            FFJ(3)        9      FLAG1           9      FLAG2          9      COMMC
*            FLAG3        9      FLAG4           9      FN             9      COMMC
*            FO(3)         9      FO1(3)          9      FO2(3)         9      COMMC
*            FO3(3)        9      F1(3)           9      F11(3)         9      COMMC
*            FPT(5)        9      COMMC
*            F12(3)        9      F13(3)          9      COMMC
COMMON      GAIN(10)      9      G3              9      COMMC
*            G3D0T        9      G4              9      G4D0T          9      COMMC
COMMON      H(3)          9      HCMG(3)         9      HDOT(3)        9      COMMC
*            HI(3)         9      HO(3)           9      HW(6)          9      COMMC
*            H1(3)         9      H1PD0T(3)       9      H1PRIM(3)     9      COMMC

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* COMMON	H3PRIM(3)	,	H4PRIM(3)	,	ICFB	, COMM
	IB2F	,	ICFA	,	IDOCK	, COMM
	ICFC	,	ICFD	,		, COMM
	IDOF(6)	,				, COMM
	IGRAVF	,	IPNDLM	,	IPNTCK	, COMM
	IPRINT	,	IPROPF			, COMM
* COMMON	NCASE	,	NCHECK	,	NDECK	, COMM
	NGAIN	,	NUMCMG			, COMM
* COMMON	OMEGA1	,	OMEGA3	,	OMEGA4	, COMM
* COMMON	PEND3L	,	PEND4L			, COMM
* COMMON	Q(4,4)					, COMM
	R	,	R0(3)	,	R1(3)	, COMM
	R1DOT(3)	,	R1YCS	,	R1YSN	, COMM
	R1ZCS	,	R1ZSN	,	R2(3)	, COMM
	R2DOT(3)	,	R2YCS	,	R2YSN	, COMM
	R2ZCS	,	R2ZSN	,	R3(3)	, COMM
	R3DOT(3)	,	R3YCS	,	R3YSN	, COMM
	R3ZCS	,	R3ZSN	,	R4(3)	, COMM
	R4DOT(3)	,	R4YCS	,	R4YSN	, COMM
	R4ZCS	,	R4ZSN			, COMM
* COMMON	S	,	SDOT	,	SINFEJ	, COMM
	SINTTJ	,	SINTT0	,	SINTT1	, COMM
	SINTT2	,	SINTT3	,	SINTT4	, COMM
	SP	,	SUM1	,	SUM2	, COMM
	SUM3	,	S2(3)	,	S3(3)	, COMM
	S4(3)					, COMM
* COMMON	T(3,3)	,	TC(3,3)	,	TEMP1(3)	, COMM
	TEMP2(3)	,				, COMM
	TEMP3(3)	,	TEMP4(3)	,	TEMP5(3,3)	, COMM
	TEMP6(3,3)	,	TEMP7(3,3)	,	TEMP8(3,3)	, COMM
	TEMP9(3,3)	,	TEMP10(3,3)	,	TEMP11(3,3)	, COMM
	TEMP12(3,3)	,	TEMP13(3,3)	,	TEMP14(3,3)	, COMM
	TEMP15(3,3)	,	TERM1(3)	,	TERM2(3)	, COMM
	TFRICT	,	THATA(6)	,	THATAAD(6)	, COMM
	THETA1	,	THETA3	,	THETA4	, COMM
	THETO	,	TIB0(3,3)	,	TIB0I(3,3)	, COMM
	TIME	,	TJ	,	TJ1(10)	, COMM
	TJ2(10)	,	TJ3(10)	,	TJ4(10)	, COMM
	TMOTOR	,				, COMM
	TOEF(3)	,	TOTMAS	,	T01	, COMM
	TQOG(3)	,	TQOP(3)	,	TQ1G(3)	, COMM
	TQ1P(3)	,	TSTART	,	TSTOP	, COMM
	TT1DOT	,	TT3DOT	,	TT4DOT	, COMM
	T1EF(3)	,	T13	,	T14	, COMM
* COMMON	V(3)					, COMM
* COMMON	W0(3)	,	WS	,	W1(3)	, COMM
	W3(3)	,	W4(3)			, COMM
* COMMON	X(6,7)	,	XC	,	XCDOT	, COMM
	XMU					, COMM

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 \*  
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THIS IS THE ENTRY POINT TO THE RUN CONTROL MODULE.  
 THE FUNCTION OF THIS MODULE IS TO MAKE THE DECISION TO STOP ALL  
 CALCULATIONS AND EXIT THE PROGRAM OR CONTINUE TO THE INPUT MODULE  
 AND READ IN THE DATA FOR THE NEXT CASE.

NCHECK = 0

C	READ IN THE NUMBER OF DATA DECKS PRESENT AT RUN TIME.	RCON
	READ (5,5000) NDECK	RCON
C	PRINT NDECK ON A NEW SHEET OF PAPER.	RCON
	WRITE(6,6000) NDECK	RCON
C	THE PROGRAM RETURNS TO THE FOLLOWING STATEMENT NUMBER AFTER EACH	RCON
C	DATA DECK HAS BEEN COMPLETELY PROCESSED.	RCON
10	NCHECK = NCHECK + 1	RCON
	IF (NDECK .GE. NCHECK) GO TO 20	RCON
	STOP	RCON
20	CONTINUE	RCON
C	*****	RCON
C	*	
C	*	
C	*****	
C	THIS IS THE ENTRY POINT TO THE INPUT MODULE.	INPUT
C	THE FUNCTION OF THIS MODULE IS TO READ IN ALL DATA PERTAINING TO	INPUT
C	THE NEXT CASE. AFTER EACH VARIABLE HAS BEEN READ IN, IT WILL BE	INPUT
C	PRINTED OUT TO INSURE PROPER CONVERSION AND TO RETAIN A RECORD OF	INPUT
C	THE INPUT DATA.	INPUT
C	DO 25 M=1,10	INPUT
	GAIN(M) = 0.	INPUT
25	CONTINUE	INPUT
	WRITE(6,6500) NCHECK	INPUT
C	READ THE PENDULUM FLAG.	INPUT
	READ (5,5000) IPNDLM	INPUT
	WRITE(6,6082) IPNDLM	INPUT
C	READ THE PRINT FLAG. (I.E. PRINT EVERY IPRINT TIME POINT.)	INPUT
	READ (5,5000) IPRINT	INPUT
	WRITE(6,6544) IPRINT	INPUT
C	READ THE STARTING TIME, STOPING TIME, AND DELTAT.	INPUT
	READ (5,5002) TSTART,TSTOP,DELTAT	INPUT
	WRITE(6,6002) TSTART,TSTOP,DELTAT	INPUT
C	READ THE ORBIT ALTITUDE.	INPUT
	READ (5,5004) ALT	INPUT
	WRITE(6,6004) ALT	INPUT
C	READ THE TRANSFORMATION FROM THE BODY 0 FRAME TO THE I FRAME.	INPUT
	DO 30 M=1,3	INPUT
	DO 30 N=1,3	INPUT
	READ (5,5006) TIBOI(M,N)	INPUT
30	CONTINUE	INPUT
	DO 35 M=1,3	INPUT
	WRITE(6,6006) M,TIBOI(M,1),M,TIBOI(M,2),M,TIBOI(M,3)	INPUT
35	CONTINUE	INPUT
C	READ BODY 0 ANGULAR RATES.	INPUT
	READ (5,5002) WO(1),WO(2),WO(3)	INPUT
	WRITE(6,6008) WO(1),WO(2),WO(3)	INPUT
C	READ THE MASS OF BODY 0.	INPUT
	READ (5,5004) BOMASS	INPUT
	J = 0	INPUT
	WRITE(6,6010) J,BOMASS	INPUT
C	READ THE INERTIA MATRIX FOR BODY 0.	INPUT
	DO 40 M=1,3	INPUT
	DO 40 N=1,3	INPUT
	READ (5,5004) BODYOI(M,N)	INPUT
40	CONTINUE	INPUT
	DO 45 M=1,3	INPUT
	WRITE(6,6012) M,BODYOI(M,1),M,BODYOI(M,2),M,BODYOI(M,3)	INPUT
45	CONTINUE	INPUT

C	READ THE NUMBER OF CONTROL MOMENT GYROs ABOARD BODY 0.	INPUT
	READ (5,5000) NUMCMG	INPUT
	WRITE(6,6014) NUMCMG	INPUT
	IF (NUMCMG .EQ. 0) GO TO 120	INPUT
	DO 110 J=1,NUMCMG	INPUT
C	READ THE DEGREE OF FREEDOM OF THE JTH CMG.	INPUT
	READ (5,5000) IDOF(J)	INPUT
	IF (IDOF(J) .NE. 0) GO TO 50	INPUT
	WRITE(6,6016) J	INPUT
	GO TO 70	INPUT
50	IF (IDOF(J) .NE. 1) GO TO 60	INPUT
	WRITE(6,6018) J	INPUT
	GO TO 70	INPUT
60	WRITE(6,6020) J	INPUT
70	CONTINUE	INPUT
C	READ THE ANGULAR MOMENTUM OF THE JTH CMG.	INPUT
	READ (5,5004) HW(J)	INPUT
	WRITE(6,6022) J,HW(J)	INPUT
C	READ THE TRANSFORMATION FROM THE JTH NULL GIMBAL FRAME TO BODY 0	INPUT
C	FRAME.	INPUT
	DO 80 M=1,3	INPUT
	DO 80 N=1,3	INPUT
	READ (5,5006) AOCJ(J,M,N)	INPUT
80	CONTINUE	INPUT
	DO 85 M=1,3	INPUT
	WRITE(6,6024) J,M,AOCJ(J,M,1),J,M,AOCJ(J,M,2),J,M,AOCJ(J,M,3)	INPUT
85	CONTINUE	INPUT
	IF (IDOF(J) .EQ. 0) GO TO 110	INPUT
C	READ THE INERTIA MATRIX FOR THE JTH INNER GIMBAL.	INPUT
	DO 90 M=1,3	INPUT
	DO 90 N=1,3	INPUT
	READ (5,5006) AII(J,M,N)	INPUT
90	CONTINUE	INPUT
	DO 95 M=1,3	INPUT
	WRITE(6,6026) J,M,AII(J,M,1),J,M,AII(J,M,2),J,M,AII(J,M,3)	INPUT
95	CONTINUE	INPUT
C	READ THE INNER GIMBAL ANGLE AND RATE OF THE JTH CMG.	INPUT
	READ (5,5006) THATA(J)	INPUT
	READ (5,5006) THATAD(J)	INPUT
	WRITE(6,6028) J,THATA(J),J,THATAD(J)	INPUT
	FEE(J) = 0.	INPUT
	FEED(J) = 0.	INPUT
	IF (IDOF(J) .EQ. 1) GO TO 110	INPUT
C	READ THE INERTIA MATRIX FOR THE JTH OUTER GIMBAL.	INPUT
	DO 100 M=1,3	INPUT
	DO 100 N=1,3	INPUT
	READ (5,5006) AIO(J,M,N)	INPUT
100	CONTINUE	INPUT
	DO 105 M=1,3	INPUT
	WRITE(6,6030) J,M,AIO(J,M,1),J,M,AIO(J,M,2),J,M,AIO(J,M,3)	INPUT
105	CONTINUE	INPUT
C	READ THE OUTER GIMBAL ANGLE AND RATE OF THE JTH CMG.	INPUT
	READ (5,5006) FEE(J)	INPUT
	READ (5,5006) FEED(J)	INPUT
	WRITE(6,6032) J,FEE(J),J,FEED(J)	INPUT
110	CONTINUE	INPUT
120	CONTINUE	INPUT
C	READ THE PROPULSION FLAG.	INPUT
	READ (5,5000) IPROPF	INPUT
	WRITE(6,6072) IPROPF	INPUT
	IF (IPROPF .EQ. 0) GO TO 140	INPUT
	READ (5,5000) IATTIF	INPUT



	WRITE(6,6562) IATTIF	INPUT
	IF (IATTIF.EQ. 0) GO TO 125	INPUT
	READ (5,5002) CA(1),CA(2),CA(3)	INPUT
	WRITE(6,6564) CA(1),CA(2),CA(3)	INPUT
125	CONTINUE	INPUT
	DO 130 J=1,3	INPUT
	READ (5,5008) AOJ(J), CGAINO(J)	INPUT
	WRITE(6,6074) J,AOJ(J),J,CGAINO(J)	INPUT
130	CONTINUE	INPUT
140	CONTINUE	INPUT
C	READ IN VARIABLES RELATED TO BODY 1.	INPUT
C	READ THE MASS OF BODY 1.	INPUT
	READ (5,5004) B1MASS	INPUT
	J = 1	INPUT
	WRITE(6,6010) J,B1MASS	INPUT
C	READ THE INERTIA MATRIX FOR BODY 1.	INPUT
	DO 150 M=1,3	INPUT
	DO 150 N=1,3	INPUT
	READ (5,5004) BODY1I(M,N)	INPUT
150	CONTINUE	INPUT
	DO 153 M=1,3	INPUT
	WRITE(6,6040) M,BODY1I(M,1),M,BODY1I(M,2),M,BODY1I(M,3)	INPUT
153	CONTINUE	INPUT
C	READ THE PRIMARY GIMBAL ANGLE AND RATE OF BODY 1 W.R.T. BODY 0.	INPUT
	READ (5,5006) THETA1	INPUT
	READ (5,5006) OMEGA1	INPUT
	WRITE(6,6042) THETA1,OMEGA1	INPUT
C	READ THE VECTOR FROM THE CM OF BODY 0 TO THE HINGE POINT BETWEEN	INPUT
C	BODY 0 AND BODY 1. (BODY 0 COORDINATES)	INPUT
	READ (5,5002) D01(1),D01(2),D01(3)	INPUT
	WRITE(6,6044) D01(1),D01(2),D01(3)	INPUT
C	READ THE BODY 2 FLAG. (I.E. THE ELEVATOR FLAG.)	INPUT
	READ (5,5000) IB2F	INPUT
	WRITE(6,6546) IB2F	INPUT
	IF (IB2F.EQ. 0) GO TO 155	INPUT
C	READ THE MASS OF THE ELEVATOR.	INPUT
	READ (5,5004) B2MASS	INPUT
	J = 2	INPUT
	WRITE(6,6010) J,B2MASS	INPUT
	READ (5,5002) D12(1),D12(2),D12(3)	INPUT
	WRITE(6,6535) D12(1),D12(2),D12(3)	INPUT
	READ (5,5002) S2(1), S2(2), S2(3)	INPUT
	J = 2	INPUT
	WRITE(6,6052) J,S2(1),J,S2(2),J,S2(3)	INPUT
C	READ THE POSITION AND VELOCITY OF THE ELEVATOR.	INPUT
	READ (5,5002) S,SDOT	INPUT
	WRITE(6,6548) S,SDOT	INPUT
	GO TO 157	INPUT
155	B2MASS = 0.	INPUT
	D12(1) = 0.	INPUT
	D12(2) = 0.	INPUT
	D12(3) = 0.	INPUT
	S2(1) = 0.	INPUT
	S2(2) = 0.	INPUT
	S2(3) = 0.	INPUT
	SDOT = 0.	INPUT
	S = 0.	INPUT
157	CONTINUE	INPUT
	IF (IPROPF.EQ. 0) GO TO 170	INPUT
	DO 160 J=1,2	INPUT
	READ (5,5008) AJ(J), CGAIN1(J)	INPUT
	WRITE(6,6076) J,AJ(J),J,CGAIN1(J)	INPUT

[illegible]

	D14(2) = 0.	INPUT
	D14(3) = 0.	INPUT
	S4(1) = 0.	INPUT
	S4(2) = 0.	INPUT
	S4(3) = 0.	INPUT
	PEND4L = 0.	INPUT
	THETA4 = 0.	INPUT
	OMEGA4 = 0.	INPUT
174	CONTINUE	INPUT
	READ (5,5006) SP	INPUT
	WRITE(6,6080) SP	INPUT
	READ (5,5000) NGAIN	INPUT
	WRITE(6,6570) NGAIN	INPUT
	IF (NGAIN .EQ. 0) GO TO 176	INPUT
	DO 175 J=1,NGAIN	INPUT
	READ (5,5004) GAIN(J)	INPUT
	WRITE(6,6572) J,GAIN(J)	INPUT
175	CONTINUE	INPUT
176	CONTINUE	INPUT
C	READ THE GRAVITY GRADIENT FLAG.	INPUT
	READ (5,5000) IGHAVF	INPUT
	WRITE(6,6078) IGRAVF	INPUT
C	READ THE DOCKING FLAG. IDOCK = 1 IMPLIES A DOCKING WILL OCCUR.	INPUT
	READ (5,5000) IDOCK	INPUT
	WRITE(6,6068) IDOCK	INPUT
	IF (IDOCK .EQ. 0) GO TO 180	INPUT
C	READ THE TIME OF DOCKING.	INPUT
	READ (5,5006) DTIME	INPUT
	WRITE(6,6070) DTIME	INPUT
	DTMIN = DTIME - DELTAT/10.	INPUT
	DTMAX = DTIME + DELTAT/10.	INPUT
	DCHMIN = DTIME - 1.1*DELTAT	INPUT
	UCHMAX = DTIME + 0.9*DELTAT	INPUT
	READ (5,5004) BDMASS	INPUT
	WRITE(6,6574) BDMASS	INPUT
	DO 177 M=1,3	INPUT
	DO 177 N=1,3	INPUT
	READ (5,5004) BODYDI(M,N)	INPUT
177	CONTINUE	INPUT
	DO 178 M=1,3	INPUT
	WRITE(6,6576) M,BODYDI(M,1),M,BODYDI(M,2),M,BODYDI(M,3)	INPUT
178	CONTINUE	INPUT
	READ (5,5002) DTI(1),DTI(2),DTI(3)	INPUT
	WRITE(6,6578) DTI(1),DTI(2),DTI(3)	INPUT
	READ (5,5002) DDO1(1),DDO1(2),DDO1(3)	INPUT
	WRITE(6,6586) DDO1(1),DDO1(2),DDO1(3)	INPUT
180	CONTINUE	INPUT
C	*****	INPUT
C	*	
C	*	
C	*	
C	*****	
C	INIT	
C	THIS IS THE ENTRY POINT TO THE INITIALIZATION BLOCK.	INIT
C	ALL INITIAL CALCULATIONS ARE PERFORMED ONE TIME ONLY FOR EACH CASE	INIT
C	INIT	
C	CALCULATE THE TOTAL MASS OF THE CONFIGURATION.	INIT
C	TOTMAS = BOMASS + B1MASS + B2MASS + B3MASS + B4MASS	INIT
C	ICFA = 0	INIT
C	ICFB = 0	INIT
C	ICFC = 0	INIT







C  
C  
C  
C

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THIS IS THE ENTRY POINT TO THE QUATERNION BLOCK.

```

Q(1,1) = 0.
Q(1,2) = -0.5*W0(1)
Q(1,3) = -0.5*W0(2)
Q(1,4) = -0.5*W0(3)
Q(2,1) = -Q(1,2)
Q(2,2) = 0.
Q(2,3) = -Q(1,4)
Q(2,4) = Q(1,3)
Q(3,1) = -Q(1,3)
Q(3,2) = Q(1,4)
Q(3,3) = 0.
Q(3,4) = -Q(1,2)
Q(4,1) = -Q(1,4)
Q(4,2) = -Q(1,3)
Q(4,3) = Q(1,2)
Q(4,4) = 0.
AED(2) = Q(1,1)*AE(2) + Q(1,2)*AE(3) + Q(1,3)*AE(4) + Q(1,4)*AE(5)
AED(3) = Q(2,1)*AE(2) + Q(2,2)*AE(3) + Q(2,3)*AE(4) + Q(2,4)*AE(5)
AED(4) = Q(3,1)*AE(2) + Q(3,2)*AE(3) + Q(3,3)*AE(4) + Q(3,4)*AE(5)
AED(5) = Q(4,1)*AE(2) + Q(4,2)*AE(3) + Q(4,3)*AE(4) + Q(4,4)*AE(5)
SET UP MATRICES USED BY THE INTEGRATION SUBROUTINE
ATHREE(1) = TIME
BTHREE(1) = DELTAT
BTHREE(2) = AED(2)
BTHREE(3) = AED(3)
BTHREE(4) = AED(4)
BTHREE(5) = AED(5)
CALL FOMS(ATHREE,BTHREE,5,FLAG3,TJ3)
AE(2) = ATHREE(2)
AE(3) = ATHREE(3)
AE(4) = ATHREE(4)
AE(5) = ATHREE(5)
CALCULATE THE NORMALIZING FACTOR.
FN = SQRT( AE(2)**2 + AE(3)**2 + AE(4)**2 + AE(5)**2 )
AE(2) = AE(2)/FN
AE(3) = AE(3)/FN
AE(4) = AE(4)/FN
AE(5) = AE(5)/FN
T(1,1) = AE(2)**2 + AE(3)**2 - AE(4)**2 - AE(5)**2
T(1,2) = 2.*(AE(3)*AE(4) - AE(2)*AE(5))
T(1,3) = 2.*(AE(3)*AE(5) + AE(2)*AE(4))
T(2,1) = 2.*(AE(3)*AE(4) + AE(2)*AE(5))
T(2,2) = AE(2)**2 - AE(3)**2 + AE(4)**2 - AE(5)**2
T(2,3) = 2.*(AE(4)*AE(5) - AE(2)*AE(3))
T(3,1) = 2.*(AE(3)*AE(5) - AE(2)*AE(4))
T(3,2) = 2.*(AE(4)*AE(5) + AE(2)*AE(3))
T(3,3) = AE(2)**2 - AE(3)**2 - AE(4)**2 + AE(5)**2
CALL MULT(DUM,DUM,DUM,TIBO,TIBOI,T,2)
CALL MULT(HI,TIBO,H,DUM,DUM,DUM,1)

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THIS IS THE ENTRY POINT TO CONTM

CONTM  
CONTM

C  
C  
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C  
C

```

IF (NUMCMG .EQ. 0) GO TO 195
CALL HCON
195 CONTINUE
FPT(1) = 0.
FPT(2) = 0.
FPT(3) = 0.
FPT(4) = 0.
FPT(5) = 0.
FAT(1) = 0.
FAT(2) = 0.
FAT(3) = 0.
FAT(4) = 0.
FAT(5) = 0.
FAT(6) = 0.
FAT(7) = 0.
FAT(8) = 0.
DO 196 M=1,3
  TQOP(M) = 0.
  TQIP(M) = 0.

```

```

196 CONTINUE
    IF (IPROFF .EQ. 0) GO TO 199
    IF (IATTIF .EQ. 0) GO TO 197
    CALL ATT
    IF (ICFA .EQ. 1) GO TO 199

```

197 CONTINUE  
CALL PCON

```

199 CONTINUE
   TMP = FAT(1) + FAT(2) + FPT(2) + FPT(3) + FPT(4)
   TAP = TAP + TMP*DELTAT
   TNP = FPT(1) + FPT(5)
   TBP = TBP + TNP*DELTAT

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ccccc

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THIS IS THE ENTRY POINT TO THE INVERSION BLOCK

CALL RECALC  
CALL EMCALC

CC

## SET UP THE X MATRIX

DO 200 M=1.6

DO 200- N#1.6

$$X(M, N) = EM(M, N)$$

200 CONTINUE

```
STEMP1 = B2MASS*SDOT*(R2(3)*S2(2) + R2(2)*S2(3))
```

$$\text{STEMP2} = \text{B2MASS} * \text{SDOT} * ((\text{R2}(3) * \text{S2}(1) - \text{R2}(1) * \text{S2}(3)) * \text{COSTT1} -$$

$$- \text{R2}(2) * \text{S2}(1) + \text{R2}(1) * \text{S2}(2)) * \text{SINTT1}$$

```

      STEMP3 = B2MASS*SDOT*( (R2(3)*S2(1) - R2(1)*S2(3))*SINTT1 +
      * (R2(2)*S2(1) + R2(1)*S2(2))*COSTT1)

```

$$STEMP4 = SDOT*(S2(2)*(-B2MASS*R2(3) + (BOMASS*B2MASS/TOTMAS)*$$

```
* (D01(2)*SINTT1 - D01(3)*COSTT1) + S2(3)*(B2MASS*R2(2) -
```

$$STEMP5 = (B2MASS*B3MASS/TOTMAS)*SDOT*((EL3(3)*S2(1)) -$$

```
* EL3(1)*S2(3))*S3(2) + (-EL3(2)*S2(1) + EL3(1)*S2(2))*S3(3))
STEMP6 = (B2MASS*B4MASS/TOTMAS)*SDOT*(EL4(3)*S2(1) -
```

$$* \text{EL4}(1) * \text{S2}(3)) * \text{S4}(2) + (-\text{EL4}(2) * \text{S2}(1) + \text{EL4}(1) * \text{S2}(2)) * \text{S4}(3))$$

H(1) = H(1) - STEMP1

[illegible]

**INVER**





[illegible]

```

WRITE(6,6590) TBP
212 CONTINUE
IF (NUMCMG .EQ. 0) GO TO 214
DO 213 J=1,NUMCMG
WRITE(6,6028) J,THATA(J),J,THATAD(J)
IF (IDOF(J) .NE. 2) GO TO 213
WRITE(6,6032) J,FEE(J),J,FEED(J)
213 CONTINUE
214 CONTINUE
IPNTCK = 0
215 IPNTCK = IPNTCK + 1

C *****
C *
C *
C *
C *****
IF (IDOCK .NE. 1) GO TO 220
IF ((TIME,LT,DCHMIN).OR.(TIME,GT,DCHMAX)) GO TO 220
DO 218 M=1,3
DO 218 N=1,3
BODYOI(M,N) = BODYDI(M,N)
218 CONTINUE
BOMASS = BDMASS
DO1(1) = DDO1(1)
DO1(2) = DDO1(2)
DO1(3) = DDO1(3)
TOTMAS = BOMASS + B1MASS + B2MASS + B3MASS + B4MASS
GO TO 190
220 IF (TIME,GT,TSTOP) GO TO 10
GO TO 190

C *****
C *
C *
C *
C *****
C THIS SECTION CONTAINS ALL OF THE INPUT AND OUTPUT FORMATS.
C
5000 FORMAT(1X,I2)
5002 FORMAT(1X,3(F11.5,2X))
5004 FORMAT(1X,E11.4)
5006 FORMAT(1X,F11.5)
5008 FORMAT(1X,E11.4,2X,E11.4)
6000 FORMAT(1H,1X,16H THERE ARE (IS) ,I2,22H DATA DECK(S) PRESENT.)
6002 FORMAT(1H,1X,14HTSTART = ,E13.6,23X,14HTSTOP = ,E13.6,
* 23X,14HDELTAT = ,E13.6)
6004 FORMAT(1X,14HALTITUDE = ,E13.6)
6006 FORMAT(1X,6HTIBOI(,I1,7H,1) = ,F11.5,25X,6HTIBOI(,I1,7H,2) = ,
* F11.5,25X,6HTIBOI(,I1,7H,3) = ,F11.5)
6008 FORMAT(1X,14HWO(1) = ,E13.6,23X,14HWO(2) = ,E13.6,23X,
* 14HWO(3) = ,E13.6)
6010 FORMAT(1X,1HB,I1,12HMASS = ,E13.6)
6012 FORMAT(1X,7HBODYOI(,I1,6H,1) = ,E13.6,23X,7HBODYOI(,I1,6H,2) = ,
* E13.6,23X,7HBODYOI(,I1,6H,3) = ,E13.6)
6014 FORMAT(1X,14HNUMCMG = ,I2)
6016 FORMAT(1X,11HCMG NUMBER ,I1,21H IS A REACTION WHEEL,)
6018 FORMAT(1X,11HCMG NUMBER ,I1,26H HAS ONE DEGREE OF FREEDOM)
6020 FORMAT(1X,11HCMG NUMBER ,I1,27H HAS TWO DEGREES OF FREEDOM)
6022 FORMAT(1X,35H THE ANGULAR MOMENTUM OF CMG NUMBER ,I1,3H = ,E13.6)
6024 FORMAT(1X,5SHAOCJ(,I1,1H,1,6H,1) = ,F11.5,25X,5SHAOCJ(,I1,1H,1,
* 6H,2) = ,F11.5,25X,5SHAOCJ(,I1,1H,1,6H,3) = ,F11.5)

```

```

6026 FORMAT(1X,4HAI1(,I1,1H,1) = ,E13.6,23X,4HAI1(,I1,1H,1, I/O
* 7H,2) = ,E13.6,23X,4HAI1(,I1,1H,1,7H,3) = ,E13.6) I/O
6028 FORMAT(1X,6HTHATA(,I1,7H) = ,E13.6,23X,7HTHATA(,I1,6H) = , I/O
* E13.6) I/O
6030 FORMAT(1X,4HAI0(,I1,1H,1) = ,E13.6,23X,4HAI0(,I1,1H,1, I/O
* 7H,2) = ,E13.6,23X,4HAI0(,I1,1H,1,7H,3) = ,E13.6) I/O
6032 FORMAT(1X,4HFEE(,I1,9H) = ,E13.6,23X,5HFEE(,I1,8H) = , I/O
* E13.6) I/O
6040 FORMAT(1X,7HBODY11(,I1,6H,1) = ,E13.6,23X,7HBODY11(,I1,6H,2) = , I/O
* E13.6,23X,7HBODY11(,I1,6H,3) = ,E13.6) I/O
6042 FORMAT(1X,14HTHETA1 = ,E13.6,23X,14HOMEGA1 = ,E13.6) I/O
6044 FORMAT(1X,14HD01(1) = ,E13.6,23X,14HD01(2) = ,E13.6, I/O
* 23X,14HD01(3) = ,E13.6) I/O
6048 FORMAT(1X,14HD13(1) = ,E13.6,23X,14HD13(2) = ,E13.6, I/O
* 23X,14HD13(3) = ,E13.6) I/O
6050 FORMAT(1X,14HD14(1) = ,E13.6,23X,14HD14(2) = ,E13.6, I/O
* 23X,14HD14(3) = ,E13.6) I/O
6052 FORMAT(1X,1HS,I1,12H(1) = ,E13.6,23X,1HS,I1,12H(2) = ,I/O
*E13.6,23X,1HS,I1,12H(3) = ,E13.6) I/O
6058 FORMAT(1X,14HPEND3L = ,E13.6) I/O
6060 FORMAT(1X,14HTHETA3 = ,E13.6) I/O
6062 FORMAT(1X,14HOMEGA3 = ,E13.6) I/O
6064 FORMAT(1X,14HPEND4L = ,E13.6) I/O
6066 FORMAT(1X,14HTHETA4 = ,E13.6,23X,14HOMEGA4 = ,E13.6) I/O
6068 FORMAT(1X,14HIDOCK = ,I2) I/O
6070 FORMAT(1X,14HDTIME = ,E13.6) I/O
6072 FORMAT(1X,14HIPROPF = ,I2) I/O
6074 FORMAT(1X,4HA0J(,I2,8H) = ,E13.6,23X,7HCGAIN0(,I2,5H) = , I/O
* E13.6) I/O
6076 FORMAT(1X,4HA1J(,I1,9H) = ,E13.6,23X,7HCGAIN1(,I1,6H) = , I/O
* E13.6) I/O
6078 FORMAT(1X,14HIGRAVF = ,I2) I/O
6080 FORMAT(1X,14HSP = ,E13.6) I/O
6082 FORMAT(1H1,1X,9HIPNDLM = ,I2,/) I/O
6500 FORMAT(1H1,1X,46H THE FOLLOWING INPUT CORRESPONDS TO DATA DECK ,I2I/O
*) I/O
6502 FORMAT(1H1,1X,127H***** I/O
***** I/O
***** ,/) I/O
6504 FORMAT(1X,14HTIME = ,F11.5,/) I/O
6506 FORMAT(1X,1HW,I1,12H(1) = ,E13.6,23X,1HW,I1,12H(2) = ,I/O
*E13.6,23X,1HW,I1,12H(3) = ,E13.6) I/O
6510 FORMAT(1X,14HH(1) = ,E13.6,23X,14HH(2) = ,E13.6, I/O
* 23X,14HH(3) = ,E13.6) I/O
6512 FORMAT(1X,14HHI(1) = ,E13.6,23X,14HHI(2) = ,E13.6, I/O
* 23X,14HHI(3) = ,E13.6) I/O
6514 FORMAT(1X,14HHDOT(1) = ,E13.6,23X,14HHDOT(2) = ,E13.6, I/O
* 23X,14HHDOT(3) = ,E13.6) I/O
6516 FORMAT(1X,1HH,I1,12HPRIM(1) = ,E13.6,23X,1HH,I1,12HPRIM(2) = ,I/O
*E13.6,23X,1HH,I1,12HPRIM(3) = ,E13.6) I/O
6522 FORMAT(1X,2HEL,I1,11H(1) = ,E13.6,23X,2HEL,I1,11H(2) = ,I/O
*E13.6,23X,2HEL,I1,11H(3) = ,E13.6) I/O
6524 FORMAT(1X,2HEL,I1,11HDOT(1) = ,E13.6,23X,2HEL,I1,11HDOT(2) = ,I/O
*E13.6,23X,2HEL,I1,11HDOT(3) = ,E13.6) I/O
6526 FORMAT(1X,1HR,I1,12H(1) = ,E13.6,23X,1HR,I1,12H(2) = ,I/O
*E13.6,23X,1HR,I1,12H(3) = ,E13.6) I/O
6528 FORMAT(1X,1HR,I1,12HDOT(1) = ,E13.6,23X,1HR,I1,12HDOT(2) = ,I/O
*E13.6,23X,1HR,I1,12HDOT(3) = ,E13.6) I/O
6535 FORMAT(1X,14HD12(1) = ,E13.6,23X,14HD12(2) = ,E13.6, I/O
* 23X,14HD12(3) = ,E13.6) I/O
6536 FORMAT(1X,14HTOTMAS = ,F11.5,25X,14HTOTMAS = ,E13.6,/) I/O
6538 FORMAT(1X,5HTIB0(,I1,8H,1) = ,F11.5,25X,5HTIB0(,I1,8H,2) = , I/O

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*F11.5,25X,5HTIB0(,I1,8H,3) = ,F11.5) I/O
6544 FORMAT(1X,14HIPRINT = ,I2) I/O
6546 FURMAT(1X,14HIB2F = ,I2) I/O
6548 FURMAT(1X,14HS = ,E13.6,23X,14HSDOT = ,E13.6) I/O
6550 FORMAT(1X,19HGENERAL INFORMATION,/) I/O
6552 FURMAT(1X,5HBODY ,I1,12H INFORMATION,/) I/O
6554 FORMAT(/) I/O
6556 FORMAT(1X,14HS = ,E13.6,23X,14HSDOT = ,E13.6) I/O
6558 FURMAT(1X,5HTHETA,I1,8H = ,E13.6,23X,5HOMEGA,I1,8H = , I/O
* E13.6) I/O
6560 FORMAT(1X,1HG,I1,12H = ,E13.6,23X,1HG,I1,12HDOT = , I/O
* E13.6) I/O
6562 FORMAT(1X,14HIATTIF = ,I1) I/O
6564 FORMAT(1X,14HCA(1) = ,E13.6,23X,14HCA(2) = ,E13.6, I/O
* 23X,14HCA(3) = ,E13.6) I/O
6566 FORMAT(1X,14HAA01 = ,E13.6,23X,14HAGAIN1 = ,E13.6) I/O
6568 FORMAT(1X,14HAA02 = ,E13.6,23X,14HAGAIN2 = ,E13.6) I/O
6570 FORMAT(1X,14HNGAIN = ,I2) I/O
6572 FURMAT(1X,5HGAIN(,I1,8H) = ,E13.6) I/O
6574 FORMAT(1X,14HBDMASS = ,E13.6) I/O
6576 FORMAT(1X,7HBODYDI(,I1,6H,1) = ,E13.6,23X,7HBODYDI(,I1,6H,2) = , I/O
* E13.6,23X,7HBODYDI(,I1,6H,3) = ,E13.6) I/O
6578 FORMAT(1X,14HDTI(1) = ,E13.6,23X,14HDTI(2) = ,E13.6, I/O
* 23X,14HDTI(3) = ,E13.6) I/O
6580 FORMAT(1X,20HDOCKING HAS OCCURRED) I/O
6582 FORMAT(1X,14HCP1 = ,E13.6) I/O
6584 FURMAT(1X,14HCP2 = ,E13.6) I/O
6586 FURMAT(1X,14HDD01(1) = ,E13.6,23X,14HDD01(2) = ,E13.6, I/O
* 23X,14HDD01(3) = ,E13.6) I/O
6588 FORMAT(1X,54HTHE TOTAL PROPULSION IMPULSE ON THE TRANSVERSE AXIS = I/O
* ,E13.6) I/O
6590 FORMAT(1X,48HTHE TOTAL PROPULSION IMPULSE ON THE SPIN AXIS = , I/O
* E13.6) I/O

C *****
C *
C *
C *
C *
END

```

C  
C  
C  
C

# SUBROUTINE ATT

```

*****
COMMON      A(3)          ,      AE(5)          ,      AED(5)          ,      COMM
*            AF0UR(2)      ,      AII(6,3,3)      ,      ,      COMM
*            AIO(6,3,3)    ,      AJ1(3)          ,      ALT          ,      COMM
*            AOCJ(6,3,3)   ,      AOJ(3)          ,      AONE(7)       ,      COMM
*            ATCPT2(3,3)   ,      ATHREE(5)       ,      ATWO(4)      ,      COMM
*            A1(3,3)       ,      A1J(2)          ,      ,      COMM
COMMON      BDMASS        ,      BFOUR(2)         ,      BMOM          ,      COMM
*            BODYDI(3,3)   ,      BODYOI(3,3)    ,      BODY1I(3,3)   ,      COMM
*            BOMASS        ,      BONE(7)          ,      BTHREE(5)      ,      COMM
*            BTWO(4)       ,      B1MASS         ,      B2MASS        ,      COMM
*            B3MASS        ,      B4MASS         ,      ,      COMM
COMMON      CA(3)         ,      CB(3)          ,      CGAINO(3)      ,      COMM
*            CGAIN1(2)     ,      ,      ,      COMM
*            COSFEJ        ,      COSTTJ         ,      COSTTO         ,      COMM
*            COSTT1        ,      COSTT3         ,      COSTT4         ,      COMM
*            CO2T          ,      CP1           ,      CP2           ,      COMM
*            CST           ,      C1            ,      ,      COMM
COMMON      DB(3)         ,      DD01(3)        ,      ,      COMM
*            DELTAT        ,      D01(3)         ,      D01DOT(3)      ,      COMM
*            DTI(3)        ,      ,      ,      COMM
*            DTIME         ,      D12(3)         ,      D13(3)         ,      COMM
*            D13DOT(3)     ,      D13YCS         ,      D13YSN         ,      COMM
*            D13ZCS        ,      D13ZSN         ,      D14(3)         ,      COMM
*            D14DOT(3)     ,      D14YCS         ,      D14YSN         ,      COMM
*            D14ZCS        ,      D14ZSN         ,      ,      COMM
COMMON      EEE(3,3)      ,      EEJ(3,3)       ,      EL2(3)         ,      COMM
*            EL2DOT(3)     ,      EL2YCS         ,      EL2YSN         ,      COMM
*            EL2ZCS        ,      EL2ZSN         ,      EL3(3)         ,      COMM
*            EL3DOT(3)     ,      EL3YCS         ,      EL3YSN         ,      COMM
*            EL3ZCS        ,      EL3ZSN         ,      EL4(3)         ,      COMM
*            EL4DOT(3)     ,      EL4YCS         ,      EL4YSN         ,      COMM
*            EL4ZCS        ,      EL4ZSN         ,      EM(6,6)        ,      COMM
COMMON      FAT(8)        ,      ,      ,      COMM
*            FEE(6)        ,      FEED(6)        ,      FFF(3)         ,      COMM
*            FFJ(3)        ,      FLAG1          ,      FLAG2          ,      COMM
*            FLAG3        ,      FLAG4          ,      FNI            ,      COMM
*            FO(3)         ,      FO1(3)         ,      FO2(3)         ,      COMM
*            FO3(3)        ,      F1(3)          ,      F11(3)         ,      COMM
*            FPT(5)        ,      ,      ,      COMM
*            F12(3)        ,      F13(3)         ,      ,      COMM
COMMON      GAIN(10)      ,      G3            ,      ,      COMM
*            G3DOT        ,      G4            ,      G4DOT          ,      COMM
COMMON      H(3)          ,      HCMG(3)        ,      HDOT(3)        ,      COMM
*            HI(3)         ,      HO(3)          ,      HW(6)          ,      COMM
*            H1(3)         ,      H1PDOT(3)       ,      H1PRIM(3)       ,      COMM
*            H3PRIM(3)     ,      H4PRIM(3)       ,      ,      COMM
COMMON      IBZF          ,      ICFA           ,      ICFB           ,      COMM
*            ICFC          ,      ICFO           ,      IDOCK          ,      COMM
*            IDOF(6)       ,      ,      ,      COMM
*            IGRAVF        ,      IPNDLM          ,      IPNTCK          ,      COMM
*            IPRINT        ,      IPROPF          ,      ,      COMM
COMMON      NCASE         ,      NCHECK          ,      NDECK          ,      COMM
*            NGAIN         ,      NUMCMG          ,      ,      COMM
COMMON      OMEGA1        ,      OMEGA3          ,      OMEGA4          ,      COMM
COMMON      PEND3L        ,      PEND4L          ,      ,      COMM
COMMON      Q(4,4)        ,      ,      ,      COMM

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COMMON	R	R0(3)	R1(3)
R1DOT(3)	R1YCS	R1YSN	
R1ZCS	R1ZSN	R2(3)	
R2DOT(3)	R2YCS	R2YSN	
R2ZCS	R2ZSN	R3(3)	
R3DOT(3)	R3YCS	R3YSN	
R3ZCS	R3ZSN	R4(3)	
R4DOT(3)	R4YCS	R4YSN	
R4ZCS	R4ZSN		
S	SDOT	SINFEJ	
SINTTJ	SINTT0	SINTT1	
SINTT2	SINTT3	SINTT4	
SP	SUM1	SUM2	
SUM3	S2(3)	S3(3)	
S4(3)			
COMMON	T(3,3)	TC(3,3)	TEMP1(3)
TEMP2(3)			
TEMP3(3)	TEMP4(3)	TEMP5(3,3)	
TEMP6(3,3)	TEMP7(3,3)	TEMP8(3,3)	
TEMP9(3,3)	TEMP10(3,3)	TEMP11(3,3)	
TEMP12(3,3)	TEMP13(3,3)	TEMP14(3,3)	
TEMP15(3,3)	TERM1(3)	TERM2(3)	
YFRIC	THATA(6)	THATAD(6)	
THETA1	THETA3	THETA4	
THETO	TIBO(3,3)	TIBOI(3,3)	
TIME	TJ	TJ1(10)	
TJ2(10)	TJ3(10)	TJ4(10)	
TMOTOR			
TOEF(3)	TOTMAS	TO1	
TQOG(3)	TQOP(3)	TQ1G(3)	
TQ1P(3)	TSTART	TSTOP	
TT1DOT	TT3DOT	TT4DOT	
T1EF(3)	T13	T14	
COMMON	V(3)		
COMMON	W0(3)	W1(3)	
W3(3)	W4(3)		
COMMON	X(6,7)	XC	XCDOT
XMU			

```

*****
*
*
*
*****

ICFD = 0
IF (ICFA .EQ. 1) GO TO 11
IF (ABS(WO(2)) .GT. 0.0002) GO TO 60
IF (ABS(WO(3)) .GT. 0.0002) GO TO 60
DO 10 M=1,3
CB(M) = TIBO(1,M)*CA(1) + TIBO(2,M)*CA(2) + TIBO(3,M)*CA(3)
10 CONTINUE
IF (CB(1) .LT. 0.9994) GO TO 11
ICFA = 0
ICFB = 0
ICFC = 0
GO TO 60
11 CONTINUE
ICFA = 1
IF (ICFB .EQ. 1) GO TO 30
TMA = TIME
ZTCL = 0

```

DO 13 M=1,3	ATT
DU 13 N=1,3	ATT
TC(M,N) = TIBO(M,N)	ATT
13 CONTINUE	ATT
CN = CB(3)**2 + CB(2)**2	ATT
CN = SQRT(CN)	ATT
CA2 = CB(2)/CN	ATT
CA3 = CB(3)/CN	ATT
AL = 0.5*ACOS(CB(1))	ATT
AK = BODY11(1,1)*OMEGA1*SIN(AL)/(5.5 + DELTAT)	ATT
ICFB = 1	ATT
30 CONTINUE	ATT
TMACHK = TMA + 5.0	ATT
IF (TIME .GT. TMACHK) GO TO 40	ATT
ICFD = 1	ATT
GO TO 60	ATT
40 CONTINUE	ATT
IF (ICFC .EQ. 1) GO TO 50	ATT
ZTC = -CA3*(TC(1,2)*TIBO(1,1)+TC(2,2)*TIBO(2,1)+TC(3,2)*TIBO(3,1))	ATT
*       +CA2*(TC(1,3)*TIBO(1,1)+TC(2,3)*TIBO(2,1)+TC(3,3)*TIBO(3,1))	ATT
IF (ZTC .GT. ZTCL) GO TO 71	ATT
ZTCL = ZTC	ATT
GO TO 60	ATT
71 CONTINUE	ATT
TMB = TIME	ATT
TMC = TMB - TMA - 6.0	ATT
TMC = TMB + TMC	ATT
TMB = TMC + 5.0	ATT
ICFC = 1	ATT
GO TO 60	ATT
50 CONTINUE	ATT
IF (TIME .GT. TMB) GO TO 80	ATT
IF (TIME .LT. TMC) GO TO 60	ATT
ICFD = 1	ATT
GO TO 60	ATT
80 CONTINUE	ATT
ICFA = 0	ATT
ICFB = 0	ATT
ICFC = 0	ATT
60 CONTINUE	ATT
IF (ICFD .EQ. 0) GO TO 90	ATT
TQOP(2) = AK*CA2	ATT
TQOP(3) = AK*CA3	ATT
FAT(1) = 2.*ABS(TQOP(2)/AOJ(2))	ATT
FAT(2) = 2.*ABS(TQOP(3)/AOJ(3))	ATT
90 CONTINUE	ATT
65 CONTINUE	ATT
RETURN	ATT
*****	ATT
*	ATT
*	ATT
*	ATT
END	ATT

C  
C  
C  
C



C  
C  
C  
C

## SUBROUTINE CMG

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*****
COMMON      A(3)          ,      AE(5)          ,      AED(5)          ,      COMMC
*            AFOUR(2)      ,      AII(6,3,3)     ,      ,      COMMC
*            AIO(6,3,3)    ,      AJ1(3)         ,      ALT          ,      COMMC
*            AOCJ(6,3,3)   ,      AOJ(3)         ,      AONE(7)       ,      COMMC
*            ATCPT2(3,3)   ,      ATHREE(5)      ,      ATWO(4)      ,      COMMC
*            A1(3,3)       ,      AIJ(2)         ,      ,      COMMC
COMMON      BDMASS        ,      BFOUR(2)        ,      BMOM          ,      COMMC
*            BODYDI(3,3)   ,      BODYOI(3,3)     ,      BODY1I(3,3) ,      COMMC
*            BOMASS        ,      BONE(7)         ,      BTHREE(5)    ,      COMMC
*            BTWO(4)       ,      B1MASS         ,      B2MASS      ,      COMMC
*            B3MASS        ,      B4MASS         ,      ,      COMMC
COMMON      CA(3)         ,      CB(3)          ,      CGAINO(3)     ,      COMMC
*            CGAIN1(2)     ,      ,      ,      COMMC
*            COSFEJ        ,      COSTTJ         ,      COSTTO      ,      COMMC
*            COSTT1        ,      COSTT3         ,      COSTT4      ,      COMMC
*            CO2T          ,      CP1           ,      CPE          ,      COMMC
*            CST           ,      C1            ,      ,      COMMC
COMMON      DB(3)         ,      DDO1(3)        ,      ,      COMMC
*            DELTAT        ,      DO1(3)         ,      ,      COMMC
*            DTI(3)        ,      ,      ,      COMMC
*            DTIME        ,      D12(3)          ,      D13(3)         ,      COMMC
*            D13DOT(3)     ,      D13YCS         ,      D13YSN        ,      COMMC
*            D13ZCS        ,      D13ZSN         ,      D14(3)         ,      COMMC
*            D14DOT(3)     ,      D14YCS         ,      D14YSN        ,      COMMC
*            D14ZCS        ,      D14ZSN         ,      ,      COMMC
COMMON      EEE(3,3)      ,      EEJ(3,3)        ,      EL2(3)         ,      COMMC
*            EL2DOT(3)     ,      EL2YCS         ,      EL2YSN        ,      COMMC
*            EL2ZCS        ,      EL2ZSN         ,      EL3(3)         ,      COMMC
*            EL3DOT(3)     ,      EL3YCS         ,      EL3YSN        ,      COMMC
*            EL3ZCS        ,      EL3ZSN         ,      EL4(3)         ,      COMMC
*            EL4DOT(3)     ,      EL4YCS         ,      EL4YSN        ,      COMMC
*            EL4ZCS        ,      EL4ZSN         ,      EM(6,6)       ,      COMMC
COMMON      FAT(8)        ,      ,      ,      COMMC
*            FEE(6)        ,      FEED(6)        ,      FFF(3)         ,      COMMC
*            FFJ(3)        ,      FLAG1         ,      FLAG2        ,      COMMC
*            FLAG3        ,      FLAG4         ,      FNI          ,      COMMC
*            FO(3)         ,      FO1(3)         ,      FO2(3)         ,      COMMC
*            FO3(3)        ,      F1(3)         ,      F11(3)        ,      COMMC
*            FPT(5)        ,      ,      ,      COMMC
*            F12(3)        ,      F13(3)         ,      ,      COMMC
COMMON      GAIN(10)      ,      G3           ,      ,      COMMC
*            G3DOT        ,      G4            ,      G4DOT         ,      COMMC
COMMON      H(3)          ,      HCMG(3)        ,      HDOT(3)       ,      COMMC
*            HI(3)         ,      HO(3)         ,      HW(6)         ,      COMMC
*            H1(3)         ,      H1PDOT(3)     ,      H1PRIM(3)    ,      COMMC
*            H3PRIM(3)     ,      H4PRIM(3)     ,      ,      COMMC
COMMON      IB2F          ,      ICFA          ,      ICFB          ,      COMMC
*            ICFC          ,      ICFO          ,      IDOCK         ,      COMMC
*            IDOF(6)       ,      ,      ,      COMMC
*            IGRAVF        ,      IPNDLM        ,      IPNTCK        ,      COMMC
*            IPRINT        ,      IPROPF        ,      ,      COMMC
COMMON      NCASE         ,      NCHECK        ,      NDECK        ,      COMMC
*            NGAIN         ,      NUMCMG        ,      ,      COMMC
COMMON      OMEGA1        ,      OMEGA3        ,      OMEGA4        ,      COMMC
COMMON      PEND3L        ,      PEND4L        ,      ,      COMMC
COMMON      Q(4,4)        ,      ,      ,      COMMC
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COMMON	R		R0(3)		R1(3)	COMMON
	R1DOT(3)		R1YCS		R1YSN	COMMON
	R1ZCS		R1ZSN		R2(3)	COMMON
	R2DOT(3)		R2YCS		R2YSN	COMMON
	R2ZCS		R2ZSN		R3(3)	COMMON
	R3DOT(3)		R3YCS		R3YSN	COMMON
	R3ZCS		R3ZSN		R4(3)	COMMON
	R4DOT(3)		R4YCS		R4YSN	COMMON
	R4ZCS		R4ZSN			COMMON
COMMON	S		SDOT		SINFEJ	COMMON
	SINTTJ		SINTT0		SINTT1	COMMON
	SINTT2		SINTT3		SINTT4	COMMON
	SP		SUM1		SUM2	COMMON
	SUM3		S2(3)		S3(3)	COMMON
	S4(3)					COMMON
COMMON	T(3,3)		TC(3,3)		TEMP1(3)	COMMON
	TEMP2(3)					COMMON
	TEMP3(3)		TEMP4(3)		TEMP5(3,3)	COMMON
	TEMP6(3,3)		TEMP7(3,3)		TEMP8(3,3)	COMMON
	TEMP9(3,3)		TEMP10(3,3)		TEMP11(3,3)	COMMON
	TEMP12(3,3)		TEMP13(3,3)		TEMP14(3,3)	COMMON
	TEMP15(3,3)		TERM1(3)		TERM2(3)	COMMON
	TFRIC		THATA(6)		THATA(6)	COMMON
	THETA1		THETA3		THETA4	COMMON
	THETO		TIB0(3,3)		TIB01(3,3)	COMMON
	TIME		TJ		TJ1(10)	COMMON
	TJ2(10)		TJ3(10)		TJ4(10)	COMMON
	TMOTOR					COMMON
	TOEF(3)		TOTMAS		TO1	COMMON
	TQOG(3)		TQOP(3)		TQ1G(3)	COMMON
	TQ1P(3)		TSTART		TSTOP	COMMON
	TT1DOT		TT3DOT		TT4DOT	COMMON
	T1EF(3)		T13		T14	COMMON
COMMON	V(3)					COMMON
COMMON	W0(3)		WS		W1(3)	COMMON
	W3(3)		W4(3)			COMMON
COMMON	X(6,7)		XC		XCDOT	COMMON
	XMU					COMMON

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## SUBROUTINE EMCALC

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COMMON A(3) , AE(5) , AED(5) , COMM
*      AF0UR(2) , AII(6,3,3) , COMM
*      AIO(6,3,3) , AJ1(3) , ALT , COMM
*      AOCJ(6,3,3) , AOJ(3) , AONE(7) , COMM
*      ATCPT2(3,3) , ATHREE(5) , ATWO(4) , COMM
*      A1(3,3) , A1J(2) , COMM
COMMON BDMASS , BFOUR(2) , BMOM , COMM
*      BODYDI(3,3) , BODYUI(3,3) , BODY1I(3,3) , COMM
*      BOMASS , BONE(7) , BTHREE(5) , COMM
*      BTWO(4) , B1MASS , B2MASS , COMM
*      B3MASS , B4MASS , COMM
COMMON CA(3) , CB(3) , CGAINO(3) , COMM
*      CGAIN1(2) , COMM
*      COSFEJ , COSTTJ , COSTTQ , COMM
*      COSTT1 , COSTI3 , COSTT4 , COMM
*      CO2T , CP1 , CP2 , COMM
*      CST , C1 , COMM
COMMON DB(3) , DD01(3) , COMM
*      DELTAT , DO1(3) , DO1DOT(3) , COMM
*      DT1(3) , COMM
*      DTIME , D12(3) , D13(3) , COMM
*      D13DOT(3) , D13YCS , D13YSN , COMM
*      D13ZCS , D13ZSN , D14(3) , COMM
*      D14DOT(3) , D14YCS , D14YSN , COMM
*      D14ZCS , D14ZSN , COMM
COMMON EEE(3,3) , EEJ(3,3) , EL2(3) , COMM
*      EL2DOT(3) , EL2YCS , EL2YSN , COMM
*      EL2ZCS , EL2ZSN , EL3(3) , COMM
*      EL3DOT(3) , EL3YCS , EL3YSN , COMM
*      EL3ZCS , EL3ZSN , EL4(3) , COMM
*      EL4DOT(3) , EL4YCS , EL4YSN , COMM
*      EL4ZCS , EL4ZSN , EM(6,6) , COMM
COMMON FAT(8) , COMM
*      FEE(6) , FEED(6) , FFF(3) , COMM
*      FFJ(3) , FLAG1 , FLAG2 , COMM
*      FLAG3 , FLAG4 , FN , COMM
*      FO(3) , FO1(3) , FO2(3) , COMM
*      FO3(3) , F1(3) , F11(3) , COMM
*      FPT(5) , COMM
*      F12(3) , F13(3) , COMM
COMMON GAIN(10) , G3 , COMM
*      G3DOT , G4 , G4DOT , COMM
COMMON H(3) , HCMG(3) , HDOT(3) , COMM
*      HI(3) , HO(3) , HW(6) , COMM
*      H1(3) , H1PDOT(3) , H1PRIM(3) , COMM
*      H3PRIM(3) , H4PRIM(3) , COMM
COMMON IBZF , ICFA , ICFB , COMM
*      ICFC , ICFD , IDOCK , COMM
*      IDOF(6) , COMM
*      IGRAVF , IPNDLM , IPNTCK , COMM
*      IPRINT , IPROPF , COMM
COMMON NCASE , NCHECK , NDECK , COMM
*      NGAIN , NUMCMG , COMM
COMMON OMEGA1 , OMEGA3 , OMEGA4 , COMM
COMMON PEND3L , PEND4L , COMM
COMMON Q(4,4) , COMM

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COMMON	R	RO(3)	R1(3)	COMMON
*	R1DOT(3)	R1YCS	R1YSN	COMMON
*	R1ZCS	R1ZSN	R2(3)	COMMON
*	R2DOT(3)	R2YCS	R2YSN	COMMON
*	R2ZCS	R2ZSN	R3(3)	COMMON
*	R3DOT(3)	R3YCS	R3YSN	COMMON
*	R3ZCS	R3ZSN	R4(3)	COMMON
*	R4DOT(3)	R4YCS	R4YSN	COMMON
*	R4ZCS	R4ZSN		COMMON
COMMON	S	SDOT	SINFEJ	COMMON
*	SINTTJ	SINTT0	SINTT1	COMMON
*	SINTT2	SINTT3	SINTT4	COMMON
*	SP	SUM1	SUM2	COMMON
*	SUM3	S2(3)	S3(3)	COMMON
*	S4(3)			COMMON
COMMON	T(3,3)	TC(3,3)	TEMP1(3)	COMMON
*	TEMP2(3)			COMMON
*	TEMP3(3)	TEMP4(3)	TEMP5(3,3)	COMMON
*	TEMP6(3,3)	TEMP7(3,3)	TEMP8(3,3)	COMMON
*	TEMP9(3,3)	TEMP10(3,3)	TEMP11(3,3)	COMMON
*	TEMP12(3,3)	TEMP13(3,3)	TEMP14(3,3)	COMMON
*	TEMP15(3,3)	TERM1(3)	TERM2(3)	COMMON
*	TFRICT	THATA(6)	THATA4(6)	COMMON
*	THETA1	THETA3	THETA4	COMMON
*	THETO	TIBO(3,3)	TIBO1(3,3)	COMMON
*	TIME	TJ	TJ1(10)	COMMON
*	TJ2(10)	TJ3(10)	TJ4(10)	COMMON
*	TMOTOR			COMMON
*	TOEF(3)	TOTMAS	TO1	COMMON
*	TQOG(3)	TQOP(3)	TQ1G(3)	COMMON
*	TQ1P(3)	TSTART	TSTOP	COMMON
*	TT1DOT	TT3DOT	TT4DOT	COMMON
*	T1EF(3)	T13	T14	COMMON
COMMON	V(3)			COMMON
COMMON	W0(3)	WS	W1(3)	COMMON
*	W3(3)	W4(3)		COMMON
COMMON	X(6,7)	XC	XCDOT	COMMON
*	XMU			COMMON

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THE FOLLOWING CALCULATIONS WILL BE USED REPEATEDLY TO CALCULATE M

SINTT1 = SIN(THETA1)	EMCAL
COSTT1 = COS(THETA1)	EMCAL
C02T = COSTT1**2	EMCAL
CST = COSTT1*SINTT1	EMCAL
SI2T = SINTT1**2	EMCAL
R1YCS = R1(2)*COSTT1	EMCAL
R2YCS = R2(2)*COSTT1	EMCAL
R3YCS = R3(2)*COSTT1	EMCAL
R4YCS = R4(2)*COSTT1	EMCAL
R1ZCS = R1(3)*COSTT1	EMCAL
R2ZCS = R2(3)*COSTT1	EMCAL
R3ZCS = R3(3)*COSTT1	EMCAL
R4ZCS = R4(3)*COSTT1	EMCAL
R1YSN = R1(2)*SINTT1	EMCAL
R2YSN = R2(2)*SINTT1	EMCAL





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C      EM(1,6)=-B4MASS*R4(3)*(S4(3)*EL4(1)-S4(1)*EL4(3))+
*      B4MASS*R4(2)*(-S4(2)*EL4(1)+S4(1)*EL4(2))
C
      EM(2,1)=BODYOI(2,1)+BODYII(2,1)*COSTT1-BODYII(3,1)*SINTT1-
*      B1MASS*DO1(1)*(R1YCS-R1ZSN)-
*      B2MASS*(R2YCS-R2ZSN)*(DO1(1)+EL2(1))-
*      B3MASS*(R3YCS-R3ZSN)*(DO1(1)+D13(1)+EL3(1))-
*      B4MASS*(R4YCS-R4ZSN)*(DO1(1)+D14(1)+EL4(1))
C
      EM(2,2)=BODYOI(2,2)+BODYII(2,2)*COSTT1-BODYII(2,3)*CST
*      -BODYII(3,2)*CST + BODYII(3,3)*SI2T +
*      B1MASS*R1(1)*DO1(1)+B1MASS*DO1(3)*(R1YSN+R1ZCS)+
*      B2MASS*R2(1)*(DO1(1)+EL2(1))+
*      B2MASS*(R2YSN+R2ZCS)*(DO1(3)+EL2YSN+EL2ZCS)+
*      B3MASS*R3(1)*(DO1(1)+D13(1)+EL3(1))+
*      B3MASS*(R3YSN+R3ZCS)*(DO1(3)+D13YSN+D13ZCS+EL3YSN+EL3ZCS)+
*      B4MASS*R4(2)*(DO1(1)+D14(1)+EL4(1))+
*      B4MASS*(R4YSN+R4ZCS)*(DO1(3)+D14YSN+D14ZCS+EL4YSN+EL4ZCS)
C
      EM(2,3)=BODYOI(2,3)+BODYII(2,2)*CST +BODYII(2,3)*COSTT1
*      -BODYII(3,2)*SI2T - BODYII(3,3)*CST -
*      B1MASS*DO1(3)*(R1YCS-R1ZSN)-
*      B2MASS*(R2YCS-R2ZSN)*(DO1(3)+EL2YSN+EL2ZCS)-
*      B3MASS*(R3YCS-R3ZSN)*(DO1(3)+D13YSN+D13ZCS+EL3YSN+EL3ZCS)-
*      B4MASS*(R4YCS-R4ZSN)*(DO1(3)+D14YSN+D14ZCS+EL4YSN+EL4ZCS)
C
      EM(2,4)=BODYII(1,2)*COSTT1-BODYII(1,3)*SINTT1-B1MASS*DO1(1)*R1YCS+
*      B1MASS*DO1(1)*R1ZSN+BMOM*B1MASS*DO1(1)*DO1(2)-
*      B2MASS*(DO1(1)+EL2(1))*(R2YCS-R2ZSN-BMOM*DO1(2))-
*      B3MASS*(DO1(1)+D13(1)+EL3(1))*(R3YCS-R3ZSN-BMOM*DO1(2))-
*      B4MASS*(DO1(1)+D14(1)+EL4(1))*(R4YCS-R4ZSN-BMOM*DO1(2))
C
      EM(2,5)=(B3MASS*R3(3)*(-S3(3)*EL3(2)+S3(2)*EL3(3))-
*      B3MASS*R3(1)*(-S3(2)*EL3(1)+S3(1)*EL3(2)))*COSTT1-
*      (-B3MASS*R3(2)*(-S3(3)*EL3(2)+S3(2)*EL3(3))+
*      B3MASS*R3(1)*(S3(3)*EL3(1)-S3(1)*EL3(3)))*SINTT1
C
      EM(2,6)=(B4MASS*R4(3)*(-S4(3)*EL4(2)+S4(2)*EL4(3))-
*      B4MASS*R4(1)*(-S4(2)*EL4(1)+S4(1)*EL4(2)))*COSTT1-
*      (-B4MASS*R4(2)*(-S4(3)*EL4(2)+S4(2)*EL4(3))+
*      B4MASS*R4(1)*(S4(3)*EL4(1)-S4(1)*EL4(3)))*SINTT1
C
      EM(3,1)=BODYOI(3,1)+BODYII(2,1)*SINTT1+BODYII(3,1)*COSTT1-
*      B1MASS*DO1(1)*(R1YSN+R1ZCS)-
*      B2MASS*(DO1(1)+EL2(1))*(R2YSN+R2ZCS)-
*      B3MASS*(DO1(1)+D13(1)+EL3(1))*(R3YSN+R3ZCS)-
*      B4MASS*(DO1(1)+D14(1)+EL4(1))*(R4YSN+R4ZCS)
C
      EM(3,2)=BODYOI(3,2)+BODYII(2,2)*CST -BODYII(2,3)*SI2T
*      +BODYII(3,2)*COSTT1-BODYII(3,3)*CST-
*      B1MASS*DO1(2)*(R1YSN+R1ZCS)-
*      B2MASS*(R2YSN+R2ZCS)*(DO1(2)+EL2YCS-EL2ZSN)-
*      B3MASS*(R3YSN+R3ZCS)*(DO1(2)+D13YCS-D13ZSN+EL3YCS-EL3ZSN)-
*      B4MASS*(R4YSN+R4ZCS)*(DO1(2)+D14YCS-D14ZSN+EL4YCS-EL4ZSN)
C
      EM(3,3)=BODYOI(3,3)+BODYII(2,2)*SI2T +BODYII(2,3)*CST
*      +BODYII(3,2)*CST + BODYII(3,3)*COSTT1 +
*      B1MASS*R1(1)*DO1(1)+B1MASS*(R1YCS-R1ZSN)*DO1(2)+
*      B2MASS*R2(1)*(DO1(1)+EL2(1))+
*      B2MASS*(R2YCS-R2ZSN)*(DO1(2)+EL2YCS-EL2ZSN)+
*      B3MASS*R3(1)*(DO1(1)+D13(1)+EL3(1))+

```

\* B3MASS\*(R3YCS-R3ZSN)\*(D01(2)\*D13YCS-D13ZSN+EL3YCS-EL3ZSN)\*  
 \* B4MASS\*R4(1)\*(D01(1)\*D14(1)\*EL4(1))\*  
 \* B4MASS\*(R4YCS-R4ZSN)\*(D01(2)\*D14YCS-D14ZSN+EL4YCS-EL4ZSN)

EM(3,4)=BODY11(1,2)\*SINTT1\*BODY11(1,3)\*COSTT1\*  
 \* B1MASS\*D01(1)\*(BMOM\*D01(3)-R1YSN-R1ZCS)\*  
 \* B2MASS\*(D01(1)\*EL2(1))\*(BMOM\*D01(3)-R2YSN-R2ZCS)\*  
 \* B3MASS\*(D01(1)\*D13(1)\*EL3(1))\*(BMOM\*D01(3)-R3YSN-R3ZCS)\*  
 \* B4MASS\*(D01(1)\*D14(1)\*EL4(1))\*(BMOM\*D01(3)-R4YSN-R4ZCS)

EM(3,5)=(B3MASS\*R3(3)\*(-S3(3)\*EL3(2)+S3(2)\*EL3(3))-  
 \* B3MASS\*R3(1)\*(-S3(2)\*EL3(1)+S3(1)\*EL3(2))\*SINTT1\*  
 \* (-B3MASS\*R3(2)\*(-S3(3)\*EL3(2)+S3(2)\*EL3(3))\*  
 \* B3MASS\*R3(1)\*(S3(3)\*EL3(1)-S3(1)\*EL3(3))\*COSTT1

EM(3,6)=(B4MASS\*R4(3)\*(-S4(3)\*EL4(2)+S4(2)\*EL4(3))-  
 \* B4MASS\*R4(1)\*(-S4(2)\*EL4(1)+S4(1)\*EL4(2))\*SINTT1\*  
 \* (-B4MASS\*R4(2)\*(-S4(3)\*EL4(2)+S4(2)\*EL4(3))\*  
 \* B4MASS\*R4(1)\*(S4(3)\*EL4(1)-S4(1)\*EL4(3))\*COSTT1

NOW SET UP THE LOWER HALF OF THE M MATRIX.

DEFINE SOME REOCCURRING TERMS

SR3 = B3MASS\*(D13(2) + EL3(2))  
 SR4 = B3MASS\*(D13(3) + EL3(3))  
 SR5 = B4MASS\*(D14(2) + EL4(2))  
 SR6 = B4MASS\*(D14(3) + EL4(3))  
 SR1=BODY11(1,2)-B2MASS\*EL2(2)\*R2(1)-SR3\*R3(1)-SR5\*R4(1)  
 SR2=BODY11(1,3)-B2MASS\*EL2(3)\*R2(1)-SR4\*R3(1)-SR6\*R4(1)

EM(4,1)=BODY11(1,1)+B2MASS\*(EL2(3)\*R2(3)+EL2(2)\*R2(2))\*  
 \* SR4\*R3(3)+SR3\*R3(2)+SR6\*R4(3)+SR5\*R4(2)

EM(4,2)=SR1\*COSTT1-SR2\*SINTT1

EM(4,3)=SR1\*SINTT1+SR2\*COSTT1

REDEFINE SR1 AND SR2

SR1=BMOM\*(D01(2)\*COSTT1+D01(3)\*SINTT1)  
 SR2=BMOM\*(-D01(2)\*SINTT1+D01(3)\*COSTT1)

EM(4,4) = BODY11(1,1)  
 \* B2MASS\*(EL2(3)\*(R2(3)-SR2) + EL2(2)\*(R2(2) - SR1)) \*  
 \* SR4\*(R3(3)-SR2)+SR3\*(R3(2)-SR1)+SR6\*(R4(3)-SR2)+SR5\*(R4(2)-SR1)

EM(4,5)=B3MASS\*((R3(3)-SR2)\*EL3(3)+(R3(2)-SR1)\*EL3(2))\*S3(1)\*  
 \* (R3(2)-SR1)\*EL3(1)\*S3(2)-((R3(3)-SR2)\*EL3(1)\*S3(3))

EM(4,6)=B4MASS\*((R4(3)-SR2)\*EL4(3)+(R4(2)-SR1)\*EL4(2))\*S4(1)\*  
 \* (R4(2)-SR1)\*EL4(1)\*S4(2)-((R4(3)-SR2)\*EL4(1)\*S4(3))

EM(5,1)=-B3MASS\*EL3(1)\*(R3(2)\*S3(2)+R3(3)\*S3(3))

EM(5,2)=B3MASS\*((EL3(3)\*R3(3)+EL3(1)\*R3(1))\*COSTT1\*  
 \* EL3(3)\*R3YSN)\*S3(2)+(-EL3(2)\*R3ZCS-(EL3(2)\*R3(2)+EL3(1)\*R3(1))\*  
 \* SINTT1)\*S3(3)

EM(5,3)=B3MASS\*((EL3(3)\*R3(3)+EL3(1)\*R3(1))\*SINTT1\*  
 \* EL3(3)\*R3YCS)\*S3(2)+(-EL3(2)\*R3ZSN-(EL3(2)\*R3(2)+EL3(1)\*R3(1))\*  
 \* COSTT1)\*S3(3)

EM(5,4)=B3MASS\*EL3(1)\*((-R3(2)+SR1)\*S3(2)+(-R3(3)+SR2)\*S3(3))

C	EM(5,5)=B3MASS*(1.=B3MASS/TOTMAS)*((EL3(3)**2+EL3(1)**2)*S3(2)-	EMCAL
	* EL3(3)*EL3(2)*S3(3))*S3(2)+((EL3(2)**2+EL3(1)**2)*S3(3)-	EMCAL
	* EL3(2)*EL3(3)*S3(2))*S3(3))	EMCAL
C	EM(5,6)=(B3MASS*B4MASS/TOTMAS)*((-EL3(3)*EL4(3)+EL3(1)*EL4(1))*	EMCAL
	* S4(2)+EL3(3)*EL4(2)*S4(3))*S3(2)+((-EL3(2)*EL4(2)+EL3(1)*EL4(1))*	EMCAL
	* S4(3)+EL3(2)*EL4(3)*S4(2))*S3(3))	EMCAL
C	EM(6,1)=B4MASS*EL4(1)*(R4(2)*S4(2)+R4(3)*S4(3))	EMCAL
C	EM(6,2)=B4MASS*((EL4(3)*R4(3)+EL4(1)*R4(1))*COSTT1+EL4(3)*R4YSN)*	EMCAL
	* S4(2)+(-EL4(2)*R4ZCS-(EL4(2)*R4(2)+EL4(1)*R4(1))*SINTT1)*S4(3))	EMCAL
C	EM(6,3)=B4MASS*((EL4(3)*R4(3)+EL4(1)*R4(1))*SINTT1-EL4(3)*R4YCS)*	EMCAL
	* S4(2)+(-EL4(2)*R4ZSN-(EL4(2)*R4(2)+EL4(1)*R4(1))*COSTT1)*S4(3))	EMCAL
C	EM(6,4)=B4MASS*EL4(1)*((-R4(2)*SR1)*S4(2)+(-R4(3)*SR2)*S4(3))	EMCAL
C	EM(6,5)=(B3MASS*B4MASS/TOTMAS)*((-EL4(3)*EL3(3)+EL4(1)*EL3(1))*	EMCAL
	* S3(2)+EL4(3)*EL3(2)*S3(3))*S4(2)+((-EL4(2)*EL3(2)+EL4(1)*EL3(1))*	EMCAL
	* S3(3)+EL4(2)*EL3(3)*S3(2))*S4(3))	EMCAL
C	EM(6,6)=B4MASS*(1.=B4MASS/TOTMAS)*((EL4(3)**2+EL4(1)**2)*S4(2)-	EMCAL
	* EL4(3)*EL4(2)*S4(3))*S4(2)+((EL4(2)**2+EL4(1)**2)*S4(3)-	EMCAL
	* EL4(2)*EL4(3)*S4(2))*S4(3))	EMCAL
	DO 10 M=1,3	EMCAL
	DO 10 N=1,3	EMCAL
	EM(M,N)=EM(M,N) + EEE(M,N)	EMCAL
10	CONTINUE	EMCAL
	RETURN	EMCAL
C	*****	EMCAL
C	*	
C	*	
C	*	
	END	

SUBROUTINE FOMS(A,B,N,E,TJ)

DIMENSION A(1),B(1),TJ(1)

\*\*\*\*\*

A(1) CONTAINS THE CURRENT TIME. I.E.  $A(1) = \text{TIME}$ . FOMS

A(2) THROUGH A(N) CONTAIN THE INTEGRALS WHERE N EQUALS THE FOMS

NUMBER OF INTEGRALS PLUS 1. FOMS

TJ IS A SCRATCH ARRAY. TJ(1) CONTAINS THE INITIAL DELT AND TJ(2) FOMS

THROUGH TJ(N) CONTAIN THE BACK VALUES OF THE DERIVATIVES. FOMS

B(1) CONTAINS THE CURRENT DELT AND B(2) THROUGH B(N) CONTAIN THE FOMS

CURRENT DERIVATIVES. FOMS

IF E = 0. REINITIALIZE THE DERIVATIVES. FOMS

IF E = 1. CONTINUE THE INTEGRATION. FOMS

FOMS

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\*

IF(N .LE. 1) RETURN FOMS

IF(E .NE. 0.) GO TO 20 FOMS

E = 1. FOMS

DO 10 I=1,N FOMS

TJ(I) = B(I) FOMS

10 CONTINUE FOMS

20 H02 = B(1)\*0.5 FOMS

DO 30 I=2,N FOMS

A(I) = A(I) + H02\*(3\*B(I)-TJ(I)) FOMS

TJ(I) = B(I) FOMS

30 CONTINUE FOMS

A(1) = A(1) + B(1) FOMS

RETURN FOMS

FOMS

\*\*\*\*\*

\*

\*

\*

\*

END

C  
C  
C  
C

## SUBROUTINE GGRAD

```

*
*
*
*****
COMMON      A(3)          ,      AE(5)          ,      AED(5)          ,      COMM
*            AFOUR(2)      ,      AII(6,3,3)      ,      ALT          ,      COMM
*            AIO(6,3,3)    ,      AJ1(3)          ,      AONE(7)       ,      COMM
*            AOCJ(6,3,3)   ,      AOJ(3)          ,      ATWO(4)      ,      COMM
*            ATCPT2(3,3)   ,      ATHREE(5)       ,      COMMC
*            A1(3,3)      ,      A1J(2)          ,      COMMC
COMMON      BDMASS        ,      BFOUR(2)        ,      BMOM          ,      COMM
*            BODYDI(3,3)   ,      BODYOI(3,3)     ,      BODY1I(3,3)   ,      COMM
*            BOMASS        ,      BONE(7)         ,      BTHREE(5)    ,      COMM
*            BTWO(4)       ,      B1MASS          ,      B2MASS      ,      COMM
*            B3MASS        ,      B4MASS          ,      COMMC
COMMON      CA(3)         ,      CB(3)          ,      CGAIN0(3)    ,      COMM
*            CGAIN1(2)     ,      COMMC
*            COSFEJ        ,      COSTTJ         ,      COSTT0      ,      COMM
*            COSTT1        ,      COSTT3         ,      COSTT4      ,      COMM
*            CO2T          ,      CP1            ,      CP2          ,      COMM
*            CST           ,      C1            ,      COMMC
COMMON      DB(3)         ,      DD01(3)        ,      COMMC
*            DELTAT        ,      D01(3)         ,      D01DOT(3)    ,      COMM
*            DTI(3)        ,      COMMC
*            DTIME         ,      D12(3)         ,      D13(3)       ,      COMM
*            D13DOT(3)     ,      D13YCS        ,      D13YSN      ,      COMM
*            D13ZCS        ,      D13ZSN        ,      D14(3)       ,      COMM
*            D14DOT(3)     ,      D14YCS        ,      D14YSN      ,      COMM
*            D14ZCS        ,      D14ZSN        ,      COMMC
COMMON      EEE(3,3)      ,      EEJ(3,3)      ,      EL2(3)       ,      COMM
*            EL2DOT(3)     ,      EL2YCS        ,      EL2YSN      ,      COMM
*            EL2ZCS        ,      EL2ZSN        ,      EL3(3)       ,      COMM
*            EL3DOT(3)     ,      EL3YCS        ,      EL3YSN      ,      COMM
*            EL3ZCS        ,      EL3ZSN        ,      EL4(3)       ,      COMM
*            EL4DOT(3)     ,      EL4YCS        ,      EL4YSN      ,      COMM
*            EL4ZCS        ,      EL4ZSN        ,      EM(6,6)     ,      COMM
COMMON      FAT(8)        ,      COMMC
*            FEE(6)        ,      FEED(6)       ,      FFF(3)       ,      COMM
*            FFJ(3)        ,      FLAG1         ,      FLAG2       ,      COMM
*            FLAG3         ,      FLAG4         ,      FNI          ,      COMM
*            FO(3)         ,      FO1(3)        ,      F02(3)      ,      COMM
*            FO3(3)        ,      F1(3)         ,      F11(3)      ,      COMM
*            FPT(5)        ,      COMMC
*            F12(3)        ,      F13(3)        ,      COMMC
COMMON      GAIN(10)      ,      G3           ,      COMMC
*            G3DOT        ,      G4           ,      G4DOT        ,      COMM
COMMON      H(3)         ,      HCMG(3)      ,      HDOT(3)     ,      COMM
*            HI(3)         ,      HO(3)         ,      HW(6)        ,      COMM
*            H1(3)         ,      H1PDOT(3)     ,      H1PRIM(3)    ,      COMM
*            H3PRIM(3)     ,      H4PRIM(3)     ,      COMMC
COMMON      IB2F          ,      ICFA          ,      ICFB          ,      COMM
*            ICFC          ,      ICFD          ,      IDOCK         ,      COMM
*            IDOF(6)       ,      COMMC
*            IGRAVF        ,      IPNDLM        ,      IPNTCK        ,      COMM
*            IPRINT        ,      IPROFF        ,      COMMC
COMMON      NCASE         ,      NCHECK        ,      NDECK        ,      COMM
*            NGAIN         ,      NUMCMG        ,      COMMC
COMMON      OMEGA1        ,      OMEGA3        ,      OMEGA4       ,      COMM
COMMON      PEND3L        ,      PEND4L        ,      COMMC
COMMON      Q(4,4)        ,      COMMC

```



TQ0G(3) = 3.*C1*(DB(1)*A(2) - DB(2)*A(1))	GGRA
DB(1) = -SINTTO*TIBO(1,1) + COSTTO*TIBO(2,1)	GGRA
DB(2) = COSTT1*(-SINTTO*TIBO(1,2) + COSTTO*TIBO(2,2)) +	GGRA
* SINTT1*(-SINTTO*TIBO(1,3) + COSTTO*TIBO(2,3))	GGRA
DB(3) = -SINTT1*(-SINTTO*TIBO(1,2) + COSTTO*TIBO(2,2)) +	GGRA
* COSTT1*(-SINTTO*TIBO(1,3) + COSTTO*TIBO(2,3))	GGRA
REMP = 0.	GGRA
DO 30 M=1,3	GGRA
REMP = REM + DB(M)*R1(M)	GGRA
30 CONTINUE	GGRA
DO 40 L=1,3	GGRA
F11(L) = C1*B1MASS*(3.*REMP*DB(L) - R1(L))	GGRA
A(L) = 0.	GGRA
DO 40 M=1,3	GGRA
A(L) = A(L) + BODY11(L,M)*DB(M)	GGRA
40 CONTINUE	GGRA
TQ1G(1) = 3.*C1*(DB(2)*A(3) - DB(3)*A(2))	GGRA
TQ1G(2) = 3.*C1*(DB(3)*A(1) - DB(1)*A(3))	GGRA
TQ1G(3) = 3.*C1*(DB(1)*A(2) - DB(2)*A(1))	GGRA
RETURN	GGRA
*****	
*	
*	
*	
END	

C  
C  
C  
C

## SUBROUTINE HCON

```

*
*
*
*****
COMMON      A(3)      ,      AE(5)      ,      AED(5)      ,      COMMC
*            AF0UR(2)  ,      AII(6,3,3) ,      ,      COMMC
*            AIO(6,3,3) ,      AJ1(3)     ,      ALT      ,      COMMC
*            AOCJ(6,3,3) ,      AOJ(3)    ,      AONE(7)   ,      COMMC
*            ATCPT2(3,3) ,      ATHREE(5) ,      ATWO(4)   ,      COMMC
*            A1(3,3)    ,      AIJ(2)     ,      ,      COMMC
COMMON      BDMASS     ,      BFOUR(2)   ,      BMOM      ,      COMMC
*            BODYDI(3,3) ,      BODYOI(3,3) ,      BODY1I(3,3) ,      COMMC
*            BOMASS     ,      BONE(7)    ,      BTHREE(5) ,      COMMC
*            BTWO(4)    ,      B1MASS     ,      B2MASS     ,      COMMC
*            B3MASS     ,      B4MASS     ,      ,      COMMC
COMMON      CA(3)      ,      CB(3)      ,      CGAINO(3)   ,      COMMC
*            CGAIN1(2)  ,      ,      ,      COMMC
*            COSFEJ     ,      COSTTJ     ,      COSTTO     ,      COMMC
*            COSTT1     ,      COSTT3     ,      COSTT4     ,      COMMC
*            CO2T       ,      CP1        ,      CP2        ,      COMMC
*            CST        ,      C1         ,      ,      COMMC
COMMON      DB(3)      ,      DD01(3)    ,      ,      COMMC
*            DELTAT     ,      D01(3)     ,      D01DOT(3)   ,      COMMC
*            DT1(3)     ,      ,      ,      COMMC
*            DTIME      ,      D12(3)     ,      D13(3)     ,      COMMC
*            D13DOT(3)  ,      D13YCS     ,      D13YSN     ,      COMMC
*            D13ZCS     ,      D13ZSN     ,      D14(3)     ,      COMMC
*            D14DOT(3)  ,      D14YCS     ,      D14YSN     ,      COMMC
*            D14ZCS     ,      D14ZSN     ,      ,      COMMC
COMMON      EEE(3,3)   ,      EEJ(3,3)   ,      EL2(3)     ,      COMMC
*            EL2DOT(3)  ,      EL2YCS     ,      EL2YSN     ,      COMMC
*            EL2ZCS     ,      EL2ZSN     ,      EL3(3)     ,      COMMC
*            EL3DOT(3)  ,      EL3YCS     ,      EL3YSN     ,      COMMC
*            EL3ZCS     ,      EL3ZSN     ,      EL4(3)     ,      COMMC
*            EL4DOT(3)  ,      EL4YCS     ,      EL4YSN     ,      COMMC
*            EL4ZCS     ,      EL4ZSN     ,      EM(6,6)    ,      COMMC
COMMON      FAT(8)     ,      ,      ,      COMMC
*            FEE(6)     ,      FEED(6)    ,      FFF(3)     ,      COMMC
*            FFJ(3)     ,      FLAG1     ,      FLAG2     ,      COMMC
*            FLAG3     ,      FLAG4     ,      FNI      ,      COMMC
*            FO(3)      ,      FO1(3)    ,      FO2(3)    ,      COMMC
*            FO3(3)     ,      F1(3)     ,      F11(3)    ,      COMMC
*            FPT(5)     ,      ,      ,      COMMC
*            F12(3)     ,      F13(3)    ,      ,      COMMC
COMMON      GAIN(10)   ,      G3        ,      ,      COMMC
*            G3DOT     ,      G4        ,      G4DOT     ,      COMMC
COMMON      H(3)       ,      HCMG(3)   ,      HDOT(3)    ,      COMMC
*            HI(3)      ,      HO(3)     ,      HW(6)     ,      COMMC
*            H1(3)      ,      H1PDOT(3) ,      H1PRIM(3) ,      COMMC
*            H3PRIM(3)  ,      H4PRIM(3) ,      ,      COMMC
COMMON      IB2F       ,      ICFA      ,      ICFB      ,      COMMC
*            ICFE      ,      ICFD      ,      IDOCK     ,      COMMC
*            IDOF(6)    ,      ,      ,      COMMC
*            IGRAVF     ,      IPNDLM    ,      IPNTCK     ,      COMMC
*            IPRINT     ,      IPROPF    ,      ,      COMMC
COMMON      NCASE      ,      NCHECK     ,      NDECK     ,      COMMC
*            NGAIN      ,      NUMCMG     ,      ,      COMMC

```



COMMON	OMEGA1	,	OMEGA3	,	OMEGA4	COMMON
COMMON	PEND3L	,	PEND4L	,		COMMON
COMMON	Q(4,4)	,				COMMON
COMMON	R	,	R0(3)	,	R1(3)	COMMON
*	R1DOT(3)	,	R1YCS	,	R1YSN	COMMON
*	R1ZCS	,	R1ZSN	,	R2(3)	COMMON
*	R2DOT(3)	,	R2YCS	,	R2YSN	COMMON
*	R2ZCS	,	R2ZSN	,	R3(3)	COMMON
*	R3DOT(3)	,	R3YCS	,	R3YSN	COMMON
*	R3ZCS	,	R3ZSN	,	R4(3)	COMMON
*	R4DOT(3)	,	R4YCS	,	R4YSN	COMMON
*	R4ZCS	,	R4ZSN	,		COMMON
COMMON	S	,	SDOT	,	SINFEJ	COMMON
*	SINTTJ	,	SINTT0	,	SINTT1	COMMON
*	SINTT2	,	SINTT3	,	SINTT4	COMMON
*	SP	,	SUM1	,	SUM2	COMMON
*	SUM3	,	S2(3)	,	S3(3)	COMMON
*	S4(3)	,				COMMON
COMMON	T(3,3)	,	TC(3,3)	,	TEMP1(3)	COMMON
*	TEMP2(3)	,				COMMON
*	TEMP3(3)	,	TEMP4(3)	,	TEMP5(3,3)	COMMON
*	TEMP6(3,3)	,	TEMP7(3,3)	,	TEMP8(3,3)	COMMON
*	TEMP9(3,3)	,	TEMP10(3,3)	,	TEMP11(3,3)	COMMON
*	TEMP12(3,3)	,	TEMP13(3,3)	,	TEMP14(3,3)	COMMON
*	TEMP15(3,3)	,	TERM1(3)	,	TERM2(3)	COMMON
*	TFRICT	,	THATA(6)	,	THATAD(6)	COMMON
*	THETA1	,	THETA3	,	THETA4	COMMON
*	THETO	,	TIBO(3,3)	,	TIBOI(3,3)	COMMON
*	TIME	,	TJ	,	TJ1(10)	COMMON
*	TJ2(10)	,	TJ3(10)	,	TJ4(10)	COMMON
*	TMOTOR	,				COMMON
*	TOEF(3)	,	TOTMAS	,	TO1	COMMON
*	TQOG(3)	,	TQOP(3)	,	TQ1G(3)	COMMON
*	TQ1P(3)	,	TSTART	,	TSTOP	COMMON
*	TT1DOT	,	TT3DOT	,	TT4DOT	COMMON
*	T1EF(3)	,	T13	,	T14	COMMON
COMMON	V(3)	,				COMMON
COMMON	W0(3)	,	WS	,	W1(3)	COMMON
*	W3(3)	,	W4(3)	,		COMMON
COMMON	X(6,7)	,	XC	,	XCDOT	COMMON
*	XMU	,				COMMON

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THATAD(1) = +GAIN(4)\*TIBO(3,2) +GAIN(5)\*W0(1)  
 THATAD(2) = +THATAD(1)  
 CALL CMG  
 RETURN

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## SUBROUTINE PCON

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*****
COMMON  A(3)      ,      AE(5)      ,      AED(5)      ,      COMM
*      AF0UR(2)    ,      AII(6,3,3) ,      ,      COMM
*      AIO(6,3,3)  ,      AJ1(3)     ,      ALIT      ,      COMM
*      AOCJ(6,3,3) ,      AOJ(3)     ,      AONE(7)   ,      COMM
*      ATCPT2(3,3) ,      ATHREE(5)  ,      ATWO(4)   ,      COMM
*      A1(3,3)     ,      A1J(2)     ,      ,      COMM
COMMON  BDMASS     ,      BFOUR(2)   ,      BMDM      ,      COMM
*      BODYDI(3,3) ,      BODYOI(3,3) ,      BODY1I(3,3) ,      COMM
*      BOMASS      ,      BONE(7)    ,      BTHREE(5) ,      COMM
*      BTWO(4)     ,      B1MASS     ,      B2MASS     ,      COMM
*      B3MASS      ,      B4MASS     ,      ,      COMM
COMMON  CA(3)      ,      CB(3)      ,      CGAIN0(3)   ,      COMM
*      CGAIN1(2)   ,      ,      ,      COMM
*      COSFEJ      ,      COSTTJ     ,      COSTT0     ,      COMM
*      COSTT1      ,      COSTT3     ,      COSTT4     ,      COMM
*      C02T        ,      CP1        ,      CP2        ,      COMM
*      CST         ,      C1         ,      ,      COMM
COMMON  DB(3)      ,      DD01(3)   ,      ,      COMM
*      DELTAT      ,      D01(3)     ,      D01DOT(3)   ,      COMM
*      DTI(3)      ,      ,      ,      COMM
*      DTIME       ,      D12(3)     ,      D13(3)     ,      COMM
*      D13DOT(3)   ,      D13YCS     ,      D13YSN     ,      COMM
*      D13ZCS      ,      D13ZSN     ,      D14(3)     ,      COMM
*      D14DOT(3)   ,      D14YCS     ,      D14YSN     ,      COMM
*      D14ZCS      ,      D14ZSN     ,      ,      COMM
COMMON  EEE(3,3)   ,      EEJ(3,3)   ,      EL2(3)     ,      COMM
*      EL2DOT(3)   ,      EL2YCS     ,      EL2YSN     ,      COMM
*      EL2ZCS      ,      EL2ZSN     ,      EL3(3)     ,      COMM
*      EL3DOT(3)   ,      EL3YCS     ,      EL3YSN     ,      COMM
*      EL3ZCS      ,      EL3ZSN     ,      EL4(3)     ,      COMM
*      EL4DOT(3)   ,      EL4YCS     ,      EL4YSN     ,      COMM
*      EL4ZCS      ,      EL4ZSN     ,      EM(6,6)    ,      COMM
COMMON  FAT(8)     ,      ,      ,      COMM
*      FEE(6)      ,      FEED(6)    ,      FFF(3)     ,      COMM
*      FFJ(3)      ,      FLAG1      ,      FLAG2     ,      COMM
*      FLAG3       ,      FLAG4      ,      ENI        ,      COMM
*      FO(3)        ,      FO1(3)     ,      F02(3)     ,      COMM
*      F03(3)      ,      F1(3)      ,      F11(3)     ,      COMM
*      FPT(5)      ,      ,      ,      COMM
*      F12(3)      ,      F13(3)     ,      ,      COMM
COMMON  GAIN(10)   ,      G3         ,      ,      COMM
*      G3DOT       ,      G4         ,      G4DOT     ,      COMM
COMMON  H(3)       ,      HCMG(3)    ,      HDOT(3)    ,      COMM
*      HI(3)       ,      HO(3)      ,      HW(6)      ,      COMM
*      H1(3)       ,      H1PDOT(3)  ,      H1PRIM(3)  ,      COMM
*      H3PRIM(3)   ,      H4PRIM(3)  ,      ,      COMM
COMMON  IB2F       ,      ICFA       ,      ICFB       ,      COMM
*      ICFC        ,      ICFD       ,      IDOCK      ,      COMM
*      IDOF(6)     ,      ,      ,      COMM
*      IGRAVF      ,      IPNDLM     ,      IPNTCK     ,      COMM
*      IPRINT      ,      IPROPF     ,      ,      COMM
COMMON  NCASE      ,      NCHECK     ,      NDECK     ,      COMM
*      NGAIN       ,      NUMCMG     ,      ,      COMM
COMMON  OMEGA1     ,      OMEGA3     ,      OMEGA4     ,      COMM
COMMON  PEND3L     ,      PEND4L     ,      ,      COMM
COMMON  Q(4,4)     ,      ,      ,      COMM

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COMMON	R		RO(3)		R1(3)	COMMON
*	R1DOT(3)		R1YCS		R1YSN	COMMON
*	R1ZCS		R1ZSN		R2(3)	COMMON
*	R2DOT(3)		R2YCS		R2YSN	COMMON
*	R2ZCS		R2ZSN		R3(3)	COMMON
*	R3DOT(3)		R3YCS		R3YSN	COMMON
*	R3ZCS		R3ZSN		R4(3)	COMMON
*	R4DOT(3)		R4YCS		R4YSN	COMMON
*	R4ZCS		R4ZSN			COMMON
COMMON	S		SDOT		SINFEJ	COMMON
*	SINTTJ		SINTT0		SINTT1	COMMON
*	SINTT2		SINTT3		SINTT4	COMMON
*	SP		SUM1		SUM2	COMMON
*	SUM3		S2(3)		S3(3)	COMMON
*	S4(3)					COMMON
COMMON	T(3,3)		TC(3,3)		TEMP1(3)	COMMON
*	TEMP2(3)					COMMON
*	TEMP3(3)		TEMP4(3)		TEMP5(3,3)	COMMON
*	TEMP6(3,3)		TEMP7(3,3)		TEMP8(3,3)	COMMON
*	TEMP9(3,3)		TEMP10(3,3)		TEMP11(3,3)	COMMON
*	TEMP12(3,3)		TEMP13(3,3)		TEMP14(3,3)	COMMON
*	TEMP15(3,3)		TERM1(3)		TERM2(3)	COMMON
*	TRICT		THATA(6)		THATA0(6)	COMMON
*	THETA1		THETA3		THETA4	COMMON
*	THETO		TIBO(3,3)		TIBO1(3,3)	COMMON
*	TIME		TJ		TJ1(10)	COMMON
*	TJ2(10)		TJ3(10)		TJ4(10)	COMMON
*	TMOTOR					COMMON
*	TOEF(3)		TOTMAS		TO1	COMMON
*	TQOG(3)		TQOP(3)		TQ1G(3)	COMMON
*	TQ1P(3)		TSTART		TSTOP	COMMON
*	TT1DOT		TT3DOT		TT4DOT	COMMON
*	TIEF(3)		T13		T14	COMMON
COMMON	V(3)					COMMON
COMMON	W0(3)		WS		W1(3)	COMMON
*	W3(3)		W4(3)			COMMON
COMMON	X(6,7)		XC		XCDOT	COMMON
*	XMU					COMMON

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SINTT1 = SIN(THETA1)

COSTT1 = COS(THETA1)

DO 30 M=1,3

FS = CGAIN0(M)\*W0(M)

FPT(M) = 2.\*ABS(FS)

TQOP(M) = FS\*AOJ(M)

30 CONTINUE

FS = 0.

IF (COSTT1 .GT. 0.87) FS = CGAIN1(2)\*W0(2)

IF (COSTT1 .LT. -0.87) FS = -CGAIN1(2)\*W0(2)

IF (SINTT1 .GT. 0.87) FS = CGAIN1(2)\*W0(3)

IF (SINTT1 .LT. -0.87) FS = -CGAIN1(2)\*W0(3)

FPT(4) = 2.\*ABS(FS)

TQ1P(2) = FS\*AIJ(2)

FS = CGAIN1(1)\*(OMEGA1 - SP)

FPT(5) = 2.\*ABS(FS)

TQ1P(1) = FS\*AIJ(1)

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# SUBROUTINE RECALC

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COMMON
*      A(3)          *      AE(5)          *      AED(5)          *      COMMC
*      AF0UR(2)      *      AI1(6,3,3)      *      ALT            *      COMMC
*      A10(6,3,3)    *      AJ1(3)          *      AONE(7)        *      COMMC
*      AOCJ(6,3,3)   *      AOJ(3)          *      ATWO(4)        *      COMMC
*      ATCPT2(3,3)   *      ATHREE(5)       *      B1J(2)         *      COMMC
*      A1(3,3)       *      BFOUR(2)        *      BMOM           *      COMMC
COMMON
*      BDMASS        *      BODYO1(3,3)     *      BODY11(3,3)   *      COMMC
*      BOMASS        *      BONE(7)         *      BTHREE(5)     *      COMMC
*      BTWO(4)       *      B1MASS          *      B2MASS        *      COMMC
*      B3MASS        *      B4MASS          *      CGAINO(3)     *      COMMC
COMMON
*      CA(3)         *      CB(3)           *      COSTTJ        *      COMMC
*      CGAIN1(2)     *      COSTT3          *      COSTT4        *      COMMC
*      COSFEJ        *      CP1             *      CP2            *      COMMC
*      COSTT1        *      C1              *      DD01(3)       *      COMMC
COMMON
*      DB(3)         *      D01(3)          *      D01DOT(3)     *      COMMC
*      DELTAT        *      D12(3)          *      D13(3)        *      COMMC
*      DTI(3)        *      D13YCS          *      D13YSN        *      COMMC
*      DTIME         *      D13ZSN          *      D14(3)        *      COMMC
*      D13DOT(3)     *      D14YCS          *      D14YSN        *      COMMC
*      D13ZCS        *      D14ZSN          *      EEJ(3,3)      *      COMMC
COMMON
*      D14DOT(3)     *      EEJ(3,3)        *      EL2(3)         *      COMMC
*      D14ZCS        *      EL2YCS          *      EL2YSN        *      COMMC
*      EEE(3,3)      *      EL2ZSN          *      EL3(3)         *      COMMC
*      EL2DOT(3)     *      EL3YCS          *      EL3YSN        *      COMMC
*      EL2ZCS        *      EL3ZSN          *      EL4(3)         *      COMMC
*      EL3DOT(3)     *      EL4YCS          *      EL4YSN        *      COMMC
*      EL3ZCS        *      EL4ZSN          *      EM(6,6)       *      COMMC
COMMON
*      EL4DOT(3)     *      FEED(6)         *      FFF(3)        *      COMMC
*      EL4ZCS        *      FLAG1           *      FLAG2         *      COMMC
*      FAT(8)        *      FLAG4           *      FN            *      COMMC
*      FEE(6)        *      F01(3)          *      F02(3)        *      COMMC
*      FFJ(3)        *      F1(3)           *      F11(3)        *      COMMC
*      FLAG3         *      F13(3)          *      G3            *      COMMC
*      F0(3)         *      G4              *      G4DOT          *      COMMC
*      F03(3)        *      HCMG(3)         *      HDOT(3)       *      COMMC
*      FPT(5)        *      HO(3)           *      HW(6)         *      COMMC
*      F12(3)        *      H1PDOT(3)       *      H1PRIM(3)     *      COMMC
COMMON
*      GAIN(10)      *      H4PRIM(3)       *      ICFA          *      COMMC
*      G3DOT         *      ICFD            *      ICFB          *      COMMC
COMMON
*      H(3)          *      IPNDLM          *      IDOCK         *      COMMC
*      HI(3)         *      IPROPF          *      IPNTCK        *      COMMC
*      H1(3)         *      NCHECK          *      NDECK         *      COMMC
*      H3PRIM(3)     *      NUMCMG          *      OMEGA4        *      COMMC
COMMON
*      IB2F          *      OMEGA3          *      PEND4L        *      COMMC
*      ICFC          *      PEND4L          *      Q(4,6)        *      COMMC
*      IDOF(6)       *
*      IGRAVF        *
*      IPRINT        *
COMMON
*      NCASE         *
*      NGAIN         *
COMMON
*      OMEGA1        *
COMMON
*      PEND3L        *
COMMON
*      Q(4,6)

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COMMON	R	,	R0(3)	,	R1(3)	,	COMMC
*	R1DOT(3)	,	R1YCS	,	R1YSN	,	COMMC
*	R1ZCS	,	R1ZSN	,	R2(3)	,	COMMC
*	R2DOT(3)	,	R2YCS	,	R2YSN	,	COMMC
*	R2ZCS	,	R2ZSN	,	R3(3)	,	COMMC
*	R3DOT(3)	,	R3YCS	,	R3YSN	,	COMMC
*	R3ZCS	,	R3ZSN	,	R4(3)	,	COMMC
*	R4DOT(3)	,	R4YCS	,	R4YSN	,	COMMC
*	R4ZCS	,	R4ZSN	,		,	COMMC
COMMON	S	,	SDOT	,	SINFEJ	,	COMMC
*	SINTTJ	,	SINTT0	,	SINTT1	,	COMMC
*	SINTT2	,	SINTT3	,	SINTT4	,	COMMC
*	SP	,	SUM1	,	SUM2	,	COMMC
*	SUM3	,	S2(3)	,	S3(3)	,	COMMC
*	S4(3)	,		,		,	COMMC
COMMON	T(3,3)	,	TC(3,3)	,	TEMP1(3)	,	COMMC
*	TEMP2(3)	,		,		,	COMMC
*	TEMP3(3)	,	TEMP4(3)	,	TEMP5(3,3)	,	COMMC
*	TEMP6(3,3)	,	TEMP7(3,3)	,	TEMP8(3,3)	,	COMMC
*	TEMP9(3,3)	,	TEMP10(3,3)	,	TEMP11(3,3)	,	COMMC
*	TEMP12(3,3)	,	TEMP13(3,3)	,	TEMP14(3,3)	,	COMMC
*	TEMP15(3,3)	,	TERM1(3)	,	TERM2(3)	,	COMMC
*	TFRICT	,	THATA(6)	,	THATA(6)	,	COMMC
*	THETA1	,	THETA3	,	THETA4	,	COMMC
*	THETO	,	TIBO(3,3)	,	TIBOI(3,3)	,	COMMC
*	TIME	,	TJ	,	TJ1(10)	,	COMMC
*	TJ2(10)	,	TJ3(10)	,	TJ4(10)	,	COMMC
*	TMOTOR	,		,		,	COMMC
*	TOEF(3)	,	TOTMAS	,	TO1	,	COMMC
*	TQOG(3)	,	TQOP(3)	,	TQ1G(3)	,	COMMC
*	TQ1P(3)	,	TSTART	,	TSTOP	,	COMMC
*	TT1DOT	,	TT3DOT	,	TT4DOT	,	COMMC
*	T1EF(3)	,	T13	,	T14	,	COMMC
COMMON	V(3)	,		,		,	COMMC
COMMON	W0(3)	,	WS	,	W1(3)	,	COMMC
*	W3(3)	,	W4(3)	,		,	COMMC
COMMON	X(6,7)	,	XC	,	XCDOT	,	COMMC
*	XMU	,		,		,	COMMC

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SINTT1 = SIN(THETA1)	RECAL
COSTT1 = COS(THETA1)	RECAL
CALL SCALC	RECAL
EL2(1) = D12(1) + S*S2(1)	RECAL
EL2(2) = D12(2) + S*S2(2)	RECAL
EL2(3) = D12(3) + S*S2(3)	RECAL
SINTT3 = SIN(THETA3)	RECAL
COSTT3 = COS(THETA3)	RECAL
EL3(1) = PEND3L*SINTT3	RECAL
EL3(2) = -PEND3L*COSTT3*S3(3)	RECAL
EL3(3) = -PEND3L*COSTT3*S3(2)	RECAL
SINTT4 = SIN(THETA4)	RECAL
COSTT4 = COS(THETA4)	RECAL
EL4(1) = -PEND4L*SINTT4	RECAL
EL4(2) = -PEND4L*COSTT4*S4(3)	RECAL
EL4(3) = -PEND4L*COSTT4*S4(2)	RECAL
R1(1) = (BOMASS/TOTMAS)*D01(1)	RECAL

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*      = (B2MASS/TOTMAS)*EL2(1) - (B3MASS/TOTMAS)*(D13(1) + EL3(1)) RECAL
*      = (B4MASS/TOTMAS)*(D14(1) + EL4(1)) RECAL
R1(2) = (B0MASS/TOTMAS)*(D01(2)*COSTT1 + D01(3)*SINTT1) RECAL
*      = (B2MASS/TOTMAS)*EL2(2) RECAL
*      = (B3MASS/TOTMAS)*(D13(2) + EL3(2)) RECAL
*      = (B4MASS/TOTMAS)*(D14(2) + EL4(2)) RECAL
R1(3) = (B0MASS/TOTMAS)*(-D01(2)*SINTT1 + D01(3)*COSTT1) RECAL
*      = (B2MASS/TOTMAS)*EL2(3) RECAL
*      = (B3MASS/TOTMAS)*(D13(3) + EL3(3)) RECAL
*      = (B4MASS/TOTMAS)*(D14(3) + EL4(3)) RECAL
R2(1) = R1(1) + EL2(1) RECAL
R2(2) = R1(2) + EL2(2) RECAL
R2(3) = R1(3) + EL2(3) RECAL
R3(1) = R1(1) + D13(1) + EL3(1) RECAL
R3(2) = R1(2) + D13(2) + EL3(2) RECAL
R3(3) = R1(3) + D13(3) + EL3(3) RECAL
R4(1) = R1(1) + D14(1) + EL4(1) RECAL
R4(2) = R1(2) + D14(2) + EL4(2) RECAL
R4(3) = R1(3) + D14(3) + EL4(3) RECAL
RETURN RECAL
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*
*
END

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## SUBROUTINE SCALC

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*****
COMMON      A(3)          ,      AE(5)          ,      AED(5)          ,      COMM
*            AF0UR(2)      ,      AII(6,3,3)     ,      ALIT          ,      COMM
*            AIO(6,3,3)    ,      AJI(3)         ,      AONE(7)       ,      COMM
*            AOCJ(6,3,3)   ,      AOJ(3)        ,      ATWO(4)      ,      COMM
*            ATCPT2(3,3)   ,      ATHREE(5)     ,      B0MOM        ,      COMM
*            A1(3,3)       ,      A1J(2)        ,      B0DY1I(3,3)   ,      COMM
COMMON      BDMASS        ,      BFOUR(2)       ,      BTHREE(5)    ,      COMM
*            BODYDI(3,3)   ,      BODYOI(3,3)    ,      B2MASS      ,      COMM
*            BOMASS        ,      BONE(7)       ,      B4MASS      ,      COMM
*            BTWO(4)       ,      B1MASS        ,      CGAINO(3)    ,      COMM
*            B3MASS        ,      B4MASS        ,      COMM
COMMON      CA(3)         ,      CB(3)         ,      COMM
*            CGAINI(2)     ,      COSTTJ      ,      COSTT0      ,      COMM
*            COSFEJ        ,      COSTT3      ,      COSTT4      ,      COMM
*            COSTT1        ,      CP1         ,      CP2         ,      COMM
*            CO2T          ,      C1          ,      COMM
COMMON      DB(3)         ,      DD01(3)     ,      DD1DOT(3)   ,      COMM
*            DELTAT        ,      D01(3)      ,      COMM
*            DTI(3)        ,      D12(3)      ,      D13(3)      ,      COMM
*            DTIME         ,      D13YCS      ,      D13YSN      ,      COMM
*            D13DOT(3)     ,      D13ZSN      ,      D14(3)      ,      COMM
*            D13ZCS        ,      D14YCS      ,      D14YSN      ,      COMM
*            D14DOT(3)     ,      D14ZSN      ,      COMM
*            D14ZCS        ,      EEJ(3,3)    ,      EL2(3)      ,      COMM
COMMON      EEE(3,3)      ,      EL2YCS      ,      EL2YSN      ,      COMM
*            EL2DOT(3)     ,      EL2ZSN      ,      EL3(3)      ,      COMM
*            EL2ZCS        ,      EL3YCS      ,      EL3YSN      ,      COMM
*            EL3DOT(3)     ,      EL3ZSN      ,      EL4(3)      ,      COMM
*            EL3ZCS        ,      EL4YCS      ,      EL4YSN      ,      COMM
*            EL4DOT(3)     ,      EL4ZSN      ,      EM(6,6)     ,      COMM
*            EL4ZCS        ,      FEED(6)     ,      FFF(3)      ,      COMM
COMMON      FAT(8)        ,      FLAG1      ,      FLAG2      ,      COMM
*            FEE(6)        ,      FLAG4      ,      FNI         ,      COMM
*            FFJ(3)        ,      F01(3)     ,      F02(3)     ,      COMM
*            FLAG3         ,      F1(3)      ,      F11(3)     ,      COMM
*            F0(3)         ,      F13(3)     ,      COMM
*            F03(3)        ,      G3          ,      G4DOT      ,      COMM
*            FPT(5)        ,      G4         ,      HDOT(3)     ,      COMM
COMMON      F12(3)        ,      HCMG(3)    ,      HW(6)       ,      COMM
*            GAIN(10)      ,      H0(3)      ,      H1PRIM(3)   ,      COMM
*            G3DOT        ,      H1PDOT(3)  ,      H4PRIM(3)   ,      COMM
COMMON      H(3)          ,      H4PRIM(3)  ,      COMM
*            HI(3)         ,      ICFA        ,      ICFB        ,      COMM
*            H1(3)         ,      ICFD        ,      IDOCK       ,      COMM
*            H3PRIM(3)     ,      IPNDLM      ,      IPNTCK      ,      COMM
COMMON      IB2F          ,      IPROPF      ,      COMM
*            ICFC          ,      NCHECK      ,      NDECK      ,      COMM
*            IDOF(6)       ,      NUMCMG      ,      COMM
*            IGRAVF        ,      OMEGA3      ,      OMEGA4      ,      COMM
COMMON      IPRINT        ,      COMM
*            NCASE         ,      PEND4L      ,      COMM
COMMON      NGAIN         ,      COMM
*            OMEGA1        ,      COMM
COMMON      PEND3L        ,      COMM
COMMON      Q(4,4)        ,      COMM

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COMMON	R	°	RO(3)	°	R1(3)	°	COMM
*	R1DOT(3)	°	R1YCS	°	R1YSN	°	COMM
*	R1ZCS	°	R1ZSN	°	R2(3)	°	COMM
*	R2DOT(3)	°	R2YCS	°	R2YSN	°	COMM
*	R2ZCS	°	R2ZSN	°	R3(3)	°	COMM
*	R3DOT(3)	°	R3YCS	°	R3YSN	°	COMM
*	R3ZCS	°	R3ZSN	°	R4(3)	°	COMM
*	R4DOT(3)	°	R4YCS	°	R4YSN	°	COMM
*	R4ZCS	°	R4ZSN	°			COMM
COMMON	S	°	SDOT	°	SINFEJ	°	COMM
*	SINTTJ	°	SINTTIO	°	SINTT1	°	COMM
*	SINTT2	°	SINTT3	°	SINTT4	°	COMM
*	SP	°	SUM1	°	SUM2	°	COMM
*	SUM3	°	S2(3)	°	S3(3)	°	COMM
*	S4(3)	°					COMM
COMMON	T(3,3)	°	TC(3,3)	°	TEMP1(3)	°	COMM
*	TEMP2(3)	°					COMM
*	TEMP3(3)	°	TEMP4(3)	°	TEMP5(3,3)	°	COMM
*	TEMP6(3,3)	°	TEMP7(3,3)	°	TEMP8(3,3)	°	COMM
*	TEMP9(3,3)	°	TEMP10(3,3)	°	TEMP11(3,3)	°	COMM
*	TEMP12(3,3)	°	TEMP13(3,3)	°	TEMP14(3,3)	°	COMM
*	TEMP15(3,3)	°	TERM1(3)	°	TERM2(3)	°	COMM
*	TFRIC	°	THATA(6)	°	THATA(6)	°	COMM
*	THETA1	°	THETA3	°	THETA4	°	COMM
*	THETO	°	TIBO(3,3)	°	TIBOI(3,3)	°	COMM
*	TIME	°	TJ	°	TJ1(10)	°	COMM
*	TJ2(10)	°	TJ3(10)	°	TJ4(10)	°	COMM
*	TMOTOR	°					COMM
*	TOEF(3)	°	TOTMAS	°	TO1	°	COMM
*	TQOG(3)	°	TQOP(3)	°	TQ1G(3)	°	COMM
*	TQ1P(3)	°	TSTART	°	TSTOP	°	COMM
*	TT1DOT	°	TT3DOT	°	TT4DOT	°	COMM
*	T1EF(3)	°	T13	°	T14	°	COMM
COMMON	V(3)	°					COMM
COMMON	W0(3)	°	WS	°	W1(3)	°	COMM
*	W3(3)	°	W4(3)	°			COMM
COMMON	X(6,7)	°	XC	°	XCDOT	°	COMM
*	XMU	°					COMM

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END

## SUBROUTINE SDCALC

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*****
COMMON      A(3)          ,      AE(5)          ,      AED(5)          ,      COMM
*            AF0UR(2)      ,      AII(6,3,3)     ,      ALI              ,      COMM
*            AIO(6,3,3)    ,      AJ1(3)         ,      ADNE(7)         ,      COMM
*            AOCJ(6,3,3)   ,      AOJ(3)         ,      ATWO(4)         ,      COMM
*            ATCPT2(3,3)   ,      ATHREE(5)      ,      A1J(2)         ,      COMM
*            A1(3,3)       ,      BFOUR(2)       ,      BMDM           ,      COMM
COMMON      BDMASS        ,      BODYOI(3,3)    ,      BODY1I(3,3)    ,      COMM
*            BOMASS        ,      BONE(7)        ,      BTHREE(5)      ,      COMM
*            BTWO(4)       ,      B1MASS         ,      B2MASS         ,      COMM
*            B3MASS        ,      B4MASS         ,      CGAINO(3)       ,      COMM
COMMON      CA(3)         ,      CB(3)         ,      CGAIN1(2)      ,      COMM
*            CGAIN1(2)     ,      COSTTJ        ,      COSTTO         ,      COMM
*            COSFEJ        ,      COSTT3        ,      COSTT4         ,      COMM
*            COSTT1        ,      CP1           ,      CP2            ,      COMM
*            C02T          ,      C1            ,      DB(3)          ,      COMM
COMMON      DB(3)         ,      DD01(3)       ,      DD01DOT(3)     ,      COMM
*            DELTAT        ,      D01(3)        ,      D12(3)         ,      COMM
*            DTI(3)        ,      D13YCS        ,      D13YSN         ,      COMM
*            DTIME         ,      D13ZSN        ,      D14(3)          ,      COMM
*            D13DOT(3)     ,      D14YCS        ,      D14YSN         ,      COMM
*            D13ZCS        ,      D14ZSN        ,      EEJ(3,3)       ,      COMM
COMMON      EEJ(3,3)     ,      EL2(3)        ,      EL2YCS         ,      COMM
*            EL2DOT(3)     ,      EL2ZSN        ,      EL3(3)          ,      COMM
*            EL2ZCS        ,      EL3YCS        ,      EL3YSN         ,      COMM
*            EL3DOT(3)     ,      EL3ZSN        ,      EL4(3)          ,      COMM
*            EL3ZCS        ,      EL4YCS        ,      EL4YSN         ,      COMM
*            EL4DOT(3)     ,      EL4ZSN        ,      EM(6,6)        ,      COMM
COMMON      EL4ZCS        ,      FEED(6)       ,      FFF(3)         ,      COMM
*            FAT(8)        ,      FLAG1         ,      FLAG2          ,      COMM
*            FEE(6)        ,      FLAG4         ,      FNI            ,      COMM
*            FFJ(3)        ,      F01(3)        ,      F02(3)         ,      COMM
*            FLAG3         ,      F1(3)         ,      F11(3)         ,      COMM
*            F0(3)         ,      F13(3)        ,      G3              ,      COMM
*            F03(3)        ,      G4            ,      G4DOT           ,      COMM
COMMON      F12(3)       ,      H(3)          ,      HCDOT(3)        ,      COMM
*            F13(3)       ,      H1(3)         ,      HW(6)           ,      COMM
*            GAIN(10)      ,      H1DOT(3)      ,      H1PRIM(3)       ,      COMM
*            G3DOT        ,      H4PRIM(3)     ,      IB2F            ,      COMM
COMMON      H(3)         ,      ICFA          ,      ICFB            ,      COMM
*            H1(3)         ,      ICFD          ,      IDOCK           ,      COMM
*            H1DOT(3)      ,      IPNDLM        ,      IPNTCK          ,      COMM
*            H3PRIM(3)     ,      IPRPF         ,      NCHECK          ,      COMM
COMMON      IB2F         ,      IPNDLM        ,      NDECK           ,      COMM
*            ICFB         ,      IPRPF         ,      OMEGA1          ,      COMM
*            ICFD         ,      NCHECK        ,      OMEGA3          ,      COMM
*            IDOF(6)       ,      NUMCMG        ,      OMEGA4          ,      COMM
*            IGRAVF        ,      OMEGA3         ,      PEND3L          ,      COMM
COMMON      IPRINT       ,      PEND4L         ,      Q(4,4)          ,      COMM
*            NCASE         ,      Q(4,4)         ,
COMMON      NGAIN        ,
COMMON      OMEGA1       ,
COMMON      PEND3L      ,
COMMON      Q(4,4)

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COMMON	R	,	R0(3)	,	R1(3)	,	COMMC
*	R1DOT(3)	,	R1YCS	,	R1YSN	,	COMMC
*	R1ZCS	,	R1ZSN	,	R2(3)	,	COMMC
*	R2DOT(3)	,	R2YCS	,	R2YSN	,	COMMC
*	R2ZCS	,	R2ZSN	,	R3(3)	,	COMMC
*	R3DOT(3)	,	R3YCS	,	R3YSN	,	COMMC
*	R3ZCS	,	R3ZSN	,	R4(3)	,	COMMC
*	R4DOT(3)	,	R4YCS	,	R4YSN	,	COMMC
*	R4ZCS	,	R4ZSN	,			COMMC
COMMON	S	,	SDOT	,	SINFEJ	,	COMMC
*	SINTTJ	,	SINTTO	,	SINTT1	,	COMMC
*	SINTT2	,	SINTT3	,	SINTT4	,	COMMC
*	SP	,	SUM1	,	SUM2	,	COMMC
*	SUM3	,	S2(3)	,	S3(3)	,	COMMC
*	S4(3)	,					COMMC
COMMON	T(3,3)	,	TC(3,3)	,	TEMP1(3)	,	COMMC
*	TEMP2(3)	,					COMMC
*	TEMP3(3)	,	TEMP4(3)	,	TEMP5(3,3)	,	COMMC
*	TEMP6(3,3)	,	TEMP7(3,3)	,	TEMP8(3,3)	,	COMMC
*	TEMP9(3,3)	,	TEMP10(3,3)	,	TEMP11(3,3)	,	COMMC
*	TEMP12(3,3)	,	TEMP13(3,3)	,	TEMP14(3,3)	,	COMMC
*	TEMP15(3,3)	,	TERM1(3)	,	TERM2(3)	,	COMMC
*	TFRICT	,	THATA(6)	,	THATAAD(6)	,	COMMC
*	THETA1	,	THETA3	,	THETA4	,	COMMC
*	THETO	,	TIBO(3,3)	,	TIBOI(3,3)	,	COMMC
*	TIME	,	TJ	,	TJ1(10)	,	COMMC
*	TJ2(10)	,	TJ3(10)	,	TJ4(10)	,	COMMC
*	TMOTOR	,					COMMC
*	TOEF(3)	,	TOTMAS	,	T01	,	COMMC
*	TQOG(3)	,	TQOP(3)	,	TQ1G(3)	,	COMMC
*	TQ1P(3)	,	TSTART	,	TSTOP	,	COMMC
*	TT1DOT	,	TT3DOT	,	TT4DOT	,	COMMC
*	T1EF(3)	,	T13	,	T14	,	COMMC
COMMON	V(3)	,					COMMC
COMMON	W0(3)	,	WS	,	W1(3)	,	COMMC
*	W3(3)	,	W4(3)	,			COMMC
COMMON	X(6,7)	,	XC	,	XCDOT	,	COMMC
*	XMU	,					COMMC

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THIS SUBROUTINE CALCULATES THE ELEVATOR VELOCITY.

SDOT = 0.

RETURN

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END

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C
SUBROUTINE SYEQNS(A,N,NR,NC,FLAG)
*
*
*
*****
*
      LINEAR SIMULTANEOUS EQUATIONS
      A   AUGMENTED MATRIX (AC)   WHERE   AX = C
      ORIGINAL DATA DESTROYED
      N   NUMBER OF EQUATIONS
      SOLUTION X WILL BE COLUMN N+1 OF MATRIX A
      FLAG = 0.   SOLUTION EXIST   F= 1.0 NO SOLUTION
DIMENSION A(NR,NC)
N1 = N
N2 = N1+1
N0 = N1 -1
FLAG = 0.
DO 60 I =1,N1
M = I
MI = M
IF(MI =N1)2,12,2
2 DO 10 II =M,N0
IF( ABS(A(MI,M))= ABS(A(II+1,M))) 5,10,10
C FIND LARGEST ABSOLUTE VALUE COLUMN M.. CALL IT BIG
5 MI = II+ 1
10 CONTINUE
12 BIG = A(MI,M)
IF( BIG )15,100,15
C BIG = 0 IMPLIES THERE IS NO SOLUTION
15 IF(MI= M)18,25,18
18 DO 20 JJ =M,N2
TEMP =A(M,JJ)
A(M,JJ) = A(MI,JJ)/BIG
C NORMALIZE ROW MI AND EXCHANGE WITH ROW M
20 A(MI,JJ)= TEMP
GO TO 35
25 DO 30 JJ=M,N2
C NORMALIZE ROW M
30 A(M,JJ) =A(M,JJ)/BIG
35 DO 50 II = 1,N1
C DO ROW OPERATIONS TO ZERO ELEMENTS OF COLUMN M EXCEPT FOR
C ELEMENT A(M,M)
TEMP =A(II,M)
IF(M=II)38,50,38
38 IF(TEMP) 39,50,39
39 DO 40 JJ= M,N2
A(II,JJ)=A(II,JJ)- TEMP *A(M,JJ)
40 CONTINUE
50 CONTINUE
60 CONTINUE
70 RETURN
C READ SOLUTION AS N ELEMENTS FROM COLUMN (N+1)
100 FLAG =1.0
C SORRY THE COEFFICIENT MATRIX IS SINGULAR
RETURN
*
*****
*
*
*
END

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## SUBROUTINE TORK01

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COMMON A(3)          AE(5)          AED(5)          COMM
      AF0UR(2)        AII(6,3,3)      ALIT          COMM
      AIO(6,3,3)      AOJ(3)          AONE(7)        COMM
      AOCJ(6,3,3)     ATHREE(5)       ATHO(4)        COMM
      ATCPT2(3,3)     A1J(2)          COMM
      A1(3,3)         BFOUR(2)        BMM          COMM
COMMON BDMASS         BODYO1(3,3)     BODY1I(3,3)   COMM
      BOMASS          BONE(7)         BTHREE(5)     COMM
      BTWO(4)         B1MASS          B2MASS         COMM
      B3MASS          B4MASS          COMM
COMMON CA(3)          CB(3)          CGAINO(3)        COMM
      CGAIN1(2)       COSTTJ          COSTTO        COMM
      COSFEJ          COSTT3          COSTT4        COMM
      COSTT1          CP1             CP2            COMM
      CO2T            CI             COMM
COMMON DB(3)          DD01(3)         DD1DOT(3)      COMM
      DELTAT          DO1(3)          COMM
      DTI(3)          D12(3)          D13(3)         COMM
      DTIME           D13YCS          D13YSN        COMM
      D13DOT(3)       D13ZSN          D14(3)         COMM
      D13ZCS          D14YCS          D14YSN        COMM
      D14DOT(3)       D14ZSN          COMM
      D14ZCS          EEJ(3,3)        EL2(3)         COMM
COMMON EEE(3,3)       EL2YCS          EL2YSN        COMM
      EL2DOT(3)       EL2ZSN          EL3(3)         COMM
      EL2ZCS          EL3YCS          EL3YSN        COMM
      EL3DOT(3)       EL3ZSN          EL4(3)         COMM
      EL3ZCS          EL4YCS          EL4YSN        COMM
      EL4DOT(3)       EL4ZSN          EM(6,6)         COMM
      EL4ZCS          FEED(6)         FFF(3)         COMM
COMMON FAT(8)         FLAG1          FLAG2         COMM
      FEE(6)          FLAG4          FN            COMM
      FFJ(3)          FO1(3)         FO2(3)         COMM
      FLAG3          F1(3)          F11(3)         COMM
      FO(3)           F12(3)         F13(3)         COMM
      FO3(3)          G3             G4             COMM
      FPT(5)          G3DOT          G4DOT          COMM
COMMON GAIN(10)       HCMG(3)        HDOT(3)        COMM
      G3DOT           HO(3)          HW(6)         COMM
COMMON H(3)           H1PDOT(3)      H1PRIM(3)     COMM
      HI(3)           H4PRIM(3)      COMM
      H1(3)          ICFA           ICFS           COMM
COMMON IB2F           ICFO          IDOCK          COMM
      ICFC           ICFO          COMM
      IDOF(6)        IPNDLM          IPNTCK        COMM
      IGRAVF         IPROPF          COMM
      IPRINT         NCHECK         NDECK          COMM
COMMON NCASE          NUMCMG         OMEGA4         COMM
      NGAIN          OMEGA3         COMM
COMMON OMEGA1         PEND4L        COMM
      PEND3L        Q(4,4)         COMM
COMMON

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COMMON	R	,	RO(3)	,	R1(3)	,	COMMON
*	R1DOT(3)	,	R1YCS	,	R1YSN	,	COMMON
*	R1ZCS	,	R1ZSN	,	R2(3)	,	COMMON
*	R2DOT(3)	,	R2YCS	,	R2YSN	,	COMMON
*	R2ZCS	,	R2ZSN	,	R3(3)	,	COMMON
*	R3DOT(3)	,	R3YCS	,	R3YSN	,	COMMON
*	R3ZCS	,	R3ZSN	,	R4(3)	,	COMMON
*	R4DOT(3)	,	R4YCS	,	R4YSN	,	COMMON
*	R4ZCS	,	R4ZSN	,		,	COMMON
COMMON	S	,	SDOT	,	SINFEJ	,	COMMON
*	SINTTJ	,	SINTT0	,	SINTT1	,	COMMON
*	SINTT2	,	SINTT3	,	SINTT4	,	COMMON
*	SP	,	SUM1	,	SUM2	,	COMMON
*	SUM3	,	S2(3)	,	S3(3)	,	COMMON
*	S4(3)	,					COMMON
COMMON	T(3,3)	,	TC(3,3)	,	TEMP1(3)	,	COMMON
*	TEMP2(3)	,					COMMON
*	TEMP3(3)	,	TEMP4(3)	,	TEMP5(3,3)	,	COMMON
*	TEMP6(3,3)	,	TEMP7(3,3)	,	TEMP8(3,3)	,	COMMON
*	TEMP9(3,3)	,	TEMP10(3,3)	,	TEMP11(3,3)	,	COMMON
*	TEMP12(3,3)	,	TEMP13(3,3)	,	TEMP14(3,3)	,	COMMON
*	TEMP15(3,3)	,	TERM1(3)	,	TERM2(3)	,	COMMON
*	TFRICT	,	THATA(6)	,	THATA(6)	,	COMMON
*	THETA1	,	THETA3	,	THETA4	,	COMMON
*	THETO	,	TIBO(3,3)	,	TIBOI(3,3)	,	COMMON
*	TIME	,	TJ	,	TJ1(10)	,	COMMON
*	TJ2(10)	,	TJ3(10)	,	TJ4(10)	,	COMMON
*	TMOTOR	,					COMMON
*	TOEF(3)	,	TOTMAS	,	T01	,	COMMON
*	TQOG(3)	,	TQOP(3)	,	TQ1G(3)	,	COMMON
*	TQ1P(3)	,	TSTART	,	TSTOP	,	COMMON
*	TT1DOT	,	TT3DOT	,	TT4DOT	,	COMMON
*	T1EF(3)	,	T13	,	T14	,	COMMON
COMMON	V(3)	,					COMMON
COMMON	W0(3)	,	WS	,	W1(3)	,	COMMON
*	W3(3)	,	W4(3)	,			COMMON
COMMON	X(6,7)	,	XC	,	XCDOT	,	COMMON
*	XMU						COMMON

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THIS SUBROUTINE COMPUTES THE TORQUE BETWEEN BODY 0 AND BODY 1.  
THIS TORQUE CONSISTS OF THE CONTROL TORQUE AND FRICTION TORQUE.

IF (TIME .NE. TSTART) GO TO 10

XC=-GAIN(2)\*OMEGA1

AFOUR(2)=XC

10 CONTINUE

AFOUR(1)=TIME

BFOUR(1)=DELTAT

XCDOT=GAIN(3)\*(OMEGA1-SP)

BFOUR(2)=XCDOT

CALL FOMS(AFOUR,BFOUR,2,FLAG4,TJ4)

XC=AFOUR(2)

TMOTOR=GAIN(2)\*OMEGA1+XC

TFRICT=GAIN(1)\*SIN(OMEGA1)

T01=TMOTOR+TFRICT

RETURN

C  
C  
C  
C

TORR

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END



SUBROUTINE TORK13(T13,CP1,CP2,THETA3,OMEGA3)

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THIS SUBROUTINE COMPUTES THE TORQUE BETWEEN BODY 1 AND BODY 3.  
THIS TORQUE CONSISTS OF THE CONTROL TORQUE AND FRICTION TORQUE.

T13 = - CP1\*OMEGA3 - CP2\*THETA3

RETURN

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END

TORK1

TORK1

TORK1

TORK1

TORK1

TORK1

TORK1

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C      SUBROUTINE TORK14(T14,CP1,CP2,THETA4,OMEGA4)
C      *
C      *
C      *****
C      THIS SUBROUTINE COMPUTES THE TORQUE BETWEEN BODY 1 AND BODY 4.
C      THIS TORQUE CONSISTS OF THE CONTROL TORQUE AND FRICTION TORQUE.
C      T14 = CP1*OMEGA4 - CP2*(THETA4 - 3.14159)
C      RETURN
C      *****
C      *
C      *
C      END

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TORK1  
 TORK1  
 TORK1  
 TORK1  
 TORK1  
 TORK1

C  
C  
C  
C

## SUBROUTINE XDOT

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*****
COMMON      A(3)      ,      AE(5)      ,      AED(5)      ,      COMM
*            AF0UR(2)  ,      AII(6,3,3) ,      ALI      ,      COMM
*            AIO(6,3,3) ,      AJ1(3)    ,      ALI      ,      COMM
*            AOCJ(6,3,3) ,      AOJ(3)    ,      ADNE(7)   ,      COMM
*            ATCPT2(3,3) ,      ATHREE(5) ,      ATWO(4)   ,      COMM
*            A1(3,3)    ,      A1J(2)    ,      COMM      ,      COMM
COMMON      BDMASS     ,      BFOUR(2)   ,      BMOM      ,      COMM
*            BODYDI(3,3) ,      BODYOI(3,3) ,      BODY1I(3,3) ,      COMM
*            BOMASS     ,      BONE(7)    ,      BTHREE(5) ,      COMM
*            BTWO(4)    ,      B1MASS     ,      B2MASS     ,      COMM
*            B3MASS     ,      B4MASS     ,      COMM      ,      COMM
COMMON      CA(3)      ,      CB(3)      ,      CGAINO(3)   ,      COMM
*            CGAIN1(2)  ,      COMM      ,      COMM      ,      COMM
*            COSFEJ     ,      COSTTJ    ,      COSTTO    ,      COMM
*            COSTT1     ,      COSTT3    ,      COSTT4    ,      COMM
*            CO2T       ,      CP1       ,      CP2       ,      COMM
*            CST        ,      C1        ,      COMM      ,      COMM
COMMON      DB(3)      ,      DD01(3)    ,      COMM      ,      COMM
*            DELTAT     ,      D01(3)    ,      D01DOT(3)   ,      COMM
*            DTI(3)     ,      COMM      ,      COMM      ,      COMM
*            DTIME      ,      D12(3)    ,      D13(3)    ,      COMM
*            D13DOT(3)  ,      D13YCS    ,      D13YSN    ,      COMM
*            D13ZCS     ,      D13ZSN    ,      D14(3)     ,      COMM
*            D14DOT(3)  ,      D14YCS    ,      D14YSN    ,      COMM
*            D14ZCS     ,      D14ZSN    ,      COMM      ,      COMM
COMMON      EEE(3,3)   ,      EEJ(3,3)   ,      EL2(3)     ,      COMM
*            EL2DOT(3)  ,      EL2YCS    ,      EL2YSN    ,      COMM
*            EL2ZCS     ,      EL2ZSN    ,      EL3(3)     ,      COMM
*            EL3DOT(3)  ,      EL3YCS    ,      EL3YSN    ,      COMM
*            EL3ZCS     ,      EL3ZSN    ,      EL4(3)     ,      COMM
*            EL4DOT(3)  ,      EL4YCS    ,      EL4YSN    ,      COMM
*            EL4ZCS     ,      EL4ZSN    ,      EM(6,6)    ,      COMM
COMMON      FAT(8)     ,      COMM      ,      COMM      ,      COMM
*            FEE(6)     ,      FEED(6)   ,      FFF(3)     ,      COMM
*            FFJ(3)     ,      FLAG1     ,      FLAG2     ,      COMM
*            FLAG3     ,      FLAG4     ,      FNI      ,      COMM
*            FO(3)      ,      FO1(3)    ,      FO2(3)    ,      COMM
*            FO3(3)     ,      F1(3)     ,      F11(3)    ,      COMM
*            FPT(5)     ,      COMM      ,      COMM      ,      COMM
*            F12(3)     ,      F13(3)    ,      COMM      ,      COMM
COMMON      GAIN(10)   ,      G3        ,      COMM      ,      COMM
*            G3DOT     ,      G4        ,      G4DOT     ,      COMM
COMMON      H(3)       ,      HCMG(3)   ,      HDOT(3)   ,      COMM
*            HI(3)      ,      HO(3)     ,      HW(6)     ,      COMM
*            H1(3)      ,      H1PDOT(3) ,      H1PRIM(3) ,      COMM
*            H3PRIM(3)  ,      H4PRIM(3) ,      COMM      ,      COMM
COMMON      IB2F       ,      ICFA      ,      ICFB      ,      COMM
*            ICFC       ,      ICFD      ,      IDOCK     ,      COMM
*            IDOF(6)    ,      COMM      ,      COMM      ,      COMM
*            IGRAVF     ,      IPNDLM    ,      IPNTCK    ,      COMM
*            IPRINT     ,      IPROPF    ,      COMM      ,      COMM
COMMON      NCASE      ,      NCHECK    ,      NDECK     ,      COMM
*            NGAIN      ,      NUMCMG    ,      COMM      ,      COMM
COMMON      OMEGA1     ,      OMEGA3    ,      OMEGA4    ,      COMM
COMMON      PEND3L     ,      PEND4L    ,      COMM      ,      COMM
COMMON      Q(4,4)     ,      COMM      ,      COMM      ,      COMM
```

COMMON	R	R0(3)	R1(3)	COMMON
*	R1DOT(3)	R1YCS	R1YSN	COMMON
*	R1ZCS	R1ZSN	R2(3)	COMMON
*	R2DOT(3)	R2YCS	R2YSN	COMMON
*	R2ZCS	R2ZSN	R3(3)	COMMON
*	R3DOT(3)	R3YCS	R3YSN	COMMON
*	R3ZCS	R3ZSN	R4(3)	COMMON
*	R4DOT(3)	R4YCS	R4YSN	COMMON
*	R4ZCS	R4ZSN		COMMON
COMMON	S	SDOT	SINFEJ	COMMON
*	SINTTJ	SINTT0	SINTT1	COMMON
*	SINTT2	SINTT3	SINTT4	COMMON
*	SP	SUM1	SUM2	COMMON
*	SUM3	S2(3)	S3(3)	COMMON
*	S4(3)			COMMON
COMMON	T(3,3)	TC(3,3)	TEMP1(3)	COMMON
*	TEMP2(3)			COMMON
*	TEMP3(3)	TEMP4(3)	TEMP5(3,3)	COMMON
*	TEMP6(3,3)	TEMP7(3,3)	TEMP8(3,3)	COMMON
*	TEMP9(3,3)	TEMP10(3,3)	TEMP11(3,3)	COMMON
*	TEMP12(3,3)	TEMP13(3,3)	TEMP14(3,3)	COMMON
*	TEMP15(3,3)	TERM1(3)	TERM2(3)	COMMON
*	TFRIC	THATA(6)	THATA(6)	COMMON
*	THETA1	THETA3	THETA4	COMMON
*	THETO	TIB0(3,3)	TIB01(3,3)	COMMON
*	TIME	TJ	TJ1(10)	COMMON
*	TJ2(10)	TJ3(10)	TJ4(10)	COMMON
*	TMOTOR			COMMON
*	TOEF(3)	TOTMAS	T01	COMMON
*	TQOG(3)	TQOP(3)	TQ1G(3)	COMMON
*	TQ1P(3)	TSTART	TSTOP	COMMON
*	TT1DOT	TT3DOT	TT4DOT	COMMON
*	TT1EF(3)	T13	T14	COMMON
COMMON	V(3)			COMMON
COMMON	W0(3)	WS	W1(3)	COMMON
*	W3(3)	W4(3)		COMMON
COMMON	X(6,7)	XC	XCDOT	COMMON
*	XMU			COMMON

\*\*\*\*\*

\*  
\*  
\*

\*\*\*\*\*

SINTT1 = SIN(THETA1)	XDOT
COSTT1 = COS(THETA1)	XDOT
W1(1) = W0(1) + OMEGA1	XDOT
W1(2) = W0(2)*COSTT1 + W0(3)*SINTT1	XDOT
W1(3) = -W0(2)*SINTT1 + W0(3)*COSTT1	XDOT
IF (TIME .NE. TSTART) GO TO 2	XDOT
CALL RECALC	XDOT
2 CONTINUE	XDOT
CALL SDCALC	XDOT
EL2DOT(1) = -W1(3)*EL2(2) + W1(2)*EL2(3) + S2(1)*SDOT	XDOT
EL2DOT(2) = W1(3)*EL2(1) - W1(1)*EL2(3) + S2(2)*SDOT	XDOT
EL2DOT(3) = -W1(2)*EL2(1) + W1(1)*EL2(2) + S2(3)*SDOT	XDOT
R0(1) = R1(1) - D01(1)	XDOT
R0(2) = R1(2)*COSTT1 - R1(3)*SINTT1 - D01(2)	XDOT
R0(3) = R1(2)*SINTT1 + R1(3)*COSTT1 - D01(3)	XDOT
W3(1) = W1(1)	XDOT
W3(2) = OMEGA3*S3(2) + W1(2)	XDOT

```

W3(3) = OMEGA3*S3(3) + W1(3)
EL3DOT(1) = -W3(3)*EL3(2) + W3(2)*EL3(3)
EL3DOT(2) = W3(3)*EL3(1) - W3(1)*EL3(3)
EL3DOT(3) = -W3(2)*EL3(1) + W3(1)*EL3(2)
W4(1) = W1(1)
W4(2) = OMEGA4*S4(2) + W1(2)
W4(3) = OMEGA4*S4(3) + W1(3)
EL4DOT(1) = -W4(3)*EL4(2) + W4(2)*EL4(3)
EL4DOT(2) = W4(3)*EL4(1) - W4(1)*EL4(3)
EL4DOT(3) = -W4(2)*EL4(1) + W4(1)*EL4(2)
D01DOT(1) = -W0(3)*D01(2) + W0(2)*D01(3)
D01DOT(2) = W0(3)*D01(1) - W0(1)*D01(3)
D01DOT(3) = -W0(2)*D01(1) + W0(1)*D01(2)
D13DOT(1) = -W1(3)*D13(2) + W1(2)*D13(3)
D13DOT(2) = W1(3)*D13(1) - W1(1)*D13(3)
D13DOT(3) = -W1(2)*D13(1) + W1(1)*D13(2)
D14DOT(1) = -W1(3)*D14(2) + W1(2)*D14(3)
D14DOT(2) = W1(3)*D14(1) - W1(1)*D14(3)
D14DOT(3) = -W1(2)*D14(1) + W1(1)*D14(2)
R1DOT(1) = (B0MASS/TOTMAS)*D01DOT(1)
*      = (B2MASS/TOTMAS)*EL2DOT(1)
*
*      = (B3MASS/TOTMAS)*(D13DOT(1) + EL3DOT(1))
*
*      = (B4MASS/TOTMAS)*(D14DOT(1) + EL4DOT(1))
R1DOT(2) = (B0MASS/TOTMAS)*(D01DOT(2)*COSTT1 + D01DOT(3)*SINTT1)
*      = (B2MASS/TOTMAS)*EL2DOT(2)
*
*      = (B3MASS/TOTMAS)*(D13DOT(2) + EL3DOT(2))
*
*      = (B4MASS/TOTMAS)*(D14DOT(2) + EL4DOT(2))
R1DOT(3) = (B0MASS/TOTMAS)*(-D01DOT(2)*SINTT1 + D01DOT(3)*COSTT1)
*      = (B2MASS/TOTMAS)*EL2DOT(3)
*
*      = (B3MASS/TOTMAS)*(D13DOT(3) + EL3DOT(3))
*
*      = (B4MASS/TOTMAS)*(D14DOT(3) + EL4DOT(3))
R2DOT(1) = R1DOT(1) + EL2DOT(1)
R2DOT(2) = R1DOT(2) + EL2DOT(2)
R2DOT(3) = R1DOT(3) + EL2DOT(3)
R3DOT(1) = R1DOT(1) + D13DOT(1) + EL3DOT(1)
R3DOT(2) = R1DOT(2) + D13DOT(2) + EL3DOT(2)
R3DOT(3) = R1DOT(3) + D13DOT(3) + EL3DOT(3)
R4DOT(1) = R1DOT(1) + D14DOT(1) + EL4DOT(1)
R4DOT(2) = R1DOT(2) + D14DOT(2) + EL4DOT(2)
R4DOT(3) = R1DOT(3) + D14DOT(3) + EL4DOT(3)
CALL MULT(H0,BODY0I,W0,DUM,DUM,DUM,1)
CALL MULT(H1,BODY1I,W1,DUM,DUM,DUM,1)
H3PRIM(1) = B3MASS*(-EL3(3)*R3DOT(2) + EL3(2)*R3DOT(3))
H3PRIM(2) = B3MASS*( EL3(3)*R3DOT(1) - EL3(1)*R3DOT(3))
H3PRIM(3) = B3MASS*(-EL3(2)*R3DOT(1) + EL3(1)*R3DOT(2))
H4PRIM(1) = B4MASS*(-EL4(3)*R4DOT(2) + EL4(2)*R4DOT(3))
H4PRIM(2) = B4MASS*( EL4(3)*R4DOT(1) - EL4(1)*R4DOT(3))
H4PRIM(3) = B4MASS*(-EL4(2)*R4DOT(1) + EL4(1)*R4DOT(2))
H1PRIM(2) = H1(2) + H3PRIM(2) + H4PRIM(2)
*      = B2MASS*( -EL2(3)*R2DOT(1) + EL2(1)*R2DOT(3))
*
*      = B3MASS*( -D13(3)*R3DOT(1) + D13(1)*R3DOT(3))
*
*      = B4MASS*( -D14(3)*R4DOT(1) + D14(1)*R4DOT(3))
H1PRIM(3) = H1(3) + H3PRIM(3) + H4PRIM(3)
*      = B2MASS*( EL2(2)*R2DOT(1) - EL2(1)*R2DOT(2))
*
*      = B3MASS*( D13(2)*R3DOT(1) - D13(1)*R3DOT(2))
*
*      = B4MASS*( D14(2)*R4DOT(1) - D14(1)*R4DOT(2))
IF (TIME .NE. TSTART) GO TO 5
H1PRIM(1) = H1(1) + H3PRIM(1) + H4PRIM(1)
*      = B2MASS*(EL2(3)*R2DOT(2) - EL2(2)*R2DOT(3))
*
*      = B3MASS*(D13(3)*R3DOT(2) - D13(2)*R3DOT(3))
*
*      = B4MASS*(D14(3)*R4DOT(2) - D14(2)*R4DOT(3))
LET US DEFINE SOME INTERMEDIATE VALUES NEEDED TO COMPUTE H.

```

```

SUM1 = B1MASS*R1DOT(1) + B2MASS*R2DOT(1)
*      + B3MASS*R3DOT(1) + B4MASS*R4DOT(1)
SUM2 = B1MASS*R1DOT(2) + B2MASS*R2DOT(2)
*      + B3MASS*R3DOT(2) + B4MASS*R4DOT(2)
SUM3 = B1MASS*R1DOT(3) + B2MASS*R2DOT(3)
*      + B3MASS*R3DOT(3) + B4MASS*R4DOT(3)
C
CALCULATE H.
DO 4 I=1,3
HCMG(I) = FFF(I)
DO 4 J=1,3
HCMG(I) = EEE(I,J)*H0(J) + HCMG(I)
4 CONTINUE
H(1) = H0(1) + H1PRIM(1)
*      + (DO1(3)*COSTT1 + DO1(2)*SINTT1)*SUM2
*      + (DO1(3)*SINTT1 + DO1(2)*COSTT1)*SUM3
*      + HCMG(1)
H(2) = H0(2) + COSTT1*H1PRIM(2) - SINTT1*H1PRIM(3)
*      + DO1(3)*SUM1 - DO1(1)*SINTT1*SUM2 - DO1(1)*COSTT1*SUM3
*      + HCMG(2)
H(3) = H0(3) + SINTT1*H1PRIM(2) + COSTT1*H1PRIM(3)
*      + DO1(2)*SUM1 + DO1(1)*COSTT1*SUM2 - DO1(1)*SINTT1*SUM3
*      + HCMG(3)
5. CONTINUE
C
COMPUTE THE UNIT VECTOR J1.
AJ1(1) = B2MASS*EL2(1)
*      + B3MASS*D13(1) + B3MASS*EL3(1)
*      + B4MASS*D14(1) + B4MASS*EL4(1)
AJ1(2) = B2MASS*EL2(2)
*      + B3MASS*D13(2) + B3MASS*EL3(2)
*      + B4MASS*D14(2) + B4MASS*EL4(2)
AJ1(3) = B2MASS*EL2(3)
*      + B3MASS*D13(3) + B3MASS*EL3(3)
*      + B4MASS*D14(3) + B4MASS*EL4(3)
C
UPDATE THE ORBIT ANGLE
THETO = TIME*WS
IF (IGRAVF.EQ. 0) GO TO 10
C
CALCULATE THE GRAVITY GRADIENT FORCES AND TORQUES.
CALL GGRAD
10. CONTINUE
C
SUM THE FORCES ON BODY ZERO.
FO(1) = FO1(1)
FO(2) = FO1(2)
FO(3) = FO1(3)
C
SUM THE FORCES ON BODY ONE.
F1(1) = F11(1)
F1(2) = F11(2)
F1(3) = F11(3)
C
SUM THE TORQUES ON BODY ZERO.
TOEF(1) = TQOG(1) + TQOP(1)
TOEF(2) = TQOG(2) + TQOP(2)
TOEF(3) = TQOG(3) + TQOP(3)
C
SUM THE TORQUES ON BODY ONE.
T1EF(1) = TQ1G(1) + TQ1P(1)
T1EF(2) = TQ1G(2) + TQ1P(2)
T1EF(3) = TQ1G(3) + TQ1P(3)
C
LET US DEFINE SOME INTERMEDIATE TERMS USED TO CALCULATE HDOT.
TERM1(1) = (BOMASS - TOTMAS)*DO1(1) - AJ1(1)
TERM1(2) = (BOMASS - TOTMAS)*DO1(2)
*      - COSTT1*AJ1(2) + SINTT1*AJ1(3)
TERM1(3) = (BOMASS - TOTMAS)*DO1(3)
*      + SINTT1*AJ1(2) - COSTT1*AJ1(3)
TERM2(1) = BOMASS*DO1(1) - AJ1(1)

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```

TERM2(2) = BOMASS*( COSTT1*DO1(2) + SINTT1*DO1(3)) - AJ1(2)
TERM2(3) = BOMASS*(-SINTT1*DO1(2) + COSTT1*DO1(3)) - AJ1(3)
ATCPT2(1,1) = 0
ATCPT2(1,2) = -TERM2(3)
ATCPT2(1,3) = TERM2(2)
ATCPT2(2,1) = COSTT1*TERM2(3) + SINTT1*TERM2(2)
ATCPT2(2,2) = -SINTT1*TERM2(1)
ATCPT2(2,3) = -COSTT1*TERM2(1)
ATCPT2(3,1) = SINTT1*TERM2(3) - COSTT1*TERM2(2)
ATCPT2(3,2) = COSTT1*TERM2(1)
ATCPT2(3,3) = -SINTT1*TERM2(1)
HDOT(1) = WO(3)*H(2) - WO(2)*H(3)
*      *(-TERM1(3)*FO(2) + TERM1(2)*FO(3))/TOTMAS
** (ATCPT2(1,1)*F1(1)+ATCPT2(1,2)*F1(2)+ATCPT2(1,3)*F1(3))/TOTMAS
** TOEF(1) + T1EF(1)
HDOT(2) = -WO(3)*H(1) + WO(1)*H(3)
*      *( TERM1(3)*FO(1) - TERM1(1)*FO(3))/TOTMAS
** (ATCPT2(2,1)*F1(1)+ATCPT2(2,2)*F1(2)+ATCPT2(2,3)*F1(3))/TOTMAS
** TOEF(2) + COSTT1*T1EF(2) - SINTT1*T1EF(3)
HDOT(3) = WO(2)*H(1) - WO(1)*H(2)
*      *(-TERM1(2)*FO(1) + TERM1(1)*FO(2))/TOTMAS
** (ATCPT2(3,1)*F1(1)+ATCPT2(3,2)*F1(2)+ATCPT2(3,3)*F1(3))/TOTMAS
** TOEF(3) + SINTT1*T1EF(2) + COSTT1*T1EF(3)
C  CALCULATE THE TORQUE BETWEEN BODY 0 AND BODY 1. (CONTROL,FRICTION)
CALL TORK01
H1PDOT(1) = -W1(2)*H1PRIM(3) + W1(3)*H1PRIM(2)
* +R1DOT(2)*(-B2MASS*EL2DOT(3)-B3MASS*(D13DOT(3)+EL3DOT(3))-
* B4MASS*(D14DOT(3)+EL4DOT(3)))-R1DOT(3)*(-B2MASS*EL2DOT(2)-
* B3MASS*(D13DOT(2)+EL3DOT(2))-B4MASS*(D14DOT(2)+EL4DOT(2)))
* -AJ1(2)*(-FO(2)*SINTT1/TOTMAS+FO(3)*COSTT1/TOTMAS)
* -AJ1(3)*( FO(2)*COSTT1/TOTMAS+FO(3)*SINTT1/TOTMAS)
* -AJ1(3)*F1(2)/TOTMAS-AJ1(2)*F1(3)/TOTMAS+T1EF(1)+T01
C  CALCULATE THE TORQUE BETWEEN BODY 1 AND BODY 3. (CONTROL,FRICTION)
CALL TORK13(T13,CP1,CP2,THETA3,OMEGA3)
G3DOT=-S3(2)*(W1(3)*H3PRIM(1)-W1(1)*H3PRIM(3))-S3(3)*(W1(1)*H3PRIM(2)
*(2)-W1(2)*H3PRIM(1))+B3MASS*S3(2)*(EL3DOT(3)+R3DOT(1)-EL3DOT(1)+R3
DOT(3))+B3MASS*S3(3)*(EL3DOT(1)+R3DOT(2)-EL3DOT(2)+R3DOT(1))-
*(B3MASS/TOTMAS)*S3(2)*(EL3(3)*(FO(1)+F1(1))-EL3(1)*(-FO(2)*SINTT1+
FO(3)*COSTT1+F1(3)))-(B3MASS/TOTMAS)*S3(3)*(EL3(1)*(-FO(2)*COSTT1+
FO(3)*SINTT1+F1(2))-EL3(2)*(FO(1)+F1(1)))+T13
C  CALCULATE THE TORQUE BETWEEN BODY 1 AND BODY 4. (CONTROL,FRICTION)
CALL TORK14(T14,CP1,CP2,THETA4,OMEGA4)
G4DOT=-S4(2)*(W1(3)*H4PRIM(1)-W1(1)*H4PRIM(3))-S4(3)*(W1(1)*H4PRIM(2)
*(2)-W1(2)*H4PRIM(1))+B4MASS*S4(2)*(EL4DOT(3)+R4DOT(1)-EL4DOT(1)+R4
DOT(3))+B4MASS*S4(3)*(EL4DOT(1)+R4DOT(2)-EL4DOT(2)+R4DOT(1))-
*(B4MASS/TOTMAS)*S4(2)*(EL4(3)*(FO(1)+F1(1))-EL4(1)*(-FO(2)*SINTT1+
FO(3)*COSTT1+F1(3)))-(B4MASS/TOTMAS)*S4(3)*(EL4(1)*(-FO(2)*COSTT1+
FO(3)*SINTT1+F1(2))-EL4(2)*(FO(1)+F1(1)))+T14
RETURN
*****
*
*
*
END

```

## APPENDIX D, PROGRAM FLOW CHARTS



# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1102-01 (4-64)

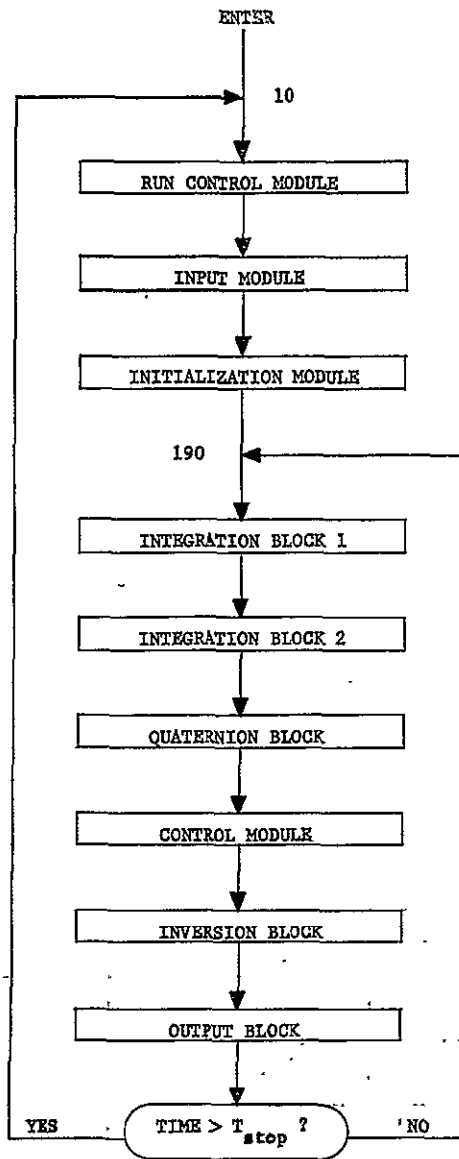
Application MAIN PROGRAM FLOW CHART

Date OCTOBER 1970

Page 1 of 1

Procedure \_\_\_\_\_

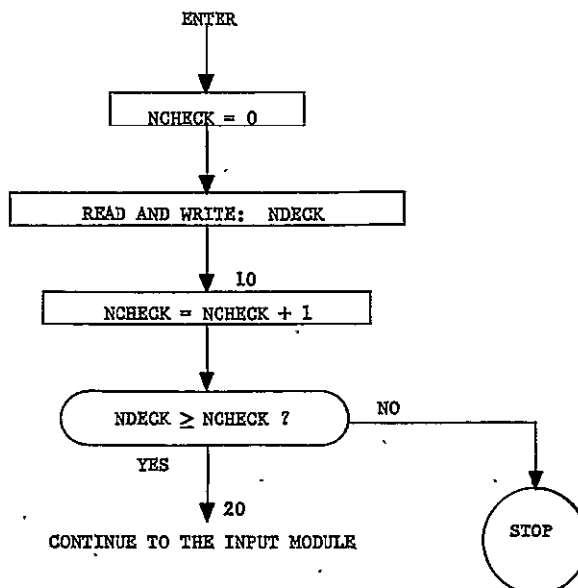
Drawn By GARY JOHNSON



# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application RUN CONTROL MODULE Date OCTOBER 1970 Page 1 of 1  
Procedure \_\_\_\_\_ Drawn By GARY JOHNSON



# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application INPUT MODULE

Date OCTOBER 1970

Page 1 of 5

Procedure

Drawn By GARY JOHNSON

ENTER

```

--- GAIN(M) = 0. M=1,10
WRITE: NCHECK
READ AND WRITE:
IPNDLM
IPRINT
T_start, T_stop, Δt
ALT
[I, B0]I
wox, woy, woz
m0
[I0]
NUMCMG
    
```

NUMCMG = 0 ?

YES

NO

```

DO 110 J = 1, NUMCMG
READ AND WRITE:
IDOF (J)
HwJ
[0, CJ]
IF (IDOF (J) .EQ. 0) GO TO 110
READ AND WRITE:
[IIJ]
θJ
φJ
θJ = 0.
φJ = 0.
IF (IDOF (J) .EQ. 1) GO TO 110
READ AND WRITE:
[IOJ]
θJ
φJ
110 CONTINUE
    
```

120

CONTINUE TO THE NEXT PAGE

# FLOW CHART & BLOCK DIAGRAM

Application INPUT MODULE CONTINUED

Date OCTOBER 1970

Page 2 of 5

Procedure

Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

READ AND WRITE: IPROFF

IPROFF = 0 ?

YES

NO

READ AND WRITE: IATTIF

IATTIF = 0 ?

YES

NO

READ AND WRITE:  
CA (1), CA (2), CA (3)

125

DO 130 J = 1, 3  
READ AND WRITE:  
A<sub>oJ</sub>, CGAIN<sub>oJ</sub>  
130 CONTINUE

140

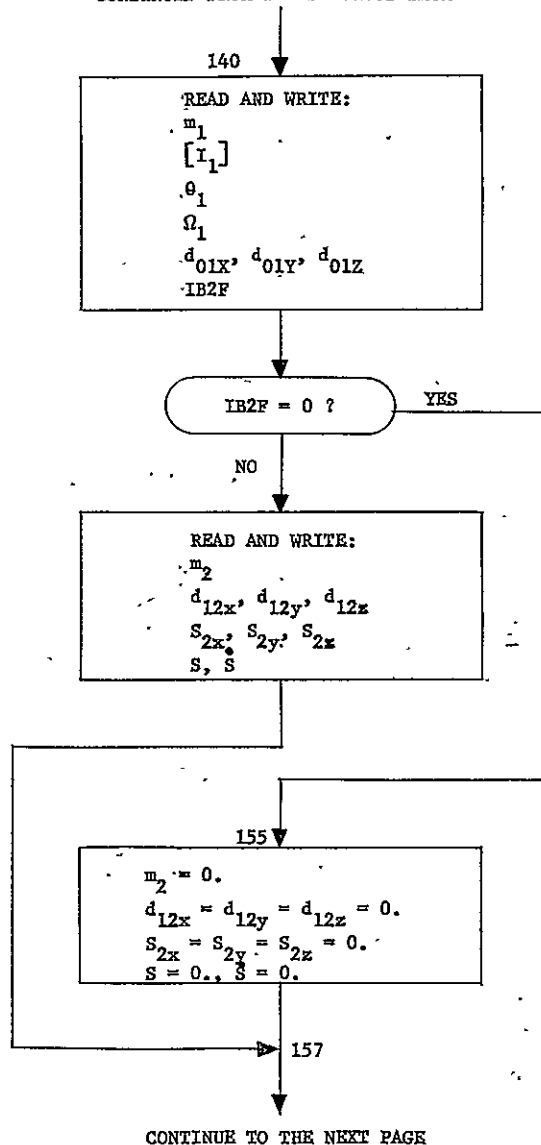
CONTINUE TO THE NEXT PAGE

# FLOW CHART & BLOCK DIAGRAM

F. A. DEW 1103-01 (4-64)

Application INPUT MODULE CONTINUED Date OCTOBER 1970 Page 3 of 5  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE



# FLOW CHART & BLOCK DIAGRAM

FORM DE 1103-01 (1-64)

Application INPUT MODULE CONTINUED

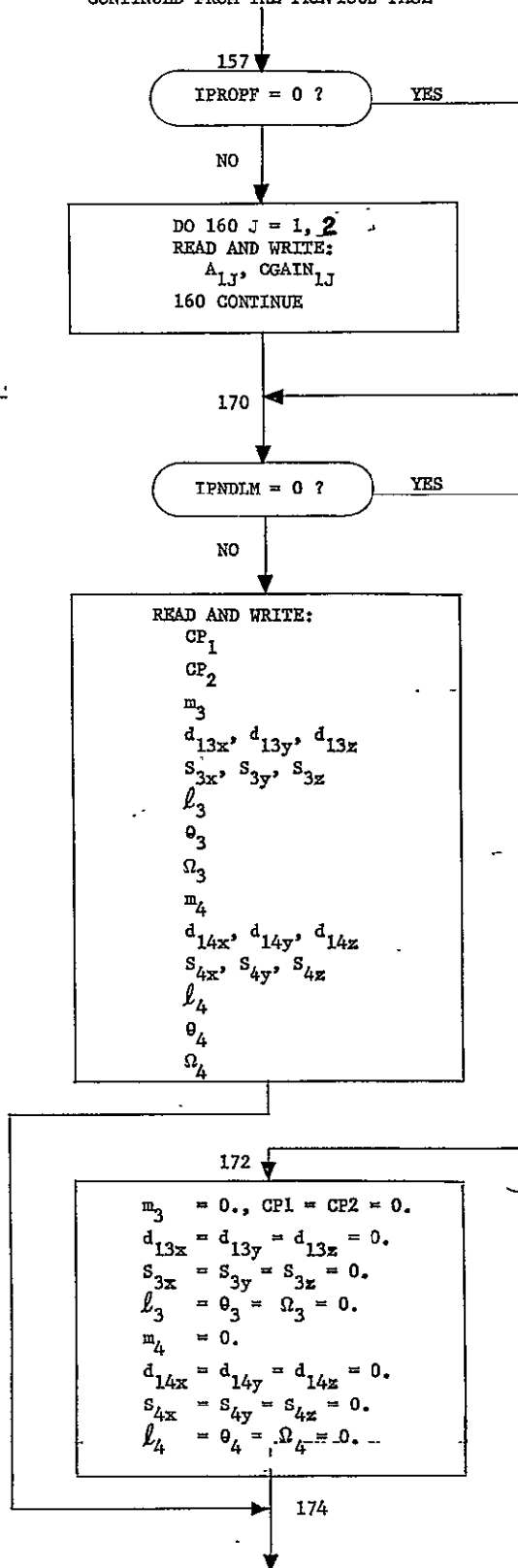
Date OCTOBER 1970

Page 4 of 5

Procedure \_\_\_\_\_

Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

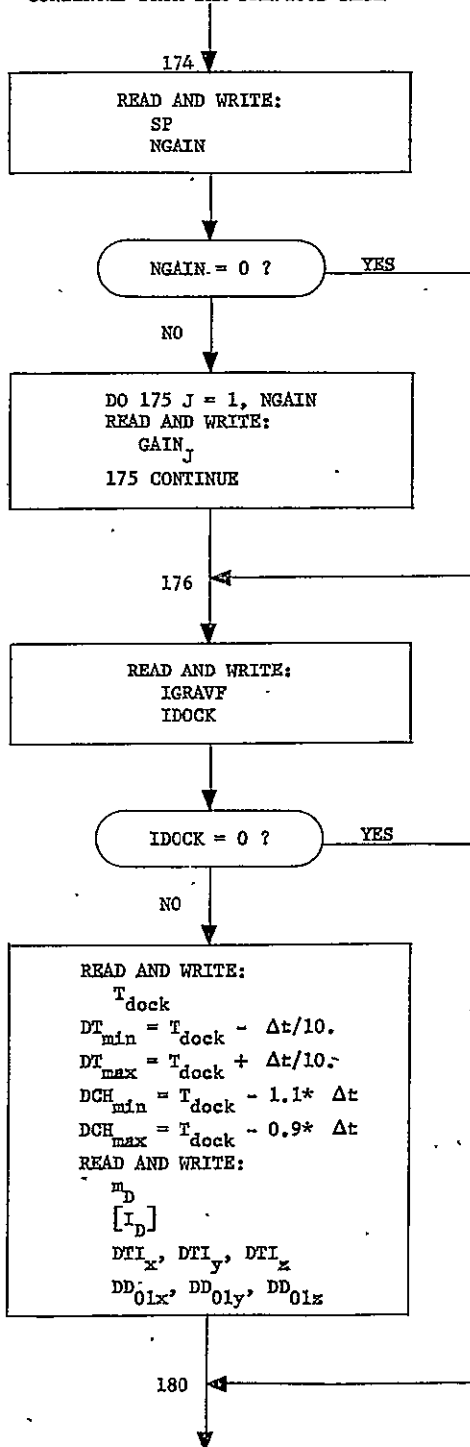


CONTINUE TO THE NEXT PAGE

# Fig 40 FLOWCHART & BLOCK DIAGRAM FORM 103-01 (2-64)

Application INPUT MODULE CONTINUED Date OCTOBER 1970 Page 5 of 5  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE



CONTINUE TO THE INITIALIZATION MODULE

# FLOW CHART & BLOCK DIAGRAM

Application INITIALIZATION MODULE

Date OCTOBER 1970

Page 1

Procedure

Drawn By GARY JOHNSON

ENTER

```

m = m0 + m1 + m2 + m3 + m4
ICFA = ICFB = ICFC = ICFD = 0.
FLAG 1 = FLAG 2 = FLAG 3 = FLAG 4 = 0.
λ2 = 1.
λ3 = λ4 = λ5 = 0.
λ̇2 = 1.
λ̇3 = λ̇4 = λ̇5 = 0.
A22 = 01
A23 = 03
A24 = 04
A2 = 1.
A3 = A4 = A5 = 0.
IENTCK = 1
TIME = Tstart
μ = 1.408 × 1016
R = ALT + 3960.
R = 5280.*R
C1 = μ/R3
ws = √C1
F01x = F01y = F01z = 0.
F02x = F02y = F02z = 0.
F0x = F0y = F0z = 0.
F11x = F11y = F11z = 0.
F12x = F12y = F12z = 0.
F1x = F1y = F1z = 0.
TQ0Gx = TQ0Gy = TQ0Gz = 0.
TQ0Px = TQ0Py = TQ0Pz = 0.
TQ1Gx = TQ1Gy = TQ1Gz = 0.
TQ1Px = TQ1Py = TQ1Pz = 0.
TAP = TBP = 0.
FFF(M) = 0. M = 1, 3
    
```

NUMCMG = 0 ?

YES

NO

CALL CMG

```

DO 183 J = 1, NUMCMG
θJ = θJ - θ̇J * Δt
φJ = φJ - φ̇J * Δt
183 CONTINUE
    
```

184

CALL XDOT

CONTINUE TO INTEGRATION BLOCK 1



# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application INTEGRATION BLOCK 1

Date OCTOBER 1970

Page 1 of 2

Procedure

Drawn By GARY JOHNSON

ENTRY POINT FROM THE OUTPUT BLOCK

ENTER

190

TIME = T<sub>start</sub> ?

NO

YES

CALL EMCALC

$$\begin{aligned} G_3 &= M_{5,1} * w_{0x} + M_{5,2} * w_{0y} + M_{5,3} * w_{0x} \\ &\quad + M_{5,4} * \Omega_1 + M_{5,5} * \Omega_3 + M_{5,6} * \Omega_4 \\ G_4 &= M_{6,1} * w_{0x} + M_{6,2} * w_{0y} + M_{6,3} * w_{0x} \\ &\quad + M_{6,4} * \Omega_1 + M_{6,5} * \Omega_3 + M_{6,6} * \Omega_4 \end{aligned}$$

192

$AI_2 = H_x$   
 $AI_3 = H_y$   
 $AI_4 = H_z$   
 $AI_5 = H_{1x}$   
 $AI_6 = G_3$   
 $AI_7 = G_4$

$AI_1 = TIME$   
 $BI_1 = \Delta t$   
 $BI_2 = H_x$   
 $BI_3 = H_y$   
 $BI_4 = H_z$   
 $BI_5 = H_{1x}$   
 $BI_6 = G_3$   
 $BI_7 = G_4$

CALL FORM

$H_x = AI_2$   
 $H_y = AI_3$   
 $H_z = AI_4$

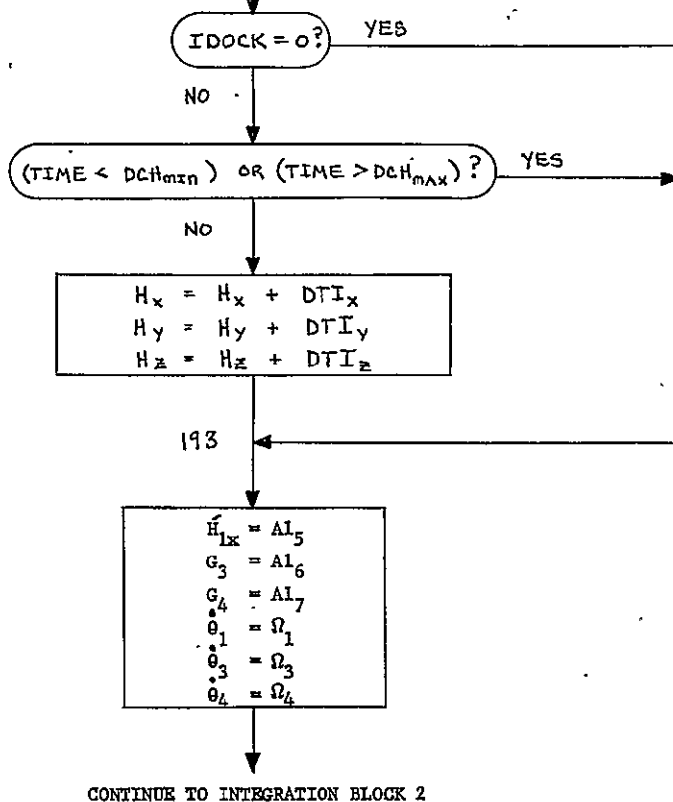
CONTINUE TO THE FOLLOWING PAGE

# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-54)

Application INTEGRATION BLOCK 1 CONTINUED Date OCTOBER 1970 Page 2 of 2  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

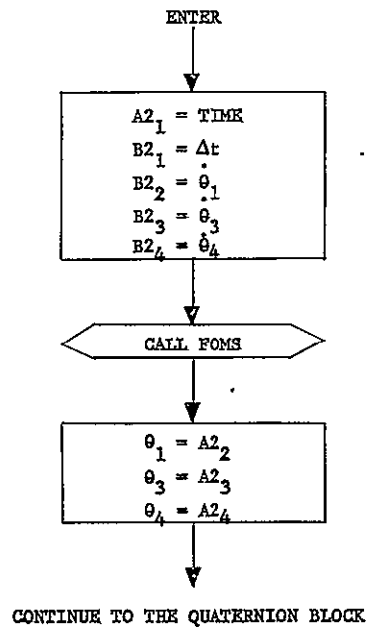
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# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application INTEGRATION BLOCK 2 Date OCTOBER 1970 Page 1 of 1  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON



# FLOW CHART & BLOCK DIAGRAM

Form DEN 1103-01 (2-64)

Application QUATERNION BLOCK Date OCTOBER 1970 Page 1 of 1  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

ENTER

$$[Q] = \frac{1}{2} \begin{bmatrix} 0. & -w_{0x} & -w_{0y} & -w_{0z} \\ w_{0x} & 0. & w_{0z} & -w_{0y} \\ w_{0y} & -w_{0z} & 0. & w_{0x} \\ w_{0z} & w_{0y} & -w_{0x} & 0. \end{bmatrix}$$

$$\begin{bmatrix} \lambda_2 \\ \lambda_3 \\ \lambda_4 \\ \lambda_5 \end{bmatrix} = [Q] \begin{bmatrix} \lambda_2 \\ \lambda_3 \\ \lambda_4 \\ \lambda_5 \end{bmatrix}$$

$A3_1 = \text{TIME}$   
 $B3_1 = \Delta t$   
 $B3_2 = \lambda_2$   
 $B3_3 = \lambda_3$   
 $B3_4 = \lambda_4$   
 $B3_5 = \lambda_5$

CALL FOMS

$$\begin{aligned} \lambda_2 &= A3_2 \\ \lambda_3 &= A3_3 \\ \lambda_4 &= A3_4 \\ \lambda_5 &= A3_5 \\ F_N &= \sqrt{\lambda_2^2 + \lambda_3^2 + \lambda_4^2 + \lambda_5^2} \\ \lambda_2 &= \lambda_2 / F_N \\ \lambda_3 &= \lambda_3 / F_N \\ \lambda_4 &= \lambda_4 / F_N \\ \lambda_5 &= \lambda_5 / F_N \\ T_{1,1} &= \lambda_2^2 + \lambda_3^2 - \lambda_4^2 - \lambda_5^2 \\ T_{1,2} &= 2 * (\lambda_3 \lambda_4 - \lambda_2 \lambda_5) \\ T_{1,3} &= 2 * (\lambda_3 \lambda_5 + \lambda_2 \lambda_4) \\ T_{2,1} &= 2 * (\lambda_3 \lambda_4 + \lambda_2 \lambda_5) \\ T_{2,2} &= \lambda_2^2 - \lambda_3^2 + \lambda_4^2 - \lambda_5^2 \\ T_{2,3} &= 2 * (\lambda_4 \lambda_5 - \lambda_2 \lambda_3) \\ T_{3,1} &= 2 * (\lambda_3 \lambda_5 - \lambda_2 \lambda_4) \\ T_{3,2} &= 2 * (\lambda_4 \lambda_5 + \lambda_2 \lambda_3) \\ T_{3,3} &= \lambda_2^2 - \lambda_3^2 - \lambda_4^2 + \lambda_5^2 \end{aligned}$$

CALL MULT

$$(I.E. [I, B] = [I, B] \cdot [F])$$

CALL MULT

$$(I.E. [R, ] = [I, B] [R])$$

CONTINUE TO THE CONTROL MODULE

# FLOW CHART & BLOCK DIAGRAM

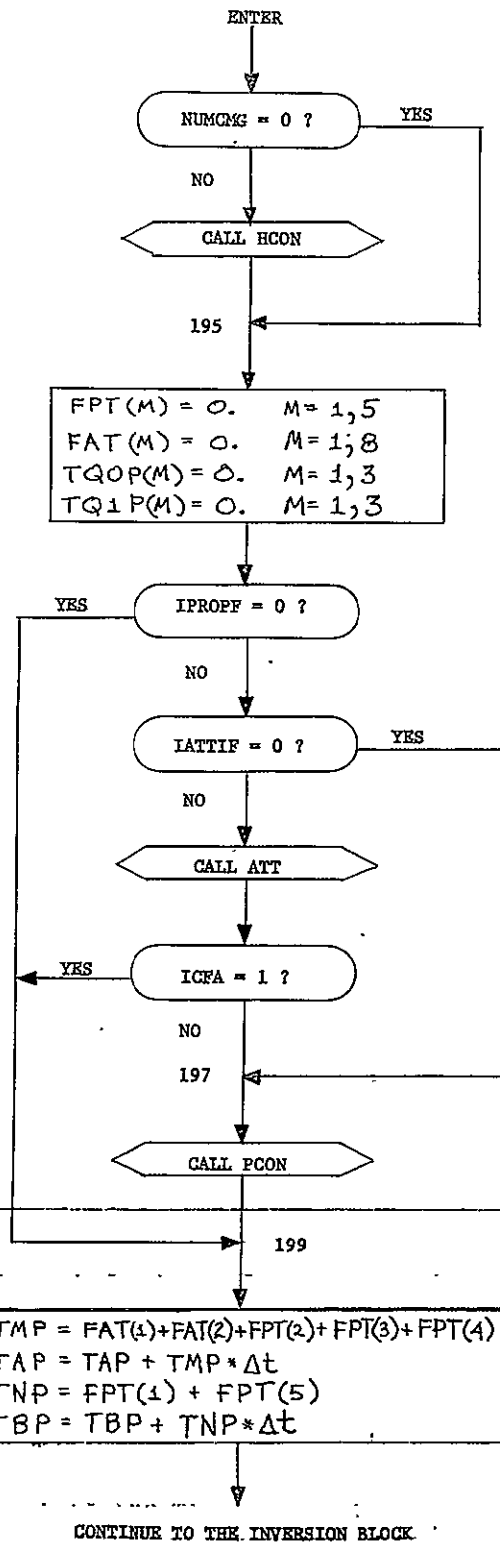
Application CONTROL MODULE

Date OCTOBER 1970

Page 1 of 1

Procedure

Drawn By GARY JOHNSON



# FLOW CHART & BLOCK DIAGRAM

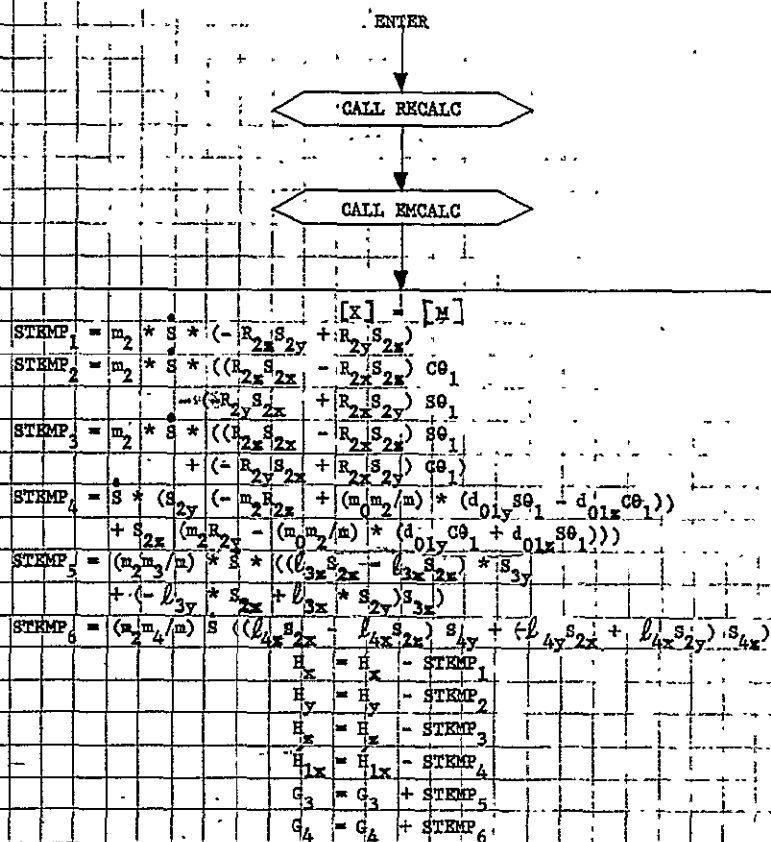
FORM DEN 1103-01 (4-64)

Application INVERSION BLOCK

Date OCTOBER 1970 Page 1 of 2

Procedure

Drawn By GARY JOHNSON

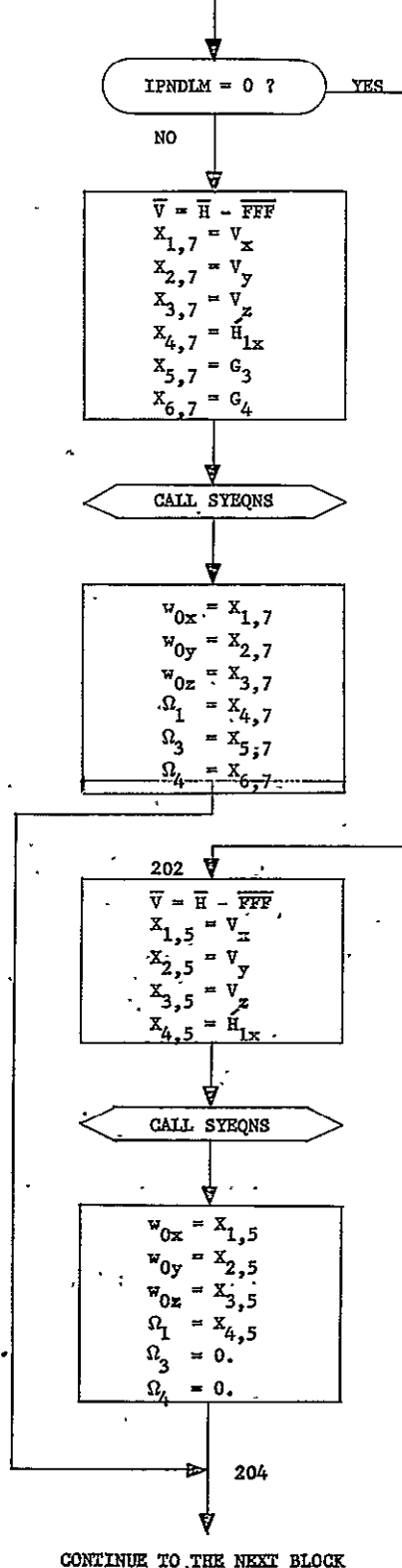


CONTINUE TO THE NEXT PAGE

# FLOW CHART & BLOCK DIAGRAM

Application INVERSION BLOCK CONTINUED Date OCTOBER 1970 Page 2 of 2  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

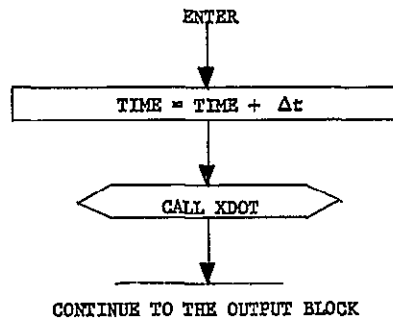
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# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

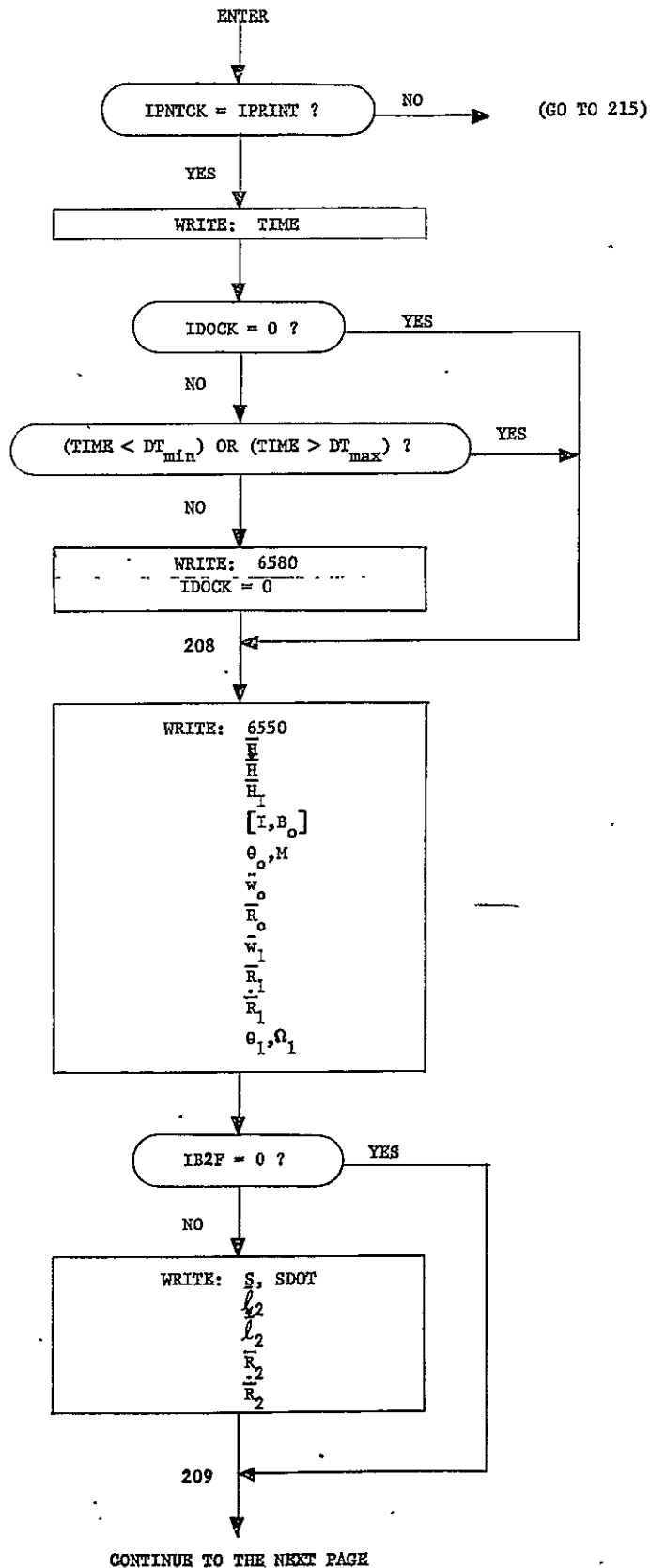
Application TIME UPDATE Date OCTOBER 1970 Page 1 of 1  
Procedure \_\_\_\_\_ Drawn By GARY JOHNSON





# FLOW CHART & BLOCK DIAGRAM

Application OUTPUT BLOCK Date OCTOBER 1970 Page 1 of 3  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON



# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application OUTPUT BLOCK CONTINUED

Date OCTOBER 1970

Page 2 of 2

Procedure

Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

209

IPNDLM = 0 ?

YES

NO

WRITE:

$\bar{w}_3$   
 $\bar{h}_3$   
 $\bar{l}_3$   
 $\bar{l}_3$   
 $\bar{r}_3$   
 $\bar{r}_3$   
 $\theta_3, \Omega_3$   
 $G_3, \dot{G}_3$   
 $\bar{w}_4$   
 $\bar{h}_4$   
 $\bar{l}_4$   
 $\bar{l}_4$   
 $\bar{r}_4$   
 $\bar{r}_4$   
 $\theta_4, \Omega_4$   
 $G_4, \dot{G}_4$

211

IPROPF = 0 ?

YES

NO

WRITE: TAP, TBP

212

NUMCMG = 0 ?

YES

NO

DO 213 J = 1, NUMCMG

WRITE:  $\theta_j, \dot{\theta}_j$

IF (IDOF(j)  $\neq$  2) GO TO 213

WRITE:  $\phi_j, \dot{\phi}_j$

213 CONTINUE

214

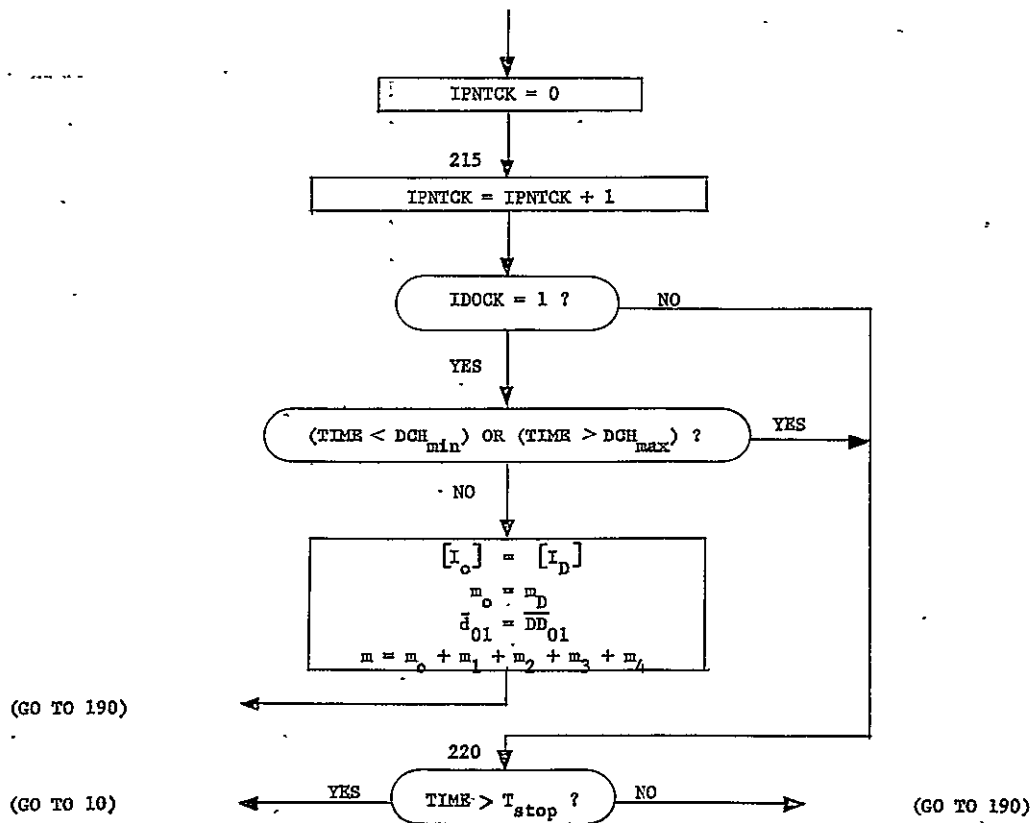
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# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application OUTPUT BLOCK CONTINUED Date OCTOBER 1970 Page 3 of 3  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE



# FLOW CHART & BLOCK DIAGRAM

FORM DEV 1102-01 (4-64)

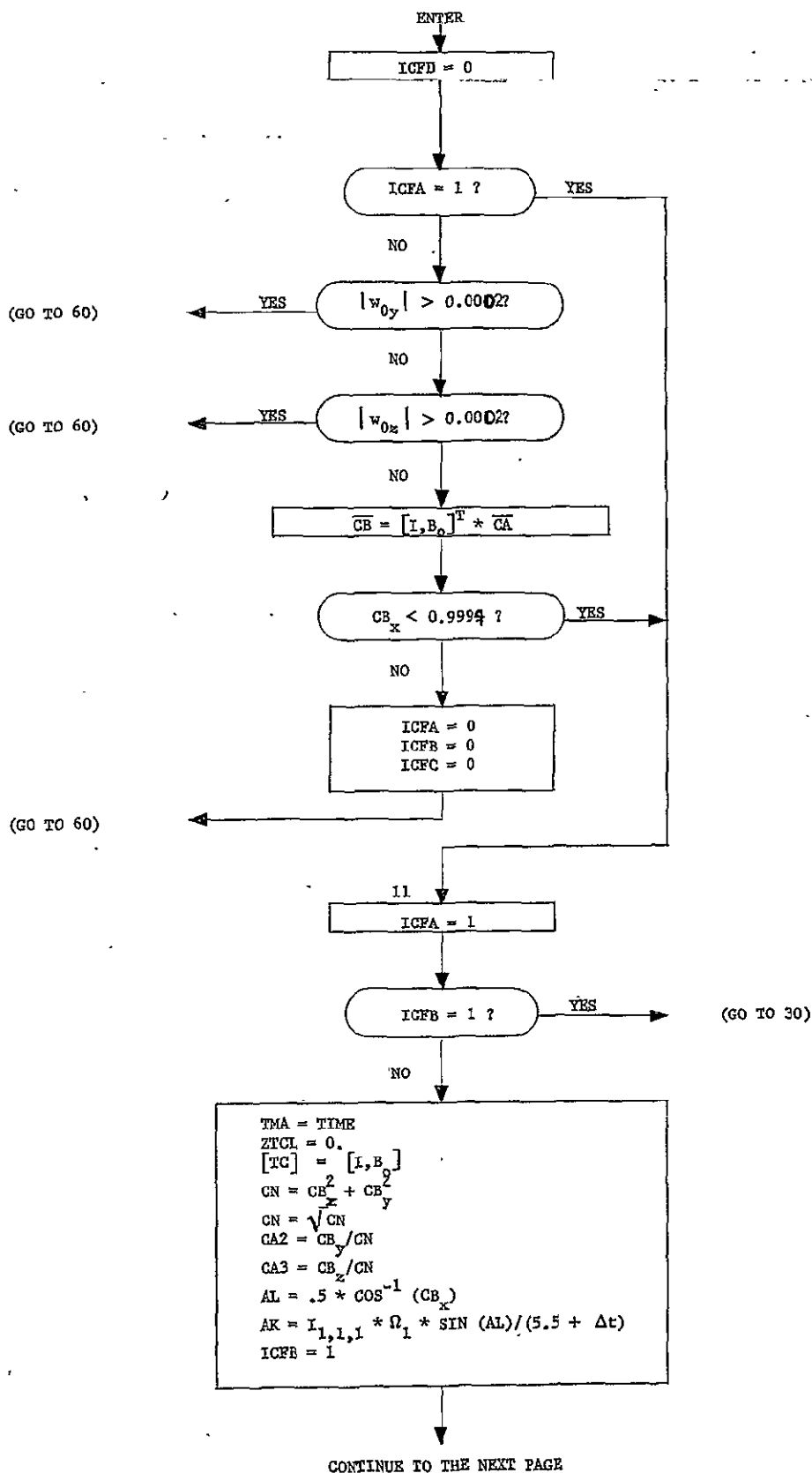
Application SUBROUTINE ATT

Date OCTOBER 1970

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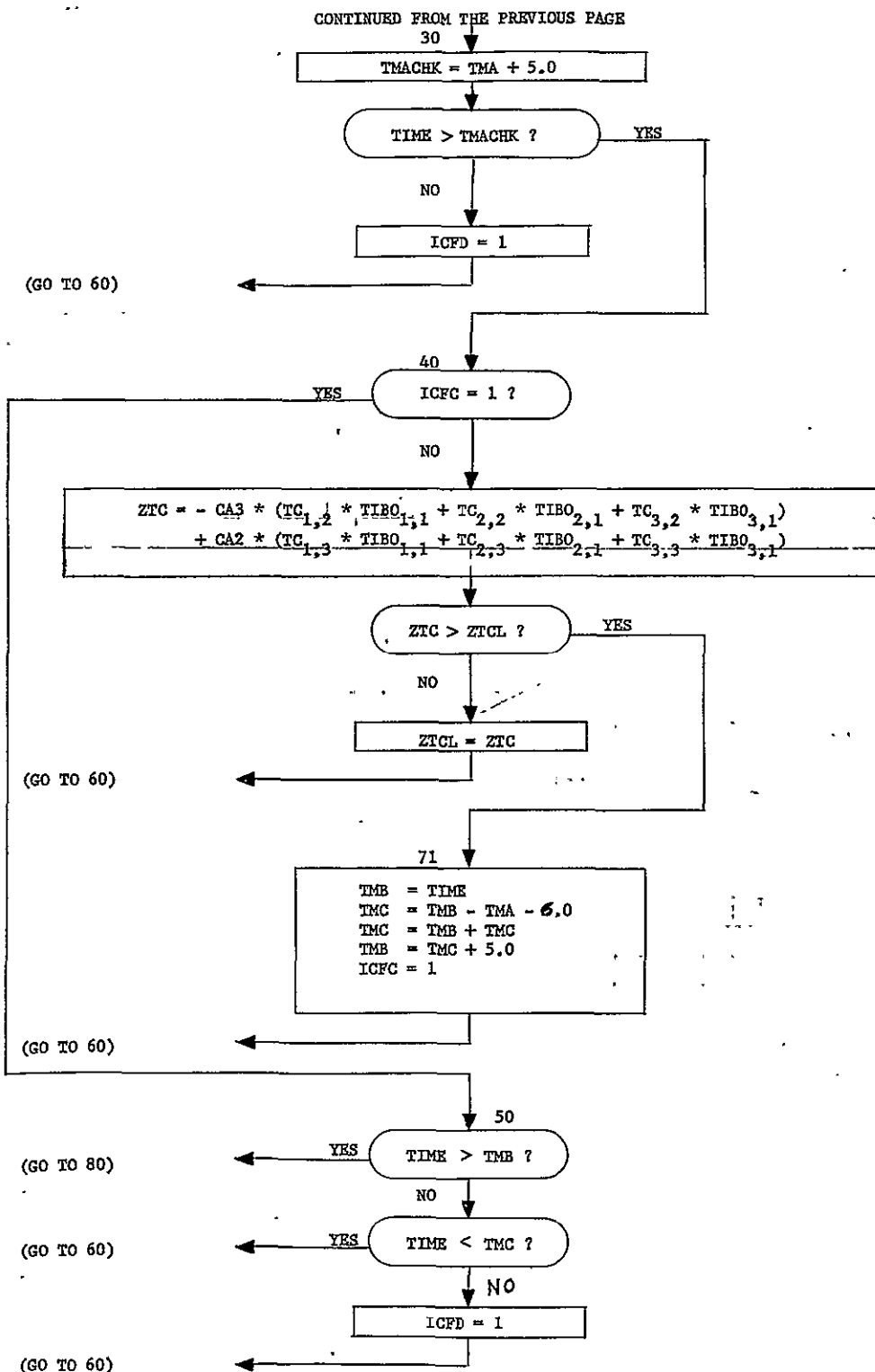
Procedure

Drawn By GARY JOHNSON



# FLOW CHART & BLOCK DIAGRAM

Application SUBROUTINE ATT CONTINUED Date OCTOBER 1970 Page 2 of 3  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON



CONTINUE TO THE NEXT PAGE

# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (1-64)

Application SUBROUTINE ATT CONTINUED

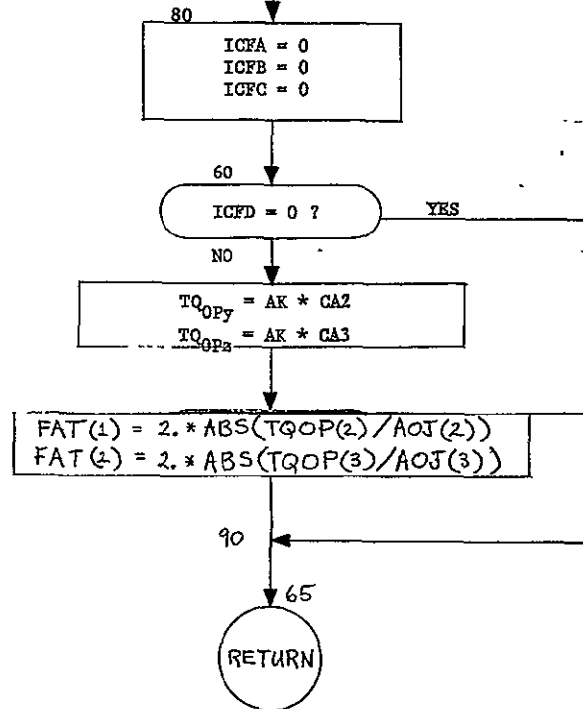
Date OCTOBER 1970

Page 3 of 3

Procedure \_\_\_\_\_

Drawn By GARY JOHNSON

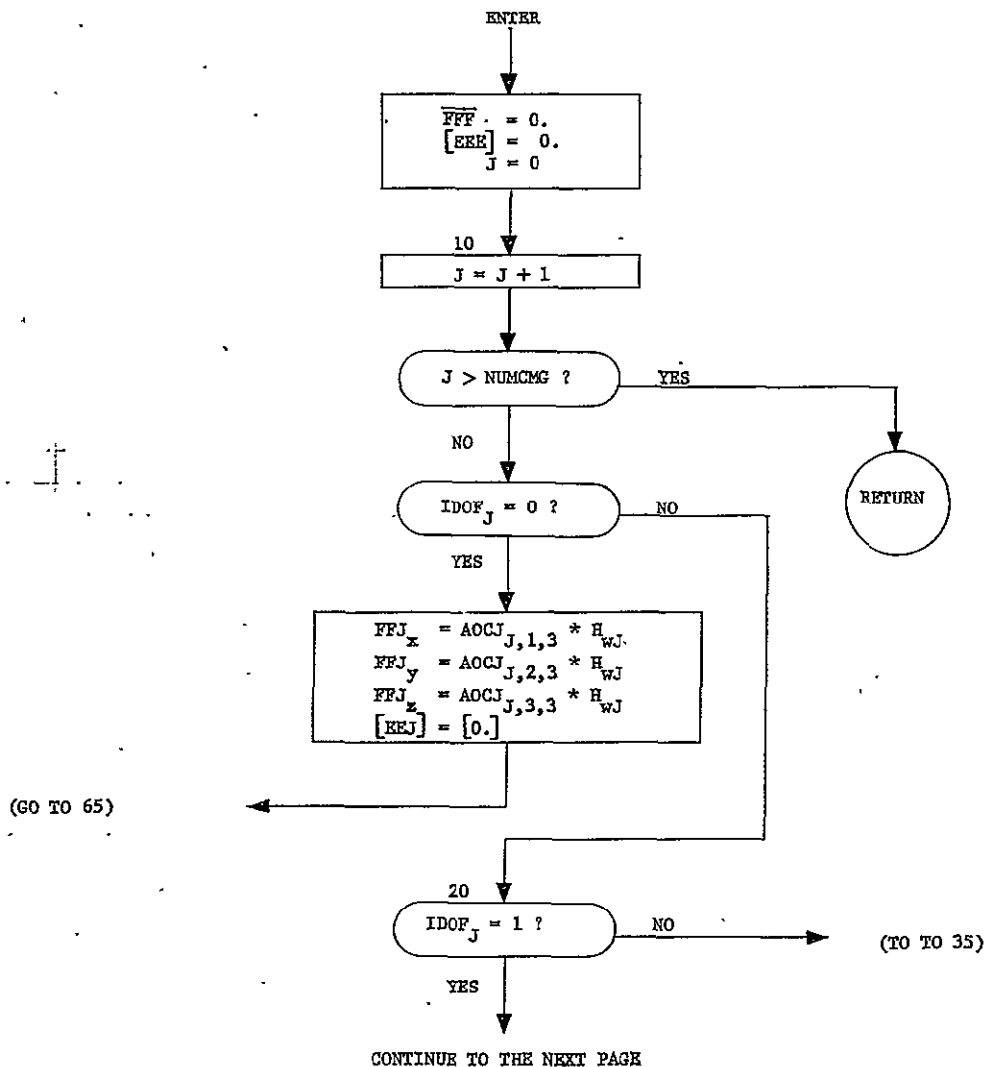
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# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application SUBROUTINE CMG Date OCTOBER 1970 Page 1 of 4  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON



# FLOW CHART & BLOCK DIAGRAM

Application SUBROUTINE CMG CONTINUED Date OCTOBER 1970 Page 2 of 4  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

```

TEMP12x = CθJ * AIIJ,1,2 * θJ + SθJ * AIIJ,3,2 * θJ + SθJ * HwJ
TEMP12y = SθJ * SθJ * AIIJ,1,2 * θJ + CθJ * AIIJ,2,2 * θJ - SθJ * CθJ * AIIJ,3,2 * θJ
TEMP12z = - SθJ * CθJ * AIIJ,1,2 * θJ + SθJ * AIIJ,2,2 * θJ
          + CθJ * CθJ * AIIJ,3,2 * θJ + HwJ * CθJ
FFJ      = [0, CJ] * TEMP12

TEMP131,1 = CθJ * AOCJJ,1,1 + SθJ * SθJ * AOCJJ,1,2 - SθJ * CθJ * AOCJJ,1,3
TEMP131,2 = CθJ * AOCJJ,2,1 + SθJ * SθJ * AOCJJ,2,2 - SθJ * CθJ * AOCJJ,2,3
TEMP131,3 = CθJ * AOCJJ,3,1 + SθJ * SθJ * AOCJJ,3,2 - SθJ * CθJ * AOCJJ,3,3
TEMP132,1 = CθJ * AOCJJ,1,2 + SθJ * AOCJJ,1,3
TEMP132,2 = CθJ * AOCJJ,2,2 + SθJ * AOCJJ,2,3
TEMP132,3 = CθJ * AOCJJ,3,2 + SθJ * AOCJJ,3,3
TEMP133,1 = SθJ * AOCJJ,1,1 - SθJ * CθJ * AOCJJ,1,2 + CθJ * CθJ * AOCJJ,1,3
TEMP133,2 = SθJ * AOCJJ,2,1 - SθJ * CθJ * AOCJJ,2,2 + CθJ * CθJ * AOCJJ,2,3
TEMP133,3 = SθJ * AOCJJ,3,1 - SθJ * CθJ * AOCJJ,3,2 + CθJ * CθJ * AOCJJ,3,3
[TEMP14] = [IIJ] * [TEMP13]
TEMP151,1 = CθJ * TEMP141,1 + SθJ * TEMP143,1
TEMP151,2 = CθJ * TEMP141,2 + SθJ * TEMP143,2
TEMP151,3 = CθJ * TEMP141,3 + SθJ * TEMP143,3
TEMP152,1 = SθJ * SθJ * TEMP141,1 + CθJ * TEMP142,1 - SθJ * CθJ * TEMP143,1
TEMP152,2 = SθJ * SθJ * TEMP141,2 + CθJ * TEMP142,2 - SθJ * CθJ * TEMP143,2
TEMP152,3 = SθJ * SθJ * TEMP141,3 + CθJ * TEMP142,3 - SθJ * CθJ * TEMP143,3
TEMP153,1 = - SθJ * CθJ * TEMP141,1 + SθJ * TEMP142,1 + CθJ * CθJ * TEMP143,1
TEMP153,2 = - SθJ * CθJ * TEMP141,2 + SθJ * TEMP142,2 + CθJ * CθJ * TEMP143,2
TEMP153,3 = - SθJ * CθJ * TEMP141,3 + SθJ * TEMP142,3 + CθJ * CθJ * TEMP143,3
[EEJ] = [0, CJ] * [TEMP15]
    
```

(GO TO 60)

CONTINUE TO THE NEXT PAGE



# FLOW CHART & BLOCK DIAGRAM

FORM DEV 1103-01 (4-66)

Application SUBROUTINE CMG CONTINUED Date OCTOBER 1970 Page 3 of 4  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

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```

TEMP1x = AIOJ,1,1 *  $\theta_J$ 
TEMP1y = C $\theta_J$  * AIOJ,2,1 *  $\theta_J$  - S $\theta_J$  * AIOJ,3,1 *  $\theta_J$ 
TEMP1z = S $\theta_J$  * AIOJ,2,1 *  $\theta_J$  + C $\theta_J$  * AIOJ,3,1 *  $\theta_J$ 
TEMP2x = C $\theta_J$  * [AIIJ,1,1 * C $\theta_J$  *  $\theta_J$  + AIIJ,1,2 *  $\theta_J$  + AIIJ,1,3 * S $\theta_J$  *  $\theta_J$ ]
    + S $\theta_J$  * [AIIJ,3,1 * C $\theta_J$  *  $\theta_J$  + AIIJ,3,2 *  $\theta_J$  + AIIJ,3,3 * S $\theta_J$  *  $\theta_J$ ]
TEMP2y = S $\theta_J$  * S $\theta_J$  * [AIIJ,1,1 * C $\theta_J$  *  $\theta_J$  + AIIJ,1,2 *  $\theta_J$  + AIIJ,1,3 * S $\theta_J$  *  $\theta_J$ ]
    + C $\theta_J$  * [AIIJ,2,1 * C $\theta_J$  *  $\theta_J$  + AIIJ,2,2 *  $\theta_J$  + AIIJ,2,3 * S $\theta_J$  *  $\theta_J$ ]
    - S $\theta_J$  * C $\theta_J$  * [AIIJ,3,1 * C $\theta_J$  *  $\theta_J$  + AIIJ,3,2 *  $\theta_J$  + AIIJ,3,3 * S $\theta_J$  *  $\theta_J$ ]
TEMP2z = - S $\theta_J$  * C $\theta_J$  * [AIIJ,1,1 * C $\theta_J$  *  $\theta_J$  + AIIJ,1,2 *  $\theta_J$  + AIIJ,1,3 * S $\theta_J$  *  $\theta_J$ ]
    + S $\theta_J$  * [AIIJ,2,1 * C $\theta_J$  *  $\theta_J$  + AIIJ,2,2 *  $\theta_J$  + AIIJ,2,3 * S $\theta_J$  *  $\theta_J$ ]
    + C $\theta_J$  * C $\theta_J$  * [AIIJ,3,1 * C $\theta_J$  *  $\theta_J$  + AIIJ,3,2 *  $\theta_J$  + AIIJ,3,3 * S $\theta_J$  *  $\theta_J$ ]
TEMP3x = HwJ * S $\theta_J$ 
TEMP3y = - HwJ * C $\theta_J$  * S $\theta_J$ 
TEMP3z = HwJ * C $\theta_J$  * C $\theta_J$ 
TEMP4 = TEMP1 + TEMP2 + TEMP3
FFJ = [0, C $\theta_J$ ] * TEMP4
TEMP51,1 = AOCJJ,1,1
TEMP51,2 = AOCJJ,2,1
TEMP51,3 = AOCJJ,3,1
TEMP52,1 = C $\theta_J$  * AOCJJ,1,2 + S $\theta_J$  * AOCJJ,1,3
TEMP52,2 = C $\theta_J$  * AOCJJ,2,2 + S $\theta_J$  * AOCJJ,2,3
TEMP52,3 = C $\theta_J$  * AOCJJ,3,2 + S $\theta_J$  * AOCJJ,3,3
TEMP53,1 = - S $\theta_J$  * AOCJJ,1,2 + C $\theta_J$  * AOCJJ,1,3
TEMP53,2 = - S $\theta_J$  * AOCJJ,2,2 + C $\theta_J$  * AOCJJ,2,3
TEMP53,3 = - S $\theta_J$  * AOCJJ,3,2 + C $\theta_J$  * AOCJJ,3,3
TEMP6 = [IOJ] * TEMP5
TEMP71,1 = TEMP61,1
TEMP71,2 = TEMP61,2
TEMP71,3 = TEMP61,3
TEMP72,1 = C $\theta_J$  * TEMP62,1 - S $\theta_J$  * TEMP63,1
TEMP72,2 = C $\theta_J$  * TEMP62,2 - S $\theta_J$  * TEMP63,2
TEMP72,3 = C $\theta_J$  * TEMP62,3 - S $\theta_J$  * TEMP63,3
TEMP73,1 = S $\theta_J$  * TEMP62,1 + C $\theta_J$  * TEMP63,1
TEMP73,2 = S $\theta_J$  * TEMP62,2 + C $\theta_J$  * TEMP63,2
TEMP73,3 = S $\theta_J$  * TEMP62,3 + C $\theta_J$  * TEMP63,3
TEMP81,1 = C $\theta_J$  * AOCJJ,1,1 + S $\theta_J$  * S $\theta_J$  * AOCJJ,1,2 - S $\theta_J$  * C $\theta_J$  * AOCJJ,1,3
TEMP81,2 = C $\theta_J$  * AOCJJ,2,1 + S $\theta_J$  * S $\theta_J$  * AOCJJ,2,2 - S $\theta_J$  * C $\theta_J$  * AOCJJ,2,3
TEMP81,3 = C $\theta_J$  * AOCJJ,3,1 + S $\theta_J$  * S $\theta_J$  * AOCJJ,3,2 - S $\theta_J$  * C $\theta_J$  * AOCJJ,3,3
TEMP82,1 = C $\theta_J$  * AOCJJ,1,2 + S $\theta_J$  * AOCJJ,1,3
TEMP82,2 = C $\theta_J$  * AOCJJ,2,2 + S $\theta_J$  * AOCJJ,2,3
TEMP82,3 = C $\theta_J$  * AOCJJ,3,2 + S $\theta_J$  * AOCJJ,3,3
TEMP83,1 = S $\theta_J$  * AOCJJ,1,1 - S $\theta_J$  * C $\theta_J$  * AOCJJ,1,2 + C $\theta_J$  * C $\theta_J$  * AOCJJ,1,3
TEMP83,2 = S $\theta_J$  * AOCJJ,2,1 - S $\theta_J$  * C $\theta_J$  * AOCJJ,2,2 + C $\theta_J$  * C $\theta_J$  * AOCJJ,2,3
TEMP83,3 = S $\theta_J$  * AOCJJ,3,1 - S $\theta_J$  * C $\theta_J$  * AOCJJ,3,2 + C $\theta_J$  * C $\theta_J$  * AOCJJ,3,3
    
```

CONTINUE TO THE NEXT PAGE

# FLOW CHART & BLOCK DIAGRAM

PL-00 074 1103-01 (4-54)

Application SUBROUTINE CMG CONTINUED Date OCTOBER 1970 Page 4 of 4  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

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```

[TEMP9] = [IIJ] [TEMP8]
TEMP101,1 = C0J * TEMP91,1 + S0J * TEMP93,1
TEMP101,2 = C0J * TEMP91,2 + S0J * TEMP93,2
TEMP101,3 = C0J * TEMP91,3 + S0J * TEMP93,3
TEMP102,1 = S0J * S0J * TEMP91,1 + C0J * TEMP92,1 - S0J * C0J * TEMP93,1
TEMP102,2 = S0J * S0J * TEMP91,2 + C0J * TEMP92,2 - S0J * C0J * TEMP93,2
TEMP102,3 = S0J * S0J * TEMP91,3 + C0J * TEMP92,3 - S0J * C0J * TEMP93,3
TEMP103,1 = -S0J * C0J * TEMP91,1 + S0J * TEMP92,1 + C0J * C0J * TEMP93,1
TEMP103,2 = -S0J * C0J * TEMP91,2 + S0J * TEMP92,2 + C0J * C0J * TEMP93,2
TEMP103,3 = -S0J * C0J * TEMP91,3 + S0J * TEMP92,3 + C0J * C0J * TEMP93,3
[TEMP11] = [TEMP7] + [TEMP10]
[EEJ] = [0,CJ] * [TEMP11]
    
```

```

0J = 0J + 0J * Δt
0J = 0J + 0J * Δt
    
```

65

```

FFF = FFF + FFJ
[EEE] = [EEK] + [EEJ]
    
```

(GO TO 10)

# FLOW CHART & BLOCK DIAGRAM

FEAR DEC 1103-01 (4-62)

Application SUBROUTINE EMGALC Date OCTOBER 1970 Page 1 of 4  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

ENTER

$$M_{1,1} = I_{0,1,1} + I_{1,1,1} + m_1 * d_{01y} * (R_{1y}C_{01} - R_{1x}S_{01}) + m_1 * d_{01x} * (R_{1y}S_{01} + R_{1x}C_{01}) \\
+ m_2 * (R_{2y}C_{01} - R_{2x}S_{01}) * (d_{01y} + l_{2y}C_{01} - l_{2x}S_{01}) \\
+ m_2 * (R_{2y}S_{01} + R_{2x}C_{01}) * (d_{01x} + l_{2y}S_{01} + l_{2x}C_{01}) \\
+ m_3 * (R_{3y}C_{01} - R_{3x}S_{01}) * (d_{01y} + d_{13y}C_{01} - d_{13x}S_{01} + l_{3y}C_{01} - l_{3x}S_{01}) \\
+ m_3 * (R_{3y}S_{01} + R_{3x}C_{01}) * (d_{01x} + d_{13y}S_{01} + d_{13x}C_{01} + l_{3y}S_{01} + l_{3x}C_{01}) \\
+ m_4 * (R_{4y}C_{01} - R_{4x}S_{01}) * (d_{01y} + d_{14y}C_{01} - d_{14x}S_{01} + l_{4y}C_{01} - l_{4x}S_{01}) \\
+ m_4 * (R_{4y}S_{01} + R_{4x}C_{01}) * (d_{01x} + d_{14y}S_{01} + d_{14x}C_{01} + l_{4y}S_{01} + l_{4x}C_{01})$$

$$M_{1,2} = I_{0,1,2} + I_{1,1,2} * C_{01} - I_{1,1,3} * S_{01} - m_1 * R_{1x} * d_{01y} \\
- m_2 * R_{2x} * (d_{01y} + l_{2y}C_{01} - l_{2x}S_{01}) \\
- m_3 * R_{3x} * (d_{01y} + d_{13y}C_{01} - d_{13x}S_{01} + l_{3y}C_{01} - l_{3x}S_{01}) \\
- m_4 * R_{4x} * (d_{01y} + d_{14y}C_{01} - d_{14x}S_{01} + l_{4y}C_{01} - l_{4x}S_{01})$$

$$M_{1,3} = I_{0,1,3} + I_{1,1,2} * S_{01} + I_{1,1,3} * C_{01} - m_1 * R_{1x} * d_{01x} \\
- m_2 * R_{2x} * (d_{01x} + l_{2y}S_{01} + l_{2x}C_{01}) \\
- m_3 * R_{3x} * (d_{01x} + d_{13y}S_{01} + d_{13x}C_{01} + l_{3y}S_{01} + l_{3x}C_{01}) \\
- m_4 * R_{4x} * (d_{01x} + d_{14y}S_{01} + d_{14x}C_{01} + l_{4y}S_{01} + l_{4x}C_{01})$$

$$M_{1,4} = I_{1,1,1} - m_1 * d_{01x} * ((m_o/m) * d_{01x} - R_{1y}S_{01} - R_{1x}C_{01}) \\
+ m_1 * d_{01y} * (R_{1y}C_{01} - R_{1x}S_{01} - (m_o/m) * d_{01y}) \\
- m_2 * (d_{01x} + l_{2y}S_{01} + l_{2x}C_{01}) * ((m_o/m) * d_{01x} - R_{2y}S_{01} - R_{2x}C_{01}) \\
+ m_2 * (d_{01y} + l_{2y}C_{01} - l_{2x}S_{01}) * (R_{2y}C_{01} - R_{2x}S_{01} - (m_o/m) * d_{01y}) \\
- m_3 * (d_{01x} + (d_{13y} + l_{3y})S_{01} + (d_{13x} + l_{3x}) * C_{01}) * ((m_o/m) * d_{01x} - R_{3y}S_{01} - R_{3x}C_{01}) \\
+ m_3 * (d_{01y} + (d_{13y} + l_{3y})C_{01} - (d_{13x} + l_{3x}) * S_{01}) * (R_{3y}C_{01} - R_{3x}S_{01} - (m_o/m) * d_{01y}) \\
- m_4 * (d_{01x} + (d_{14y} + l_{4y})S_{01} + (d_{14x} + l_{4x}) * C_{01}) * ((m_o/m) * d_{01x} - R_{4y}S_{01} - R_{4x}C_{01}) \\
+ m_4 * (d_{01y} + (d_{14y} + l_{4y})C_{01} - (d_{14x} + l_{4x}) * S_{01}) * (R_{4y}C_{01} - R_{4x}S_{01} - (m_o/m) * d_{01y})$$

$$M_{1,5} = -m_3 * R_{3x} * (S_{3x} * l_{3x} - S_{3x} * l_{3y}) \\
+ m_3 * R_{3y} * (-S_{3y} * l_{3x} + S_{3x} * l_{3y})$$

$$M_{1,6} = -m_4 * R_{4x} * (S_{4x} * l_{4x} - S_{4x} * l_{4y}) \\
+ m_4 * R_{4y} * (-S_{4y} * l_{4x} + S_{4x} * l_{4y})$$

$$M_{2,1} = I_{0,2,1} + I_{1,2,1} * C_{01} - I_{1,3,1} * S_{01} - m_1 * d_{01x} * (R_{1y}C_{01} - R_{1x}S_{01}) \\
- m_2 * (R_{2y}C_{01} - R_{2x}S_{01}) * (d_{01x} + l_{2x}) \\
- m_3 * (R_{3y}C_{01} - R_{3x}S_{01}) * (d_{01x} + d_{13x} + l_{3x}) \\
- m_4 * (R_{4y}C_{01} - R_{4x}S_{01}) * (d_{01x} + d_{14x} + l_{4x})$$

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# FLOW CHART & BLOCK DIAGRAM

Application SUBROUTINE EMCALC CONTINUED Date OCTOBER 1970 Page 2 of 4  
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CONTINUED FROM THE PREVIOUS PAGE

$$\begin{aligned} M_{2,2} = & I_{0,2,2} + I_{1,2,2} C\theta_1^2 - I_{1,2,3} C\theta_1 S\theta_1 - I_{1,3,2} * C\theta_1 S\theta_1 + I_{1,3,3} * S\theta_1^2 \\ & + m_1 * R_{1x} * d_{01x} + m_1 * d_{01x} * (R_{1y} S\theta_1 + R_{1z} C\theta_1) \\ & + m_2 * R_{2x} * (d_{01x} + l_{2x}) + m_2 * (R_{2y} S\theta_1 + R_{2z} C\theta_1) * (d_{01x} + l_{2y} S\theta_1 + l_{2z} C\theta_1) \\ & + m_3 * R_{3x} * (d_{01x} + d_{13x} + l_{3x}) \\ & + m_3 * (R_{3y} S\theta_1 + R_{3z} C\theta_1) * (d_{01x} + d_{13y} S\theta_1 + d_{13z} C\theta_1 + l_{3y} S\theta_1 + l_{3z} C\theta_1) \\ & + m_4 * R_{4x} * (d_{01x} + d_{14x} + l_{4x}) \\ & + m_4 * (R_{4y} S\theta_1 + R_{4z} C\theta_1) * (d_{01x} + d_{14y} S\theta_1 + d_{14z} C\theta_1 + l_{4y} S\theta_1 + l_{4z} C\theta_1) \end{aligned}$$

$$\begin{aligned} M_{2,3} = & I_{0,2,3} + I_{1,2,2} C\theta_1 S\theta_1 + I_{1,2,3} * C\theta_1^2 - I_{1,3,2} * S\theta_1^2 - I_{1,3,3} * C\theta_1 S\theta_1 \\ & - m_1 * d_{01x} * (R_{1y} C\theta_1 - R_{1z} S\theta_1) \\ & - m_2 * (R_{2y} C\theta_1 - R_{2z} S\theta_1) * (d_{01x} + l_{2y} S\theta_1 + l_{2z} C\theta_1) \\ & - m_3 * (R_{3y} C\theta_1 - R_{3z} S\theta_1) * (d_{01x} + d_{13y} S\theta_1 + d_{13z} C\theta_1 + l_{3y} S\theta_1 + l_{3z} C\theta_1) \\ & - m_4 * (R_{4y} C\theta_1 - R_{4z} S\theta_1) * (d_{01x} + d_{14y} S\theta_1 + d_{14z} C\theta_1 + l_{4y} S\theta_1 + l_{4z} C\theta_1) \end{aligned}$$

$$\begin{aligned} M_{2,4} = & I_{1,1,2} * C\theta_1 - I_{1,1,3} * S\theta_1 - m_1 * d_{01x} * R_{1y} C\theta_1 \\ & + m_1 * d_{01x} * R_{1z} S\theta_1 + (m_o/m) * m_1 * d_{01x} * d_{01y} \\ & - m_2 * (d_{01x} + l_{2x}) * (R_{2y} C\theta_1 - R_{2z} S\theta_1 - (m_o/m) * d_{01y}) \\ & - m_3 * (d_{01x} + d_{13x} + l_{3x}) * (R_{3y} C\theta_1 - R_{3z} S\theta_1 - (m_o/m) * d_{01y}) \\ & - m_4 * (d_{01x} + d_{14x} + l_{4x}) * (R_{4y} C\theta_1 - R_{4z} S\theta_1 - (m_o/m) * d_{01y}) \end{aligned}$$

$$\begin{aligned} M_{2,5} = & (m_3 * R_{3x} * (-S_{3x} * l_{3y} + S_{3y} * l_{3x}) \\ & - m_3 * R_{3x} * (-S_{3y} * l_{3x} + S_{3x} * l_{3y})) * C\theta_1 \\ & - (-m_3 * R_{3y} * (-S_{3x} * l_{3y} + S_{3y} * l_{3x}) \\ & + m_3 * R_{3x} * (S_{3x} * l_{3x} - S_{3x} * l_{3x})) * S\theta_1 \end{aligned}$$

$$\begin{aligned} M_{2,6} = & (m_4 * R_{4x} * (-S_{4x} * l_{4y} + S_{4y} * l_{4x}) \\ & - m_4 * R_{4x} * (-S_{4y} * l_{4x} + S_{4x} * l_{4y})) * C\theta_1 \\ & - (-m_4 * R_{4y} * (-S_{4x} * l_{4y} + S_{4y} * l_{4x}) \\ & + m_4 * R_{4x} * (S_{4x} * l_{4x} - S_{4x} * l_{4x})) * S\theta_1 \end{aligned}$$

$$\begin{aligned} M_{3,1} = & I_{0,3,1} + I_{1,2,1} * S\theta_1 + I_{1,3,1} * C\theta_1 - m_1 * d_{01x} * (R_{1y} S\theta_1 + R_{1z} C\theta_1) \\ & - m_2 * (d_{01x} + l_{2x}) * (R_{2y} S\theta_1 + R_{2z} C\theta_1) \\ & - m_3 * (d_{01x} + d_{13x} + l_{3x}) * (R_{3y} S\theta_1 + R_{3z} C\theta_1) \\ & - m_4 * (d_{01x} + d_{14x} + l_{4x}) * (R_{4y} S\theta_1 + R_{4z} C\theta_1) \end{aligned}$$

$$\begin{aligned} M_{3,2} = & I_{0,3,2} + I_{1,2,2} * C\theta_1 * S\theta_1 - I_{1,2,3} * S\theta_1^2 + I_{1,3,2} * C\theta_1^2 - I_{1,3,3} * C\theta_1 * S\theta_1 \\ & - m_1 * d_{01y} * (R_{1y} S\theta_1 + R_{1z} C\theta_1) \\ & - m_2 * (R_{2y} S\theta_1 + R_{2z} C\theta_1) * (d_{01y} + l_{2y} C\theta_1 - l_{2x} S\theta_1) \\ & - m_3 * (R_{3y} S\theta_1 + R_{3z} C\theta_1) * (d_{01y} + d_{13y} C\theta_1 - d_{13x} S\theta_1 + l_{3y} C\theta_1 - l_{3x} S\theta_1) \\ & - m_4 * (R_{4y} S\theta_1 + R_{4z} C\theta_1) * (d_{01y} + d_{14y} C\theta_1 - d_{14x} S\theta_1 + l_{4y} C\theta_1 - l_{4x} S\theta_1) \end{aligned}$$

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$$\begin{aligned}
 M_{3,3} = & I_{0,3,3} + I_{1,2,2} * S\theta_1^2 + I_{1,2,3} * C\theta_1 * S\theta_1 + I_{1,3,2} * C\theta_1 * S\theta_1 + I_{1,3,3} * C\theta_1^2 \\
 & + m_1 * R_{1x} * d_{01x} + m_1 * (R_{1y} * C\theta_1 - R_{1z} * S\theta_1) * d_{01y} + m_2 * R_{2x} * (d_{01x} + l_{2x}) \\
 & + m_2 * (R_{2y} * C\theta_1 - R_{2z} * S\theta_1) * (d_{01y} + l_{2y} * C\theta_1 - l_{2z} * S\theta_1) \\
 & + m_3 * R_{3x} * (d_{01x} + d_{13x} + l_{3x}) \\
 & + m_3 * (R_{3y} * C\theta_1 - R_{3z} * S\theta_1) * (d_{01y} + d_{13y} * C\theta_1 - d_{13z} * S\theta_1 + l_{3y} * C\theta_1 - l_{3z} * S\theta_1) \\
 & + m_4 * R_{4x} * (d_{01x} + d_{14x} + l_{4x}) \\
 & + m_4 * (R_{4y} * C\theta_1 - R_{4z} * S\theta_1) * (d_{01y} + d_{14y} * C\theta_1 - d_{14z} * S\theta_1 + l_{4y} * C\theta_1 - l_{4z} * S\theta_1)
 \end{aligned}$$

$$\begin{aligned}
 M_{3,4} = & I_{1,1,2} * S\theta_1 + I_{1,1,3} * C\theta_1 \\
 & + m_1 * d_{01x} * ((m_o/m) * d_{01x} - R_{1y} * S\theta_1 - R_{1z} * C\theta_1) \\
 & + m_2 * (d_{01x} + l_{2x}) * ((m_o/m) * d_{01x} - R_{2y} * S\theta_1 - R_{2z} * C\theta_1) \\
 & + m_3 * (d_{01x} + d_{13x} + l_{3x}) * ((m_o/m) * d_{01x} - R_{3y} * S\theta_1 - R_{3z} * C\theta_1) \\
 & + m_4 * (d_{01x} + d_{14x} + l_{4x}) * ((m_o/m) * d_{01x} - R_{4y} * S\theta_1 - R_{4z} * C\theta_1)
 \end{aligned}$$

$$\begin{aligned}
 M_{3,5} = & (m_3 * R_{3x} * (-S_{3x} * l_{3y} + S_{3y} * l_{3x}) \\
 & - m_3 * R_{3x} * (-S_{3y} * l_{3x} + S_{3x} * l_{3y})) * S\theta_1 \\
 & + (-m_3 * R_{3y} * (-S_{3x} * l_{3y} + S_{3y} * l_{3x}) \\
 & + m_3 * R_{3x} * (S_{3x} * l_{3x} - S_{3z} * l_{3z})) * C\theta_1
 \end{aligned}$$

$$\begin{aligned}
 M_{3,6} = & (m_4 * R_{4x} * (-S_{4x} * l_{4y} + S_{4y} * l_{4x}) \\
 & - m_4 * R_{4x} * (-S_{4y} * l_{4x} + S_{4x} * l_{4y})) * S\theta_1 \\
 & + (-m_4 * R_{4y} * (-S_{4x} * l_{4y} + S_{4y} * l_{4x}) \\
 & + m_4 * R_{4x} * (S_{4x} * l_{4x} - S_{4z} * l_{4z})) * C\theta_1
 \end{aligned}$$

DEFINE SOME REOCCURRING TERMS

$$SR_3 = m_3 * (d_{13y} + l_{3y})$$

$$SR_4 = m_3 * (d_{13x} + l_{3x})$$

$$SR_5 = m_4 * (d_{14y} + l_{4y})$$

$$SR_6 = m_4 * (d_{14x} + l_{4x})$$

$$SR_1 = I_{1,1,2} - m_2 * l_{2y} * R_{2x} - SR_3 * R_{3x} - SR_5 * R_{4x}$$

$$SR_2 = I_{1,1,3} - m_2 * l_{2x} * R_{2x} - SR_4 * R_{3x} - SR_6 * R_{4x}$$

$$M_{4,1} = I_{1,1,1} + m_2 * (l_{2x} * R_{2x} + l_{2y} * R_{2y}) + SR_4 * R_{3x} + SR_3 * R_{3y} + SR_6 * R_{4x} + SR_5 * R_{4y}$$

$$M_{4,2} = SR_1 * C\theta_1 - SR_2 * S\theta_1$$

$$M_{4,3} = SR_1 * S\theta_1 + SR_2 * C\theta_1$$

REDEFINE SR<sub>1</sub> AND SR<sub>2</sub>

$$SR_1 = (m_o/m) * (d_{01y} * C\theta_1 + d_{01x} * S\theta_1)$$

$$SR_2 = (m_o/m) * (-d_{01y} * S\theta_1 + d_{01x} * C\theta_1)$$

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# FLOW CHART & BLOCK DIAGRAM

Application SUBROUTINE EMGALG CONTINUED

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Procedure

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$$M_{4,4} = I_{1,1,1} + m_2 * (l_{2x} * (R_{2x} - SR_2) + l_{2y} * (R_{2y} - SR_1)) \\ + SR_4 * (R_{3x} - SR_2) + SR_3 * (R_{3y} - SR_1) + SR_6 * (R_{4x} - SR_2) + SR_5 * (R_{4y} - SR_1)$$

$$M_{4,5} = m_3 * ((R_{3x} - SR_2) * l_{3x} + (R_{3y} - SR_1) * l_{3y}) * S_{3x} \\ - (R_{3y} - SR_1) * l_{3x} * S_{3y} - (R_{3x} - SR_2) * l_{3x} * S_{3z}$$

$$M_{4,6} = m_4 * ((R_{4x} - SR_2) * l_{4x} + (R_{4y} - SR_1) * l_{4y}) * S_{4x} \\ - (R_{4y} - SR_1) * l_{4x} * S_{4y} - (R_{4x} - SR_2) * l_{4x} * S_{4z}$$

$$M_{5,1} = -m_3 * l_{3x} * (R_{3y} * S_{3y} + R_{3z} * S_{3z})$$

$$M_{5,2} = m_3 * ((l_{3x} * R_{3x} + l_{3x} * R_{3x}) * C\theta_1 + l_{3x} * R_{3y} * S\theta_1) * S_{3y} \\ + (-l_{3y} * R_{3x} * C\theta_1 - (l_{3y} * R_{3y} + l_{3x} * R_{3x}) * S\theta_1) * S_{3z}$$

$$M_{5,3} = m_3 * ((l_{3x} * R_{3x} + l_{3x} * R_{3x}) * S\theta_1 - l_{3x} * R_{3y} * C\theta_1) * S_{3y} \\ + (-l_{3y} * R_{3x} * S\theta_1 + (l_{3y} * R_{3y} + l_{3x} * R_{3x}) * C\theta_1) * S_{3z}$$

$$M_{5,4} = m_3 * l_{3x} * ((-R_{3y} + SR_1) * S_{3y} + (-R_{3z} + SR_2) * S_{3z})$$

$$M_{5,5} = m_3 * (1. - m_3/TOTMAS) * (((l_{3x}^2 + l_{3x}^2) * S_{3y} \\ - l_{3x} * l_{3y} * S_{3z}) * S_{3y} + ((l_{3y}^2 + l_{3x}^2) * S_{3x} - l_{3y} * l_{3x} * S_{3y}) * S_{3z})$$

$$M_{5,6} = (m_3 * m_4/m) * ((-l_{3x} * l_{4x} + l_{3x} * l_{4x}) * S_{4y} + l_{3x} * l_{4y} * S_{4z}) * S_{3y} \\ + (-l_{3y} * l_{4y} + l_{3x} * l_{4x}) * S_{4z} + l_{3y} * l_{4x} * S_{4y}) * S_{3z}$$

$$M_{6,1} = -m_4 * l_{4x} * (R_{4y} * S_{4y} + R_{4z} * S_{4z})$$

$$M_{6,2} = m_4 * ((l_{4x} * R_{4x} + l_{4x} * R_{4x}) * C\theta_1 + l_{4x} * R_{4y} * S\theta_1) * S_{4y} \\ + (-l_{4y} * R_{4x} * C\theta_1 - (l_{4y} * R_{4y} + l_{4x} * R_{4x}) * S\theta_1) * S_{4z}$$

$$M_{6,3} = m_4 * ((l_{4x} * R_{4x} + l_{4x} * R_{4x}) * S\theta_1 - l_{4x} * R_{4y} * C\theta_1) * S_{4y} \\ + (-l_{4y} * R_{4x} * S\theta_1 + (l_{4y} * R_{4y} + l_{4x} * R_{4x}) * C\theta_1) * S_{4z}$$

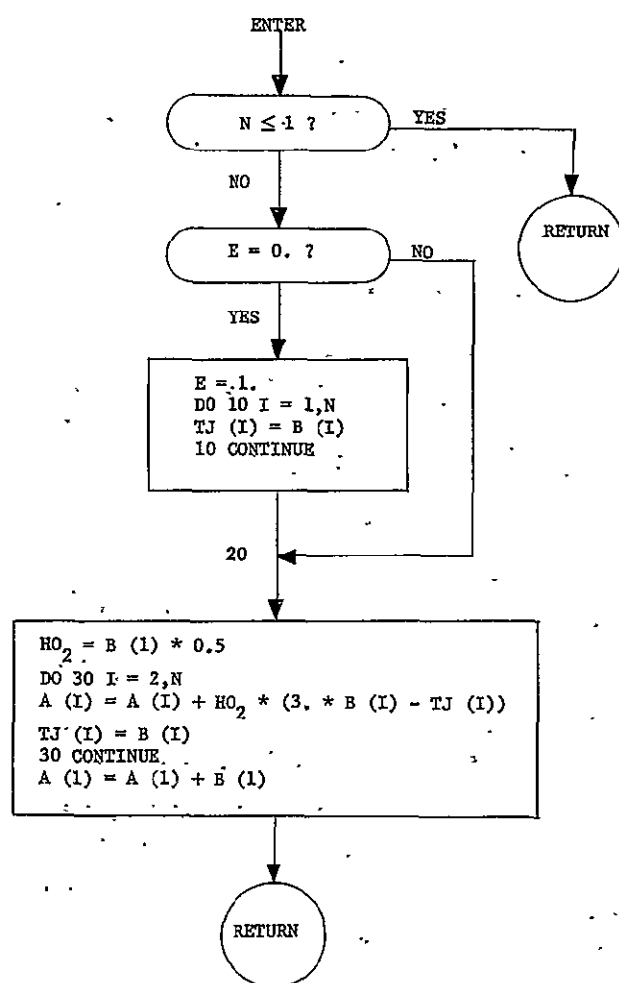
$$M_{6,4} = m_4 * l_{4x} * ((-R_{4y} + SR_1) * S_{4y} + (-R_{4z} + SR_2) * S_{4z})$$

$$M_{6,5} = (m_3 * m_4/m) * ((-l_{4x} * l_{3x} + l_{4x} * l_{3x}) * S_{3y} + l_{4x} * l_{3y} * S_{3z}) * S_{4y} \\ + (-l_{4y} * l_{3y} + l_{4x} * l_{3x}) * S_{3z} + l_{4y} * l_{3x} * S_{3y}) * S_{4z}$$

$$M_{6,6} = m_4 * (1. - m_4/m) * (((l_{4x}^2 + l_{4x}^2) * S_{4y} - l_{4x} * l_{4y} * S_{4z}) * S_{4y} \\ + ((l_{4y}^2 + l_{4x}^2) * S_{4z} - l_{4y} * l_{4x} * S_{4y}) * S_{4z})$$

$$[M] = [M] + [ERE]$$

RETURN



# FLOW CHART & BLOCK DIAGRAM

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Procedure

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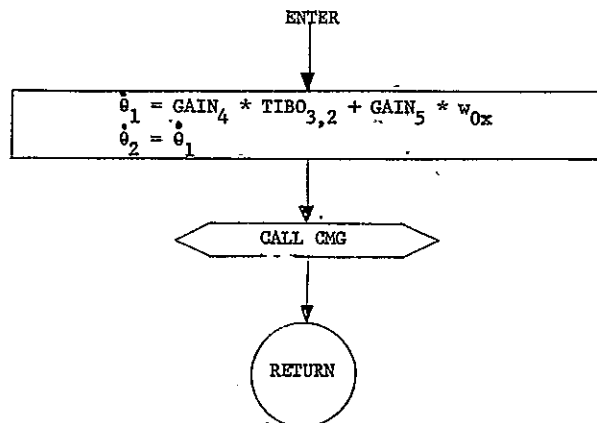
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DBx = - S0 * TIBO1,1 + C0 * TIBO2,1
DBy = - S0 * TIBO1,2 + C0 * TIBO2,2
DBz = - S0 * TIBO1,3 + C0 * TIBO2,3
REMP = DBx * Rox + DBy * Roy + DBz * Roz
F01 = C1 * m0 * (3. * REMP * DBz - Ro)
Ax = I0,1,1 * DBx + I0,1,2 * DBy + I0,1,3 * DBz
Ay = I0,2,1 * DBx + I0,2,2 * DBy + I0,2,3 * DBz
Az = I0,3,1 * DBx + I0,3,2 * DBy + I0,3,3 * DBz
TQOGx = 3. * C1 * (DBy * Az - DBz * Ay)
TQOGy = 3. * C1 * (DBz * Ax - DBx * Az)
TQOGz = 3. * C1 * (DBx * Ay - DBy * Ax)
DBx = - S0 * TIBO1,1 + C0 * TIBO2,1
DBy = C0 * (- S0 * TIBO1,2 + C0 * TIBO2,2)
      + S0 * (- S0 * TIBO1,3 + C0 * TIBO2,3)
DBz = - S0 * (- S0 * TIBO1,2 + C0 * TIBO2,2)
      + C0 * (- S0 * TIBO1,3 + C0 * TIBO2,3)
REMP = DBx * R1x + DBy * R1y + DBz * R1z
F11 = C1 * m1 * (3. * REMP * DBz - R1)
Ax = I1,1,1 * DBx + I1,1,2 * DBy + I1,1,3 * DBz
Ay = I1,2,1 * DBx + I1,2,2 * DBy + I1,2,3 * DBz
Az = I1,3,1 * DBx + I1,3,2 * DBy + I1,3,3 * DBz
TQ1Gx = 3. * C1 * (DBy * Az - DBz * Ay)
TQ1Gy = 3. * C1 * (DBz * Ax - DBx * Az)
TQ1Gz = 3. * C1 * (DBx * Ay - DBy * Ax)

```

RETURN





# FLOW CHART & BLOCK DIAGRAM

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 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

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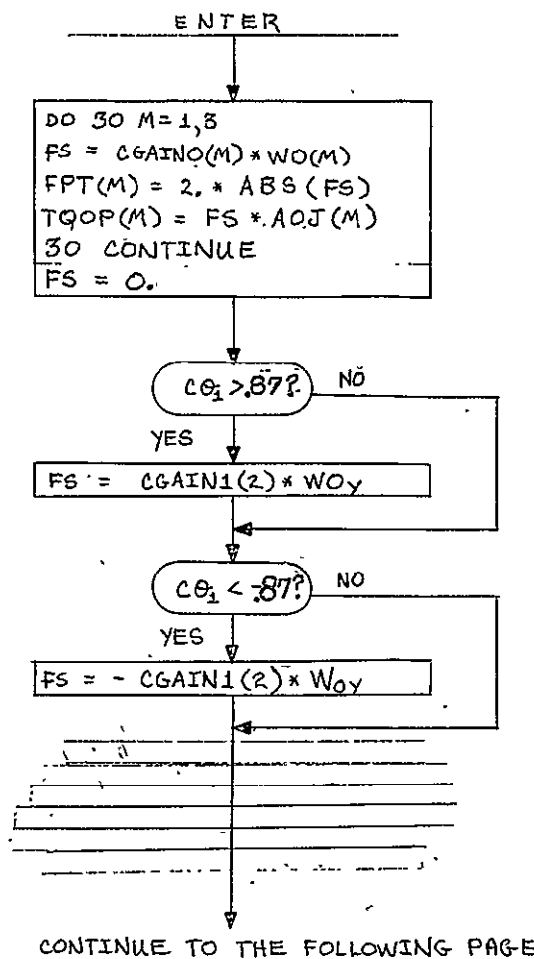
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Cx = A1,1 * Bx + A1,2 * By + A1,3 * Bz
Cy = A2,1 * Bx + A2,2 * By + A2,3 * Bz
Cz = A3,1 * Bx + A3,2 * By + A3,3 * Bz
F1,1 = D1,1 * E1,1 + D1,2 * E2,1 + D1,3 * E3,1
F1,2 = D1,1 * E1,2 + D1,2 * E2,2 + D1,3 * E3,2
F1,3 = D1,1 * E1,3 + D1,2 * E2,3 + D1,3 * E3,3
F2,1 = D2,1 * E1,1 + D2,2 * E2,1 + D2,3 * E3,1
F2,2 = D2,1 * E1,2 + D2,2 * E2,2 + D2,3 * E3,2
F2,3 = D2,1 * E1,3 + D2,2 * E2,3 + D2,3 * E3,3
F3,1 = D3,1 * E1,1 + D3,2 * E2,1 + D3,3 * E3,1
F3,2 = D3,1 * E1,2 + D3,2 * E2,2 + D3,3 * E3,2
F3,3 = D3,1 * E1,3 + D3,2 * E2,3 + D3,3 * E3,3
    
```

RETURN

# FLOW CHART & BLOCK DIAGRAM

Title: SUBROUTINE PCON Date: OCTOBER 1970 Page: 1 of 2  
 Procedure: \_\_\_\_\_ Drawn By: GARY JOHNSON



# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-6-6)

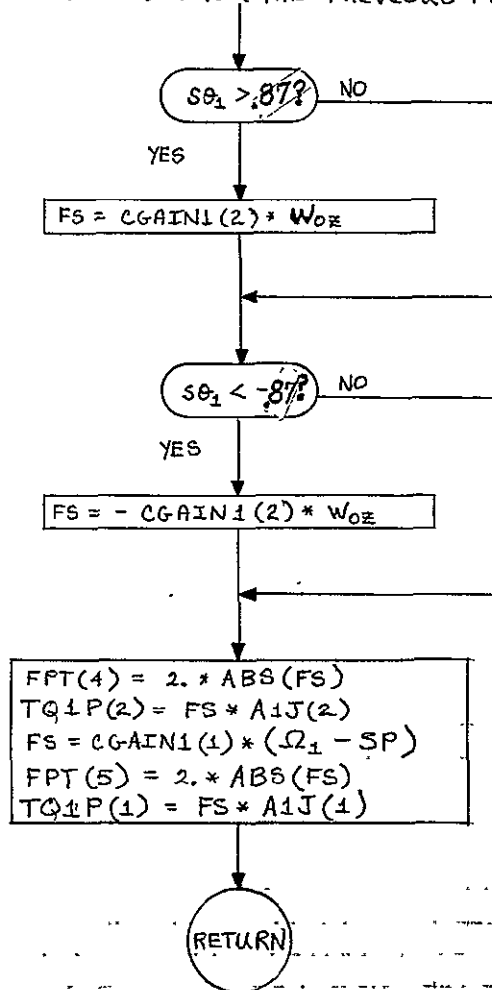
Application SUBROUTINE PCON CONTINUED

Date OCTOBER 1970 Page 2 of 2

Procedure

Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE



# FLOW CHART & BLOCK DIAGRAM

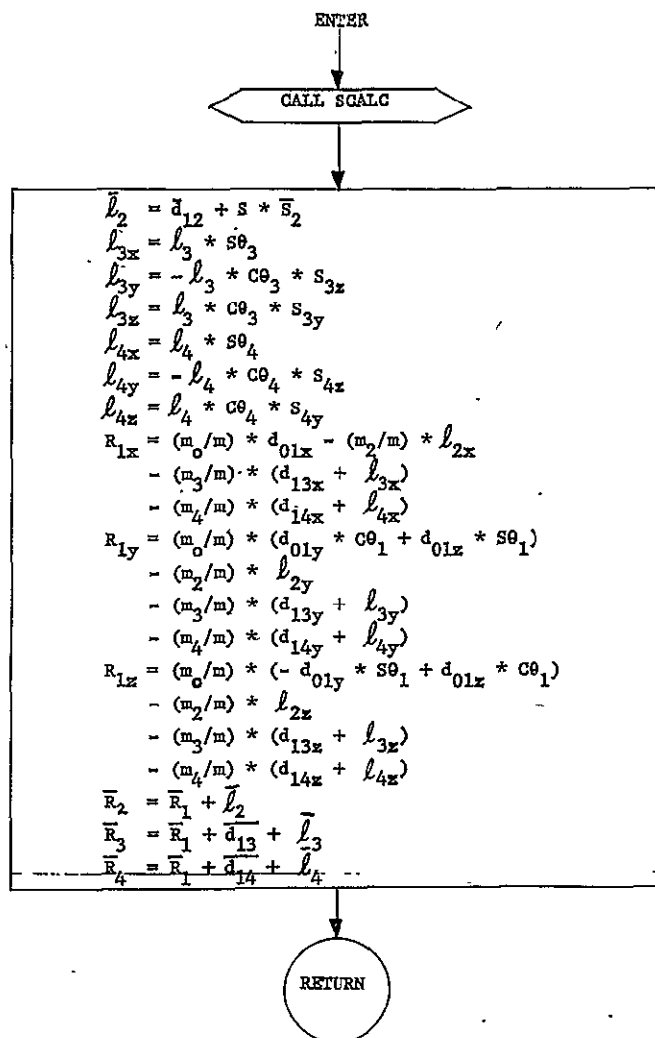
Application SUBROUTINE RECALC

Date OCTOBER 1970

Page 1 of 1

Procedure

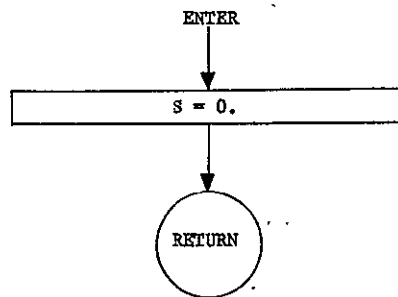
Drawn By GARY JOHNSON



# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

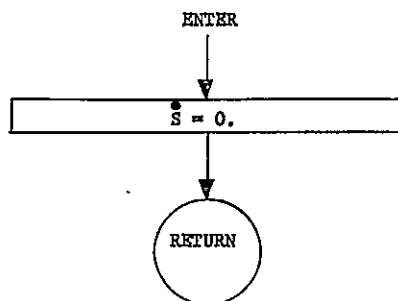
Application SUBROUTINE SCALC Date OCTOBER 1970 Page 1 of 1  
Procedure \_\_\_\_\_ Drawn By GARY JOHNSON



# FLOW CHART & BLOCK DIAGRAM

FORM NO. 11-2-31 2-64

Application SUBROUTINE SDCALC Date OCTOBER 1970 Page 1 of 1  
Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

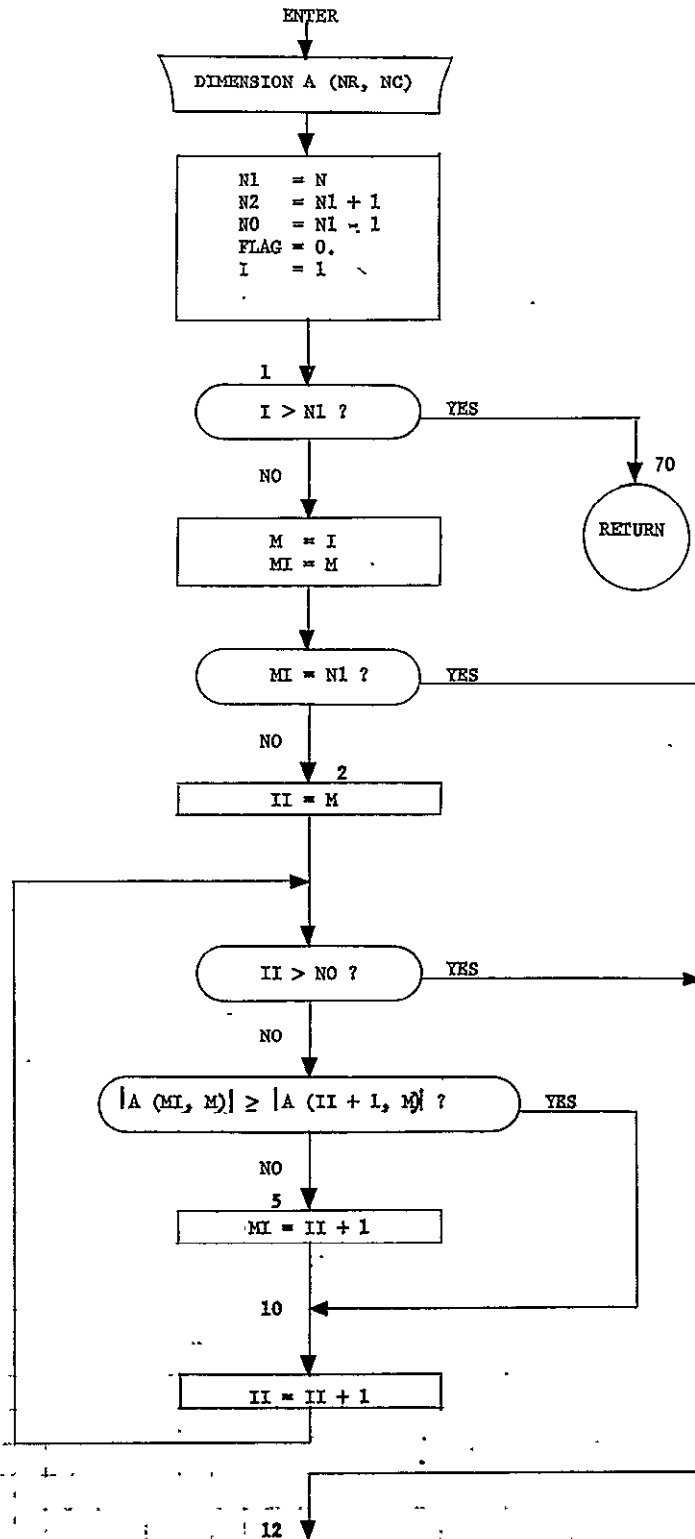


# FLOW CHART & BLOCK DIAGRAM

Form DEN 1103-01 (4-64)

Application SUBROUTINE SYEQNS Date OCTOBER 1970 Page 1 of 2  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

SUBROUTINE SYEQNS (A, N, NR, NC, FLAG)



CONTINUE TO THE NEXT PAGE



# FLOW CHART & BLOCK DIAGRAM

Application SUBROUTINE SYEQNS CONTINUED

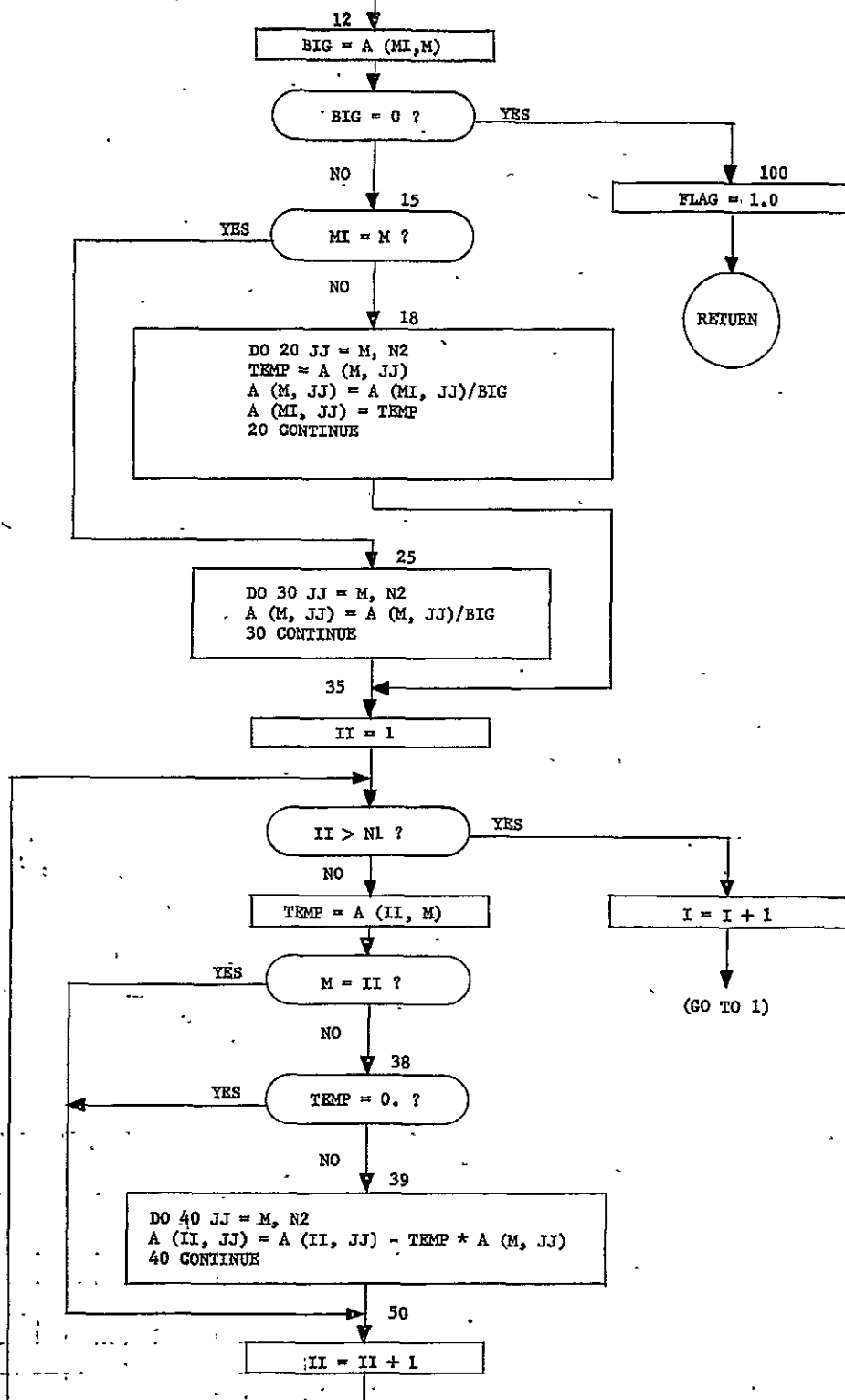
Date OCTOBER 1970

Page 2 of 2

Procedure

Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE



# FLOW CHART & BLOCK DIAGRAM

FORM 1103-01 (4-64)

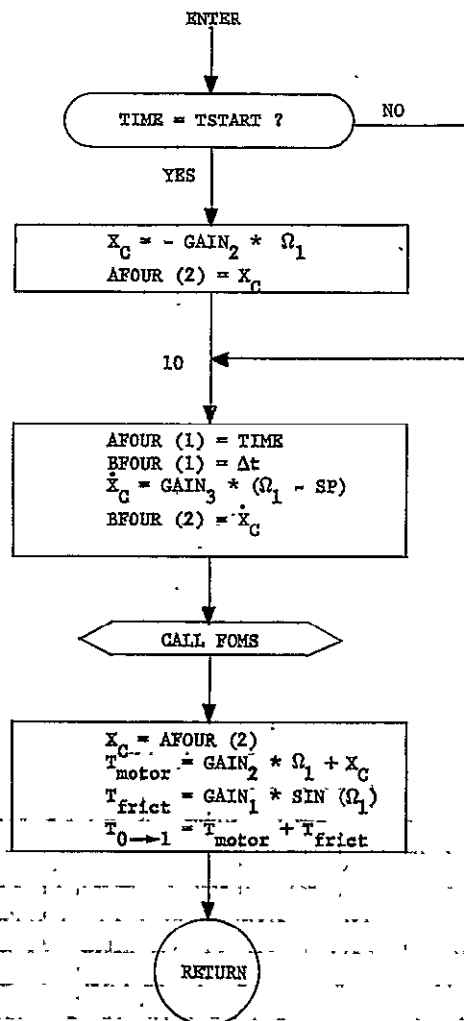
Application SUBROUTINE TORQ01

Date OCTOBER 1970

Page 1 of 1

Procedure \_\_\_\_\_

Drawn By GARY JOHNSON

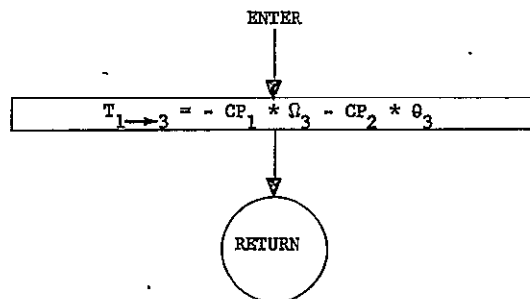


# FLOW CHART & BLOCK DIAGRAM

FORM 1103-01 (2-7-64)

Application SUBROUTINE TORK13 Date OCTOBER 1970 Page 1 of 1  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

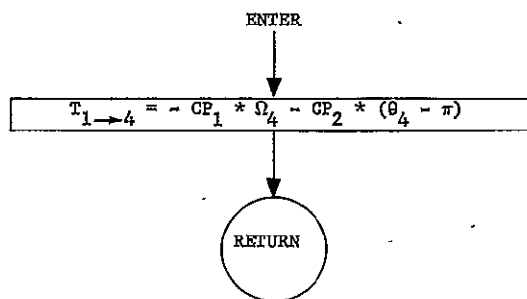
SUBROUTINE TORK13 (T13, CP1, CP2, THETA3, OMEGA3)



# FLOW CHART & BLOCK DIAGRAM

Application SUBROUTINE TORK14 Date OCTOBER 1970 Page 1 of 1  
 Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

SUBROUTINE TORK14 (T14, CP1, CP2, THETA4, OMEGA4)



# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 14-641

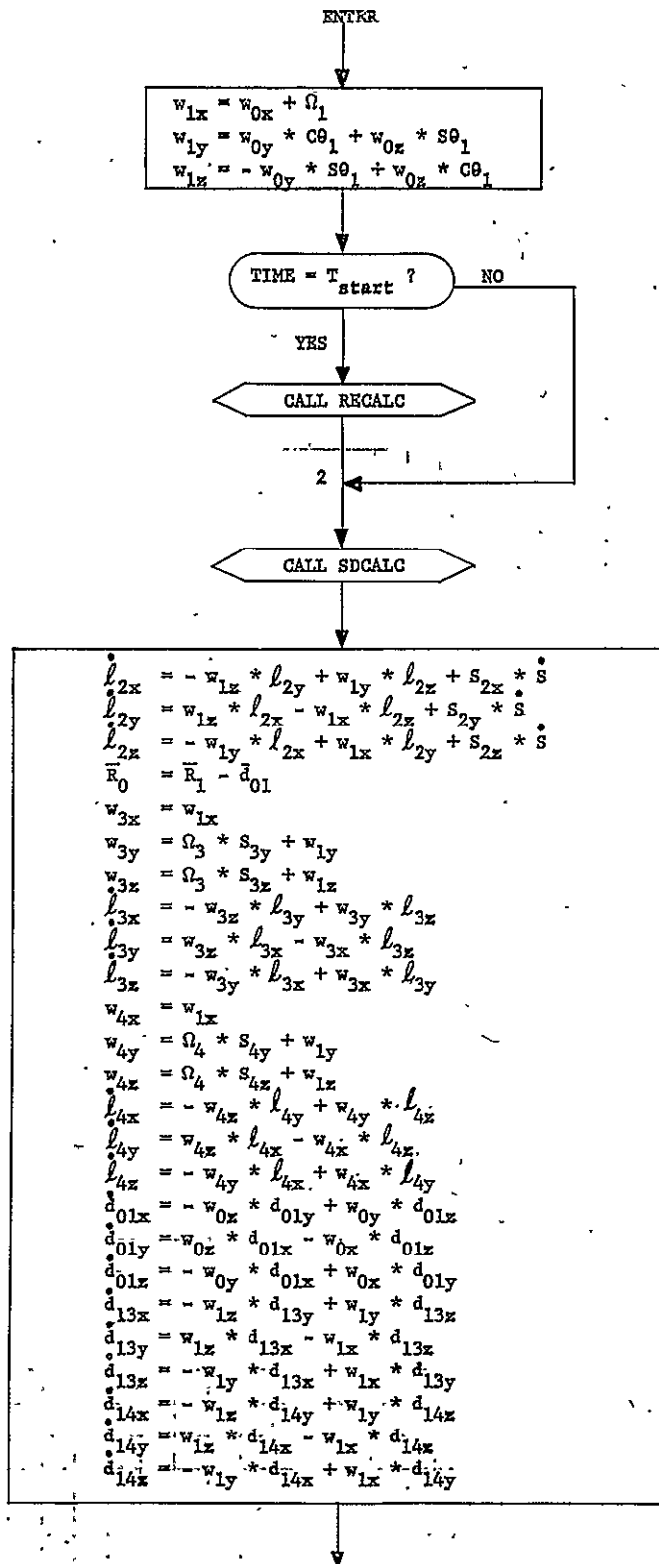
Application SUBROUTINE XDOT

Date OCTOBER 1970

Page 1 of 5

Procedure \_\_\_\_\_

Drawn By \_\_\_\_\_



CONTINUE TO THE NEXT PAGE

# FLOW CHART & BLOCK DIAGRAM

Application SUBROUTINE XDOT CONTINUED

Date OCTOBER 1970

Page 2 of 5

Procedure

Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

$$\begin{aligned}\dot{\bar{R}}_{1x} &= (m_0/m) * \dot{d}_{01x} - (m_2/m) * \dot{l}_{2x} \\ &\quad - (m_3/m) * (\dot{d}_{13x} + \dot{l}_{3x}) - (m_4/m) * (\dot{d}_{14x} + \dot{l}_{4x}) \\ \dot{\bar{R}}_{1y} &= (m_0/m) * (\dot{d}_{01y} * \cos \theta_1 + \dot{d}_{01z} * \sin \theta_1) - (m_2/m) * \dot{l}_{2y} \\ &\quad - (m_3/m) * (\dot{d}_{13y} + \dot{l}_{3y}) - (m_4/m) * (\dot{d}_{14y} + \dot{l}_{4y}) \\ \dot{\bar{R}}_{1z} &= (m_0/m) * (-\dot{d}_{01y} * \sin \theta_1 + \dot{d}_{01z} * \cos \theta_1) - (m_2/m) * \dot{l}_{2z} \\ &\quad - (m_3/m) * (\dot{d}_{13z} + \dot{l}_{3z}) - (m_4/m) * (\dot{d}_{14z} + \dot{l}_{4z}) \\ \dot{\bar{R}}_2 &= \dot{\bar{R}}_1 + \dot{l}_2 \\ \dot{\bar{R}}_3 &= \dot{\bar{R}}_1 + \dot{d}_{13} + \dot{l}_3 \\ \dot{\bar{R}}_4 &= \dot{\bar{R}}_1 + \dot{d}_{14} + \dot{l}_4\end{aligned}$$

CALL MULT

(I.E.  $\bar{H}_0 = [I_0] * \bar{w}_0$ )

CALL MULT

(I.E.  $\bar{H}_1 = [I_1] * \bar{w}_1$ )

$$\begin{aligned}h'_{3x} &= m_3 * (-l_{3x} * \dot{\bar{R}}_{3y} + l_{3y} * \dot{\bar{R}}_{3x}) \\ h'_{3y} &= m_3 * (l_{3x} * \dot{\bar{R}}_{3x} - l_{3y} * \dot{\bar{R}}_{3y}) \\ h'_{3z} &= m_3 * (-l_{3y} * \dot{\bar{R}}_{3x} + l_{3x} * \dot{\bar{R}}_{3y}) \\ h'_{4x} &= m_4 * (-l_{4x} * \dot{\bar{R}}_{4y} + l_{4y} * \dot{\bar{R}}_{4x}) \\ h'_{4y} &= m_4 * (l_{4x} * \dot{\bar{R}}_{4x} - l_{4y} * \dot{\bar{R}}_{4y}) \\ h'_{4z} &= m_4 * (-l_{4y} * \dot{\bar{R}}_{4x} + l_{4x} * \dot{\bar{R}}_{4y}) \\ h'_{1y} &= \dot{\bar{R}}_{1y} + h'_{3y} + h'_{4y} \\ &\quad - m_2 * (-l_{2y} * \dot{\bar{R}}_{2x} + l_{2x} * \dot{\bar{R}}_{2y}) \\ &\quad - m_3 * (-d_{13x} * \dot{\bar{R}}_{3x} + d_{13y} * \dot{\bar{R}}_{3y}) \\ &\quad - m_4 * (-d_{14x} * \dot{\bar{R}}_{4x} + d_{14y} * \dot{\bar{R}}_{4y}) \\ h'_{1x} &= \dot{\bar{R}}_{1x} + h'_{3x} + h'_{4x} \\ &\quad - m_2 * (l_{2y} * \dot{\bar{R}}_{2x} - l_{2x} * \dot{\bar{R}}_{2y}) \\ &\quad - m_3 * (d_{13y} * \dot{\bar{R}}_{3x} - d_{13x} * \dot{\bar{R}}_{3y}) \\ &\quad - m_4 * (d_{14y} * \dot{\bar{R}}_{4x} - d_{14x} * \dot{\bar{R}}_{4y})\end{aligned}$$

CONTINUE TO THE NEXT PAGE

# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (1-64)

Application SUBROUTINE XDOT CONTINUED

Date OCTOBER 1970

Page 3 of 5

Procedure

Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

TIME = T<sub>start</sub> ?

NO

YES

```

h'1x = h1x + h'3x + h'4x
      - m2 * (l2x * R2y - l2y * R2x)
      - m3 * (d13x * R3y - d13y * R3x)
      - m4 * (d14x * R4y - d14y * R4x)
SUM1 = m1 * R1x + m2 * R2x + m3 * R3x + m4 * R4x
SUM2 = m1 * R1y + m2 * R2y + m3 * R3y + m4 * R4y
SUM3 = m1 * R1z + m2 * R2z + m3 * R3z + m4 * R4z
DO 4 I = 1, 3
HCMGI = FFFI
DO 4 J = 1, 3
HCMGI = EEEI,J * wOJ + HCMGI
4 CONTINUE
Hx = H0x + h'1x + (- d01x * C01 + d01y * S01) * SUM2
      + (d01z * S01 + d01y * C01) * SUM3 + HCMGX
Hy = H0y + C01 * h'1y - S01 * h'1z + d01x * SUM1
      - d01x * S01 * SUM2 - d01x * C01 * SUM3 + HCMGY
Hz = H0z + S01 * h'1y + C01 * h'1z - d01y * SUM1
      + d01x * C01 * SUM2 - d01x * S01 * SUM3 + HCMGZ

```

5

```

AJ1x = m2 * l2x + m3 * d13x + m3 * l3x + m4 * d14x + m4 * l4x
AJ1y = m2 * l2y + m3 * d13y + m3 * l3y + m4 * d14y + m4 * l4y
AJ1z = m2 * l2z + m3 * d13z + m3 * l3z + m4 * d14z + m4 * l4z
00 = TIME * w0

```

IGRAVF = 0 ?

YES

NO

CALL GGRAD

10

CONTINUE TO THE FOLLOWING PAGE

# FLOW CHART & BLOCK DIAGRAM

Application SUBROUTINE XDOT CONTINUED

Date OCTOBER 1970

Page 4 of 5

Procedure Drawn By GARY JOHNSON

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$$\begin{aligned} \bar{F}_0 &= \bar{F}_{01} \\ \bar{F}_1 &= \bar{F}_{11} \\ \bar{T}_{OEF} &= \bar{T}_{OG} + \bar{T}_{OP} \\ \bar{T}_{IEF} &= \bar{T}_{IG} + \bar{T}_{IP} \\ \text{TERM1}(1) &= (m_o - m) * d_{01x} - AJ_{1x} \\ \text{TERM1}(2) &= (m_o - m) * d_{01y} - C\theta_1 * AJ_{1y} + S\theta_1 * AJ_{1z} \\ \text{TERM1}(3) &= (m_o - m) * d_{01z} - S\theta_1 * AJ_{1y} - C\theta_1 * AJ_{1z} \\ \text{TERM2}(1) &= m_o * d_{01x} - AJ_{1x} \\ \text{TERM2}(2) &= m_o * (C\theta_1 * d_{01y} + S\theta_1 * d_{01z}) - AJ_{1y} \\ \text{TERM2}(3) &= m_o * (-S\theta_1 * d_{01y} + C\theta_1 * d_{01z}) - AJ_{1z} \\ \text{ATCPT2}_{1,1} &= 0. \\ \text{ATCPT2}_{1,2} &= -\text{TERM2}(3) \\ \text{ATCPT2}_{1,3} &= \text{TERM2}(2) \\ \text{ATCPT2}_{2,1} &= C\theta_1 * \text{TERM2}(3) + S\theta_1 * \text{TERM2}(2) \\ \text{ATCPT2}_{2,2} &= -S\theta_1 * \text{TERM2}(1) \\ \text{ATCPT2}_{2,3} &= -C\theta_1 * \text{TERM2}(1) \\ \text{ATCPT2}_{3,1} &= S\theta_1 * \text{TERM2}(3) - C\theta_1 * \text{TERM2}(2) \\ \text{ATCPT2}_{3,2} &= C\theta_1 * \text{TERM2}(1) \\ \text{ATCPT2}_{3,3} &= -S\theta_1 * \text{TERM2}(1) \\ \dot{H}_x &= w_{0x} * H_y - w_{0y} * H_z + (-\text{TERM1}(3) * F_{0y} + \text{TERM1}(2) * F_{0x})/m \\ &\quad + (\text{ATCPT2}_{1,1} * F_{1x} + \text{ATCPT2}_{1,2} * F_{1y} + \text{ATCPT2}_{1,3} * F_{1z})/m \\ &\quad + T_{OEFx} + T_{IEFx} \\ \dot{H}_y &= -w_{0x} * H_x + w_{0x} * H_z + (\text{TERM1}(3) * F_{0x} - \text{TERM1}(1) * F_{0z})/m \\ &\quad + (\text{ATCPT2}_{2,1} * F_{1x} + \text{ATCPT2}_{2,2} * F_{1y} + \text{ATCPT2}_{2,3} * F_{1z})/m \\ &\quad + T_{OEFy} + C\theta_1 * T_{IEFy} - S\theta_1 * T_{IEFz} \\ \dot{H}_z &= w_{0y} * H_x - w_{0x} * H_y + (-\text{TERM1}(2) * F_{0x} + \text{TERM1}(1) * F_{0y})/m \\ &\quad + (\text{ATCPT2}_{3,1} * F_{1x} + \text{ATCPT2}_{3,2} * F_{1y} + \text{ATCPT2}_{3,3} * F_{1z})/m \\ &\quad + T_{OEFz} + S\theta_1 * T_{IEFy} + C\theta_1 * T_{IEFz} \end{aligned}$$

CALL TORKO1

$$\begin{aligned} \dot{h}_{1x} &= -w_{1y} * h'_{1x} + w_{1z} * h'_{1y} \\ &\quad + R_{1y} * (-m_2 * \dot{l}_{2x} - m_3 * (\dot{d}_{13x} + \dot{l}_{3x})) - m_4 * (\dot{d}_{14x} + \dot{l}_{4x}) \\ &\quad - R_{1z} * (-m_2 * \dot{l}_{2y} - m_3 * (\dot{d}_{13y} + \dot{l}_{3y})) - m_4 * (\dot{d}_{14y} + \dot{l}_{4y}) \\ &\quad - AJ_{1y} * (-F_{0y} * S\theta_1/m + F_{0x} * C\theta_1/m) \\ &\quad + AJ_{1z} * (F_{0y} * C\theta_1/m + F_{0x} * S\theta_1/m) \\ &\quad + AJ_{1x} * F_{1y}/m - AJ_{1y} * F_{1x}/m + T_{1EFx} + T_{0 \rightarrow 1} \end{aligned}$$

CONTINUE TO THE FOLLOWING PAGE



# FLOW CHART & BLOCK DIAGRAM

FORM DEN 1103-01 (4-64)

Application SUBROUTINE XDOT CONTINUED Date OCTOBER 1970 Page 5 of 5

Procedure \_\_\_\_\_ Drawn By GARY JOHNSON

CONTINUED FROM THE PREVIOUS PAGE

CALL TORK13

$$\begin{aligned} \dot{G}_3 = & -S_{3y} * (w_{1x} * h_{3x} - w_{1x} * h_{3z}) \\ & - S_{3x} * (w_{1x} * h_{3y} - w_{1y} * h_{3x}) \\ & + m_3 * S_{3y} * (l_{3x} * R_{3x} - l_{3x} * R_{3z}) \\ & + m_3 * S_{3x} * (l_{3x} * R_{3y} - l_{3y} * R_{3x}) \\ & - (m_3/m) * S_{3y} * (l_{3x} * (F_{0x} + F_{1x}) - l_{3x} * (-F_{0y} * S\theta_1 + F_{0z} * C\theta_1 + F_{1x})) \\ & - (m_3/m) * S_{3x} * (l_{3x} * (F_{0y} * C\theta_1 + F_{0z} * S\theta_1 + F_{1y}) \\ & - l_{3y} * (F_{0x} + F_{1x})) + T_1 \rightarrow 3 \end{aligned}$$

CALL TORK14

$$\begin{aligned} \dot{G}_4 = & -S_{4y} * (w_{1x} * h_{4x} - w_{1x} * h_{4z}) \\ & - S_{4x} * (w_{1x} * h_{4y} - w_{1y} * h_{4x}) \\ & + m_4 * S_{4y} * (l_{4x} * R_{4x} - l_{4x} * R_{4z}) \\ & + m_4 * S_{4x} * (l_{4x} * R_{4y} - l_{4y} * R_{4x}) \\ & - (m_4/m) * S_{4y} * (l_{4x} * (F_{0x} + F_{1x}) - l_{4x} * (-F_{0y} * S\theta_1 + F_{0z} * C\theta_1 + F_{1x})) \\ & - (m_4/m) * S_{4x} * (l_{4x} * (F_{0y} * C\theta_1 + F_{0z} * S\theta_1 + F_{1y}) \\ & - l_{4y} * (F_{0x} + F_{1x})) + T_1 \rightarrow 4 \end{aligned}$$

RETURN

# APPENDIX E, SUBROUTINE DESCRIPTIONS

Subroutine: CMG

Purpose: This subroutine computes the angular momenta produced by the CMGs located on body 0. Either 2 degree of freedom, 1 degree of freedom or reaction wheels can be accommodated.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	NUMCMG	$N_{CMG}$	The number of CMGs located on body 0
I	IDOF(K)	$I_{DOF}$	The number of degrees of freedom for the <u>kth</u> CMG
I	HW(K)	$\bar{H}$	The momentum of the <u>kth</u> wheel
I	AIJ(J,K,M)	$I_I$	The inertia matrix of the inner gimbal including wheel. The subscript J refers to the CMG being referenced, K, and M are dimensioned 3 and accommodate the inertia matrix
I	AJO(J,K,M)	$I_o$	The inertia matrix of the outer gimbal. The meaning of the subscripts are the same as AIJ(J,K,M)
I	THATA(J)	$\theta_j$	The inner gimbal angle
I	FEE(J)	$\phi_j$	The outer gimbal angle
I	THATA(J)	$\dot{\theta}_j$	The time-derivative of $\theta_j$
I	FEED(J)	$\dot{\phi}_j$	The time derivative of $\phi_j$
O	FFF(M)	$f$	The total angular momentum of the CMGs which is not a function of the angular rates
O	EEE(M,N)	$E$	The total angular momentum of the CMGs which is a function of the angular rates. For further discussion see the Appendix

Subroutines required: None

Discussion: None

# Subroutine ATT

Purpose: This routine simulates the action of an attitude control system using reaction jets.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	WO(3)	$\vec{\omega}_0$	Angular rates of Body 0 (stator)
I	TIBO(3,3)	$[I, B]_0$	Transformation from Body 0 to inertial frame
I	CA(3)	$\overline{CA}$	Direction cosines of reference direction
I	TIME	t	Time
I	BODY1I(1,1)	$I_{11}$	Moment of inertia around spin axis of rotor
I	OMEGA1	$\Omega_1$	Gimbal rate of rotor
I	DELTAT	$\Delta t$	Time increment per step
O	TQOP(3)		Control torques
O	FAT(8)		Control forces
I	AOJ(3)		Reaction jet lever arms

Subroutines required: none

Equations programmed:  $AK = \Omega_1 L_{11} \sin \beta / 2 / (5.5 + \Delta t)$   
coordinate transformations

Discussion: A complete description of this routine is given in the final report.

In order to activate the attitude control function it is necessary to set both IPROPF and IATTIF in the input data.

The attitude section also requires designation of the three direction cosines (CA(1), CA(2), CA(3)) of the direction in

inertial space at which control is desired. For a reorientation maneuver the initial orientation of the spin axis is inertial space read in (TIBOI(1,1), TIBOI(2,1), TIBOI(2,3) are the initial direction cosines of the spin axis in inertial space) can be specified different from GA. It is necessary, however, to ensure that the angle between the initial direction of the spin axis and the direction to which it is commanded to be redirected be not greater than  $60^{\circ}$  for the attitude control routine employed in this program.

The propulsion control section must be supplied with appropriate jet couple lengths and control gains for removal of transverse angular rates (see discussion on PCON subroutine). The control can be on either Body 0 or Body 1 or on both.

Subroutine: EMCALC

Purpose: Subroutine EMCALC assembles the M matrix used in the calculations from which the angular velocities are computed.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	THETA1	$\theta_1$	Angular displacement between bodies 0 and 1
I	R1(3)	$\vec{r}_1$	Vector distance from system c.m. to the c.m. of body 1
I	R2(3)	$\vec{r}_2$	Vector distance from system c.m. to the c.m. of body 2
I	R3(3)	$\vec{r}_3$	Vector distance from system c.m. to the c.m. of body 3
I	R4(3)	$\vec{r}_4$	Vector distance from system c.m. to the c.m. of body 4
I	EL2(3)	$\vec{l}_2$	Vector position of the movable mass
I	EL3(3)	$\vec{l}_3$	Vector position of body 3 from hinge line $s_3$
I	EL4(3)	$\vec{l}_4$	Vector position of body 4 from hinge line $s_4$
I	D01(3)	$\vec{d}_{01}$	Vector distance from the c.m. of body 0 to the hinge line of body 1
I	D13(3)	$\vec{d}_{13}$	Vector distance from the c.m. of body 1 to the hinge line of body 3
I	D14(3)	$\vec{d}_{14}$	Vector distance from the c.m. of body 1 to the hinge line of body 4
I	BOMASS	$m_0$	Mass of body 0

I	B2MASS	$m_2$	Mass of body 2
I	B3MASS	$m_3$	Mass of body 3
I	B4MASS	$m_4$	Mass of body 4
I	TOTMAS	$m_3$	Mass of composite body
I		$A_1$	Coordinate transformation from body 0 to body 1
I	R1(3)	$\vec{r}_1$	Vector distance from system c.m. to the c.m. of body 1
I	R2(3)	$\vec{r}_2$	Vector distance from the system c.m. to the c.m. of body 2
I	R3(3)	$\vec{r}_3$	Vector distance from the system c.m. to the c.m. of body 3
I	BODY0I(3,3)	$I_0$	The inertia matrix of body 0
I	BODY1I(3,3)	$I_1$	The inertia matrix of body 1
I	S3(3)	$\vec{s}_3$	The hinge line of body 3
I	S4(3)	$\vec{s}_4$	The hinge line of body 4
$\emptyset$	EM(6,6)	$m_{ij}$	The M matrix

Subroutines required: None

Equations programmed: The M matrix is related to the angular momenta and the angular velocities by the equation shown below:

$$\begin{bmatrix} H_x \\ H_y \\ H_z \\ h'_{1x} \\ h'_3 \cdot s_3 \\ h'_4 \cdot s_4 \end{bmatrix} = \begin{bmatrix} M_{11} & M_{12} & M_{13} & M_{14} & M_{15} & M_{16} \\ M_{21} & M_{22} & M_{23} & M_{24} & M_{25} & M_{26} \\ M_{31} & M_{32} & M_{33} & M_{34} & M_{35} & M_{36} \\ M_{41} & M_{42} & M_{43} & M_{44} & M_{45} & M_{46} \\ M_{51} & M_{52} & M_{53} & M_{54} & M_{55} & M_{56} \\ M_{61} & M_{62} & M_{63} & M_{64} & M_{65} & M_{66} \end{bmatrix} \begin{bmatrix} \omega_{0x} \\ \omega_{0y} \\ \omega_{0z} \\ \Omega_1 \\ \Omega_3 \\ \Omega_4 \end{bmatrix}$$



### Subroutine FOMS

**Purpose:** This integration routine calculates values of a set of variables at time  $t_{n+1}$  from their values at  $t_n$  and their derivatives at times  $t_n$  and  $t_{n-1}$ .

**Calling Sequence:** FOMS (A, B, N, E, TJ)

**Input/output:**

I/O	Fortran Name	Math Symbol	Definition
I	A(I)	$x_{i,n}$	$i$ th variable at time $t_n$ ; $i = 1, 2, \dots, n$ ; $I = i + 1$
O	A(I)	$x_{i,n+1}$	$i$ th variable at time $t_{n+1}$
I	B(I)	$\dot{x}_{i,n}$	$i$ th derivative at time $t_n$
I	N	m	Number of variables to be integrated; $m = N-1$
I,O	E		Flag to use current derivatives for past derivatives on first integration
I	TJ(I)	$\dot{x}_{i,n-1}$	$i$ th derivative at time $t_{n-1}$
O	TJ(I)	$\dot{x}_{i,n}$	$i$ th derivative at time $t_n$ , storage for next step

**Subroutines required:** none

**Equations programmed:**  $x_{n+1} = x_n + 1/2 \Delta t (3\dot{x}_n - \dot{x}_{n-1})$

**Discussion:** The variables and derivatives are indexed over values of  $I$  from 2 to  $N$ .  $B(1)$  is used to bring in  $\Delta t$ .  $A(1)$  is set up to be used for time but is not used in this program. On the first integration the current derivatives are also used as past derivatives since no past derivatives are available.

# Subroutine GGRAD

Purpose: This subroutine calculates the forces and torques due to gravity gradient on Body 0 and Body 1.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	THETO	$\theta_0$	True anomaly
I	TIBO(3,3)	$[I, B]_0$	Transformation from Body 0 to inertial frame
I	BODY0I(3,3)	$[I_0]$	Moment of inertia matrix of Body 0
I	BODY1I(3,3)	$[I_1]$	Moment of inertia matrix of Body 1
O	F01(3)	$\overline{F_{01}}$	Force on Body 0 due to gravity gradient
O	F11(3)	$\overline{F_{11}}$	Force on Body 1 due to gravity gradient
O	TQOG(3)		Torque on Body 0 due to gravity gradient
O	TQ1G(3)		Torque on Body 1 due to gravity gradient
I	C1		Gravitation constant and earth radius factor
I	BOMASS	$m_0$	Mass of Body 0
I	B1MASS	$m_1$	Mass of Body 1
I	THETA1	$\theta_1$	Gimbal angle of Body 1
I	RO(3)	$r_0$	Distance between centers of mass of Body 0 and system
I	R1(3)	$r_1$	Distance between centers of mass of Body 1 and system

Equations programmed:

$$\text{Torque: } T_G = - \frac{3\mu}{R_0} \bar{R}_0 \times [\bar{I} \cdot \bar{R}_0]$$

$$\text{Force: } F_G = \frac{\mu m}{R_0^3} \left( \bar{r} - \frac{3\bar{R}_0 \cdot \bar{r}}{R_0^2} \bar{R}_0 \right)$$

where  $R_0$  = distance to center of earth

$r$  = distance between center of mass of body and  
center of mass of system

Discussion: The translational motion is limited to circular orbits in the X-Y inertial plane in order to simplify transformations and relationships in this subroutine. Gravity gradient effects on Body 2, Body 3 and Body 4 are neglected.

Subroutine: HCON

Purpose: The subroutine contains the control laws in terms of gimbal angle rates for the CMGs. In most cases the user must furnish his own control law.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I			Any program variables to be used in the control law
O	FEED(J)	$\dot{\phi}_J$	Outer gimbal rate of the <u>J</u> th CMG
O	THATAD(J)	$\dot{\theta}_J$	Inner gimbal rate of the <u>J</u> th CMG

Subroutines required: CMG

Discussion: None

### Subroutine MULT

Purpose: Subroutine MULT multiplies either a 3 x 3 matrix by a 3 x 1 matrix or a 3 x 3 matrix by a 3 x 3 matrix.

Calling sequence: CALL MUTL (C, A, B, F, D, E, MTYPE)

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	A		A 3 x 3 matrix used in the matrix multiplication $C = A \times B$
I	B		A 3 x 1 matrix used in the matrix multiplication $C = A \times B$
Ø	C		A 3 x 1 matrix which is the result of $A \times B$
I	D		A 3 x 3 matrix used in the matrix multiplication $F = D \times E$
I	E		A 3 x 3 matrix used in the matrix multiplication $F = D \times E$
Ø	F		A 3 x 3 matrix which is the result of $D \times E$
I	MTYPE		A flag which determines the type of matrix multiplication being performed. If MTYPE = 1 then $C = A \times B$ is performed, if MTYPE $\neq$ 1 then $D = E \times F$ is performed.

Discussion: When subroutine MULT is used to multiply a 3 x 3 matrix by a 3 x 1 matrix variables F, D, E are dummies, when used to multiply two 3 x 3 matrices then variables C, A, B are dummies.

# Subroutine PCON

Purpose: To simulate a reaction jet control system for removing transverse components of angular velocity, maintaining the spin rate of the rotor and removing spin axis angular rates of the stator.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	WO	$\bar{\omega}_0$	Angular rates of Body 0
I	THETA1	$\theta_1$	Angle of Body 1 with respect to Body 0
I	OMEGA1	$\Omega_1$	Angular velocity of Body 1 with respect to Body 0
I	CGAINO(3)		Control gains of stator jets
I	AOJ(3)		Stator jet couple arm length
I	CGAIN1(2)		Control gains of rotor jets
I	ALJ(2)		Rotor jet couple arm length
O	TQOP(3)		Control torques on stator
O	TQ1P(3)		Control torques on rotor
O	FPT(5)		Control forces

Subroutines required: none

Equations programmed: none

Discussion: Certain restrictions on the configuration of the reaction jets have been assumed.

Associated with the torque around an axis there are four jets. One pair is in a pure couple to produce torque in one direction. The other pair, identical in location and strength, is oppositely directed. No torque is produced around axes other than the one designated.

In setting up input data for the reaction jet controls, the

control gain of the jets of the couple and the distance between the two jets forming the couple must be specified. Since the couples are similar for the two directions, this data is read only once for each axis.

The firing of jets on Body 1 (rotor) must be timed according to alignment with stator axes. Gimbal angle sensing is used in this routine to provide this timing.

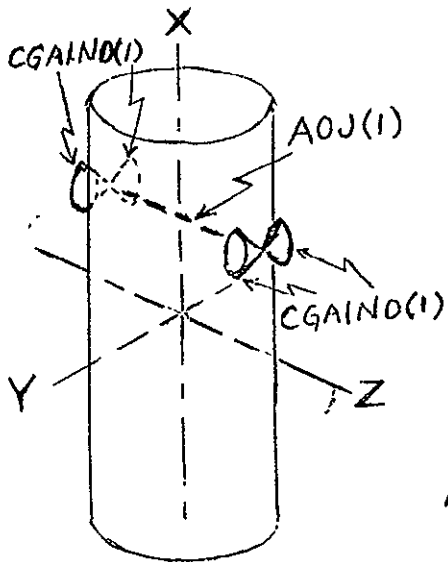
The PCON subroutine simulates a reaction jet control on angular rates. Transverse control torques are made proportional and opposite to transverse velocities. Such a control is similar in effect to an external frictional force acting against transverse motion. For a transverse torque  $T_T$  related to the magnitude of transverse rate  $\omega_T$  by  $T_T = -K \omega_T$  some estimate of the decrease in magnitude of transverse rate over a time interval  $t$  is given by  $\omega_T \approx \omega_{T0} e^{-K/I_T t}$  where  $\omega_{T0}$  is the initial transverse angular rate and  $I_T = \sqrt{(I_{022} + I_{122})(I_{033} + I_{133})}$ . This estimate will be good for jets on Body 0 where both transverse axes are controlled. For the single axis jets on the rotor the control will be much slower due to the time that the rotor spends in unfavorable positions.

In Figure      jet configurations are illustrated. Note that it is not necessary for jets to be symmetrically located with respect to any coordinate axes or planes. It is necessary, however, that the X-jet couple arm be parallel to the Y-Z plane, the Y-jet couple arm be parallel to the X-Z plane, etc. The data deck is simplified by requiring only magnitudes of jet couple arms without regard for actual directions or components.

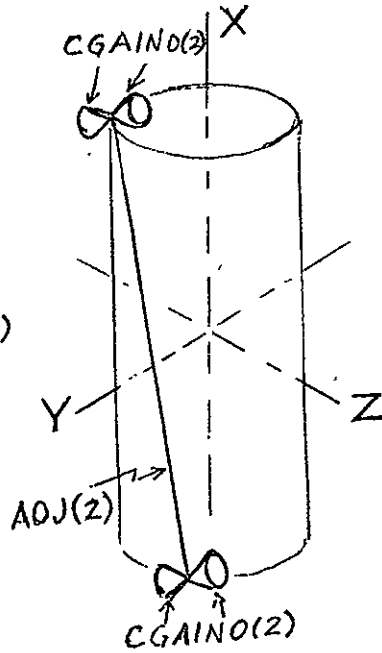
The reaction jets are activated by setting IPROPF = 1 and supplying control gain and couple arm length data. If it is desired to leave a certain axis uncontrolled, the corresponding control gain is set to zero, but the couple arm length should be given some non-zero value in order to prevent division by zero in calculation of impulse contributions.

Body 0

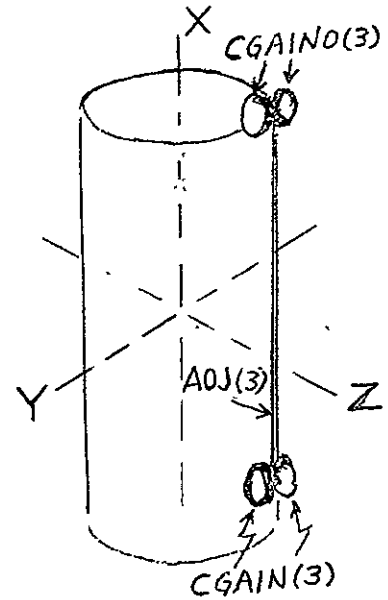
X-Axis Jets



Y-Axis Jets

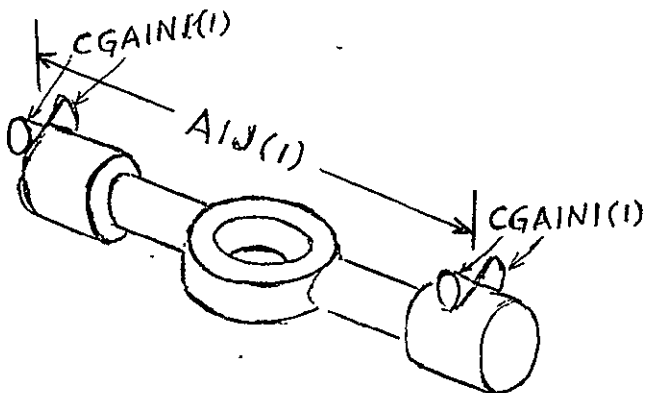


Z-Axis Jets

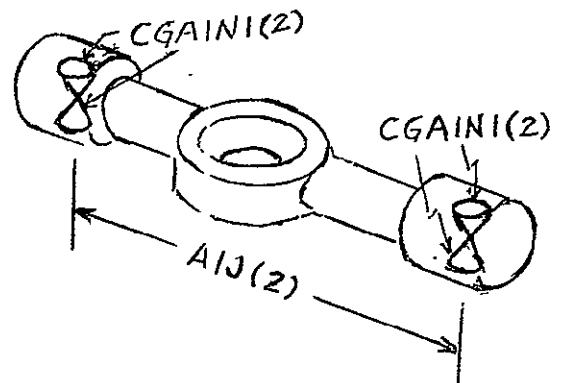


Body 1

X-Axis Jets



Y-Axis Jets





Subroutine: RECALC

Purpose: The purpose of this subroutine is to compute the distance from combined system center of mass to the center of mass of the various bodies.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	BOMASS	$m_0$	Mass of body 0
I	B2MASS	$m_2$	Mass of body 2
I	B3MASS	$m_3$	Mass of body 3
I	B4MASS	$m_4$	Mass of body 4
I	TOTMASS	$m$	Mass of composite body
I	D01(3)	$\vec{d}_{01}$	Vector distance from the c.m. of body 0 to the hinge line of body 1
I	EL2(3)	$\vec{\ell}_2$	Vector position of the movable mass
I	D13(3)	$\vec{d}_{13}$	Vector distance from the c.m. of body 1 to the hinge line of body 3
I	D14(3)	$\vec{d}_{14}$	Vector distance from the c.m. of body 1 to the hinge line of body 4
I	EL3(3)	$\vec{\ell}_3$	Vector position of body 3 from the hinge line $s_3$
I	EL4(3)	$\vec{\ell}_4$	Vector position of body 4 from the hinge line $s_4$
O	R1(3)	$\vec{r}_1$	Vector distance from system c.m. to the c.m. of body 1
O	R2(3)	$\vec{r}_2$	Vector distance from the system c.m. to the c.m. of body 2

0	R3(3)	$\bar{r}_3$	Vector distance from the system c.m. to the c.m. of body 3
0	R4(4)	$\bar{r}_4$	Vector distance from the system c.m. to the c.m. of body 4

Subroutines required: None

Equations programmed:

$$r_1 = \frac{m_0}{m} \bar{d}_{01} - \frac{m_2}{m} \bar{l}_2 - \frac{m_3}{m} (\bar{d}_{13} + \bar{l}_3) - \frac{m_4}{m} (\bar{d}_{14} + \bar{l}_4)$$

$$r_2 = \frac{m_0}{m} d_{01} + (1 - \frac{m_2}{m}) l_2 - \frac{m_3}{m} (d_{13} + l_3) - \frac{m_4}{m} (d_{14} + l_4)$$

$$r_3 = \frac{m_0}{m} d_{10} - \frac{m_2}{m} l_2 + (1 - \frac{m_3}{m}) (d_{13} + l_3) - \frac{m_4}{m} (d_{14} + l_4)$$

$$r_4 = \frac{m_0}{m} d_{01} - \frac{m_2}{m} l_2 - \frac{m_3}{m} (d_{13} + l_3) + (1 - \frac{m_4}{m}) (d_{14} + l_4)$$

$m_0, m_2, m_3, m_4, m,$

$d_{10}, d_{13}, d_{14}$

$l_2, l_3, l_4$

$r_1, r_2, r_3, r_4$

### Subroutine SCALC

Purpose: This routine supplies the position of the movable mass, Body 2.

#### Input/output:

I/O	Fortran Name	Math Symbol	Definition
0	S	S	Distance of Body 2 from D12 along direction S2

Note: Other I/O variables may be employed depending on the formulation of the subroutine.

Subroutines required: Not specified

Equations programmed: Not specified

Discussion: This subroutine will be constructed to suit the needs of the user. Any variables appearing in the common region can be employed as input/output variables.

### Subroutine SDCALC

Purpose: This routine supplies the speed of the movable mass, Body 2.

#### Input/output:

I/O	Fortran Name	Math Symbol	Definition
0	SDOT	$\dot{s}$	Magnitude of velocity of Body 2 along direction S2.

Note: Other I/O variables may be employed depending on the formulation of the subroutine.

Subroutines required: Not specified

Equations programmed: Not specified

Discussion: This subroutine will be constructed to suit the needs of the user. Any variables appearing in the common region can be employed as input/output variables.

Subroutine: SYEQNS (A,N,NR,NC,FLAG)

Purpose: Subroutine SYEQNS solves a set of linear simultaneous equations  $AX = c$  to determine the column vector  $x$ .

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I/O	A	A	A is the system matrix as depicted above. Also the answer $x$ will appear as the $N+1$ at column of matrix A
I	N	N	N is the number of linear equations to be solved
I	NR	NR	NR is the number of rows in A
I	NC	NC	NC is the number of columns in A
O	FLAG	FLAG	If FLAG = 0 as solution exists if FLAG = 1 no solution exists

Subroutines required: None

Discussion: None

Subroutine: TORK01

Purpose: The purpose of this subroutine is to compute the torque acting between bodies 0 and 1. The present version of TORK01 contains a frictional torque as well as torque motor with appropriate control law.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I			Any of the variables carried through common
O	T01	$T_{01}$	The torque acting between body 0 and body 1

Discussion: None ,

Subroutine: TORK13

Purpose: This subroutine computes the torque between body 1 and body 3.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	THETA3	$\theta_3$	Angular displacement of body 3 about the hinge line $s_3$
I	OMEGA3	$\omega_3$	Angular velocity of body 3 about the hinge line $s_3$
I	CP1	CP1	Gain for $\omega_3$
I	CP2	CP2	Gain for $\theta_3$
O	T13	$T_{13}$	The torque acting between bodies 1 and 3

Subroutines required: None

Equations programmed:

$$T_{1 \rightarrow 3} = -CP1 \times \omega_3 - CP2 \times \theta_3$$

Subroutine: TORK14

Purpose: This subroutine computes the torque acting between body 1 and body 4.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	THETA4	$\theta_4$	Angular displacement of body 4 about the hinge line $s_4$
I	OMEGA4	$\omega_4$	Angular velocity of body 4 about the hinge line $s_4$
I	CP1	$CP_1$	Gain for $\omega_4$
I	CP2	$CP_2$	Gain for $\theta_3$
O	T14	$T_{14}$	The torque acting between bodies 1 and 4

Subroutines required: None

Equation programmed:

$$T_{1 \rightarrow 4} = - CP1 \times \omega_4 - CP2 \times (\theta_4 - \pi)$$



#### Subroutine XDOT

Purpose: To compute the derivative of the unconstrained components of angular momenta as well as the variable required for these calculations.

# Segment 1

Purpose: To compute the angular velocity of body 1.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	OMEGA1	$\Omega_1$	Angular velocity between bodies 1 and 0
I	W0(3)	$\bar{\omega}_0$	Angular velocity of body 0
O	W1(3)	$\bar{\omega}_1$	Angular velocity of body 1
I	THETA1	$\theta_1$	Angular displacement between bodies 1 and 0

Subroutines required: None

Equations Programmed:

$$\begin{array}{lcl}
 \begin{array}{l} \Omega_1 \\ \bar{\omega}_0 \end{array} \rightarrow & \begin{array}{l} \omega_{1x} = \omega_{0x} \\ \omega_{1y} = \omega_{0y} \cos \theta_1 + \omega_{0z} \sin \theta_1 \\ \omega_{1z} = -\omega_{0y} \sin \theta_1 + \omega_{0z} \cos \theta_1 \end{array} & \begin{array}{l} + \Omega_1 \\ \\ \end{array} \\
 & & \rightarrow \bar{\omega}_1
 \end{array}$$

Discussion: The angular velocity of body 0 ( $\bar{\omega}_0$ ) is transformed to the body 1 coordinate system and is added to the primary gimbal rate to obtain the angular velocity of body 1 ( $\bar{\omega}_1$ ).

## Segment 2.

Purpose: To compute the vector position of the movable mass from the center-of-mass (c.m.) of body 1.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	S	s	Movable mass travel, a specified scalar function of time
I	D12(3)	$\vec{d}_{12}$	Fixed vector (in body 1 coordinates) locating the path of movable mass from c.m. of body 1
I	S2(3)	$\vec{s}_2$	Unit vector defining direction in which the movable mass travels
Ø	EL2(3)	$\vec{l}_2$	Position of movable mass (in body 1 coordinates) from c.m. of body 1

Subroutines required: None

Equations programmed:

$$\begin{array}{l}
 \vec{s} \rightarrow \\
 \vec{d}_{12} \\
 \vec{s}_2
 \end{array}
 \begin{array}{l}
 \vec{l}_{2x} = d_{12x} + s s_{2x} \\
 \vec{l}_{2y} = d_{12y} + s s_{2y} \\
 \vec{l}_{2z} = d_{12z} + s s_{2z}
 \end{array}
 \rightarrow \vec{l}_2$$

Discussion: The position of the movable mass is computed from the vector equation  $\vec{l}_2 = \vec{d}_{12} + \vec{s}_2 s$ .

### Segment 3

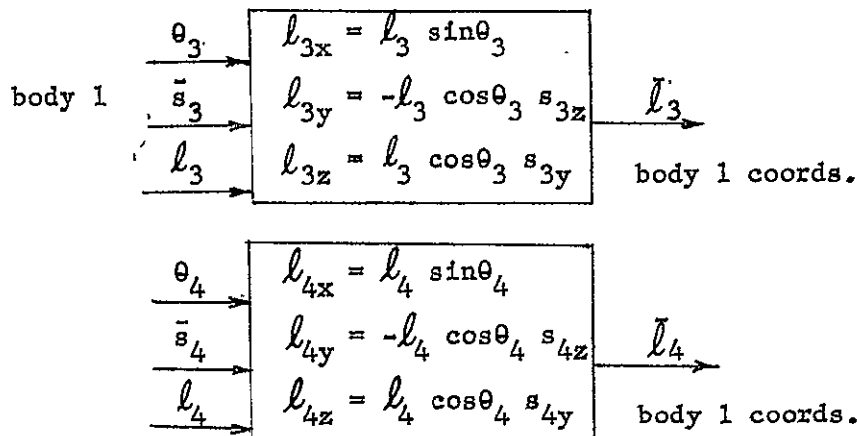
Purpose: To compute the positions of bodies 3 and 4.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	THETA3	$\theta_3$	Angular position of pendulum 3
I	S3(3)	$\bar{s}_3$	Hinge line of pendulum 3
I	PEND3L	$l_3$	Scalar length of pendulum 3
$\emptyset$	EL3(3)	$\bar{l}_3$	Vector position of pendulum 3 from hinge line $\bar{s}_3$
I	THETA4	$\theta_4$	Angular position of pendulum 4
I	S4(3)	$\bar{s}_4$	Hinge line of pendulum 4 in body 1 coordinated (no dimensions)
I	PEND4L	$l_4$	Scalar length of pendulum 4
$\emptyset$	EL4(3)	$\bar{l}_4$	Vector position of pendulum 4

Subroutines required: None

Equations programmed:



Discussion: None

#### Segment 4

Purpose: To compute the center of mass equations for bodies 0, 1, 2 and 3.  $\vec{r}_j$  is defined as the vector distance from the system center of mass to the center of mass of the jth body.

#### Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	EL2(3)	$\vec{l}_2$	Vector position of the movable mass
I	EL3(3)	$\vec{l}_3$	Vector position of body 3 from hinge line $s_3$
I	EL4(3)	$\vec{l}_4$	Vector position of body 4 from hinge line $s_4$
I	D01(3)	$\vec{d}_{01}$	Vector distance from the c.m. of body 0 to the hinge line of body 1
I	D13(3)	$\vec{d}_{13}$	Vector distance from the c.m. of body 1 to the hinge line of body 3
I	D14(3)	$\vec{d}_{14}$	Vector distance from the c.m. of body 1 to the hinge line of body 4
I	B0MASS	$m_0$	Mass of body 0 (slugs)
I	B2MASS	$m_2$	Mass of body 2
I	B3MASS	$m_3$	Mass of body 3
I	B4MASS	$m_4$	Mass of body 4
I	TOTMAS	$m$	Mass of composite body
I		$A_1$	Coordinate transformation from body 0 to body 1

$\emptyset$	R1(3)	$\vec{r}_1$	Vector distance from system c.m. to the c.m. of body 1
$\emptyset$	R2(3)	$\vec{r}_2$	Vector distance from the system c.m. to the c.m. of body 2
$\emptyset$	R3(3)	$\vec{r}_3$	Vector distance from the system c.m. to the c.m. of body 3
$\emptyset$	R4(3)	$\vec{r}_4$	Vector distance from the system c.m. to the c.m. of body 4

Subroutines required: None

Equations programmed:

$$\begin{bmatrix} r_{1x} \\ r_{1y} \\ r_{1z} \end{bmatrix} = \frac{m_0}{m} A_1 \begin{bmatrix} d_{01x} \\ d_{01y} \\ d_{01z} \end{bmatrix} - \frac{m_2}{m} \begin{bmatrix} l_{2x} \\ l_{2y} \\ l_{2z} \end{bmatrix} - \frac{m_3}{m} \begin{bmatrix} d_{13x} + l_{3x} \\ d_{13y} + l_{3y} \\ d_{13z} + l_{3z} \end{bmatrix} - \frac{m_4}{m} \begin{bmatrix} d_{14x} + l_{4x} \\ d_{14y} + l_{4y} \\ d_{14z} + l_{4z} \end{bmatrix}$$

$$\begin{bmatrix} r_{2x} \\ r_{2y} \\ r_{2z} \end{bmatrix} = \begin{bmatrix} r_{1x} \\ r_{1y} \\ r_{1z} \end{bmatrix} + \begin{bmatrix} l_{2x} \\ l_{2y} \\ l_{2z} \end{bmatrix}$$

$$\begin{bmatrix} r_{3x} \\ r_{3y} \\ r_{3z} \end{bmatrix} = \begin{bmatrix} r_{1x} \\ r_{1y} \\ r_{1z} \end{bmatrix} + \begin{bmatrix} d_{13x} \\ d_{13y} \\ d_{13z} \end{bmatrix} + \begin{bmatrix} l_{3x} \\ l_{3y} \\ l_{3z} \end{bmatrix}$$

$$\begin{bmatrix} r_{4x} \\ r_{4y} \\ r_{4z} \end{bmatrix} = \begin{bmatrix} r_{1x} \\ r_{1y} \\ r_{1z} \end{bmatrix} + \begin{bmatrix} d_{14x} \\ d_{14y} \\ d_{14z} \end{bmatrix} + \begin{bmatrix} l_{4x} \\ l_{4y} \\ l_{4z} \end{bmatrix}$$

$l_2, l_3, l_4$

$\bar{d}_{01}, \bar{d}_{13}, \bar{d}_{14}$

$A_1$

$\bar{r}_1, \bar{r}_2, \bar{r}_3, \bar{r}_4$

(body 1 coords.)

Discussion: None

# Segment 5

Purpose: To compute the derivative of  $\vec{l}_2$ , the rate at which to movable mass in moving.

Input/output:

I/O	Fortran Statement	Math Symbol	Definition
I	W1(3)	$\omega_1$	Angular velocity of body 1
I	EL2(3)	$\vec{l}_2$	Vector position of the movable mass
I	s2(3)	$\vec{s}_2$	Unit vector defining the direction of travel of the movable mass (body 2)
I	S	s	Movable mass travel, a specified scalar function of time
I	SDOT	$\dot{s}$	The time derivative of s.
Ø	EL2DOT(3)	$\dot{\vec{l}}_2$	The time derivative of $\vec{l}_2$

Subroutines required: SDCALC

Equations programmed:

$$\begin{array}{c}
 \vec{\omega}_1 \\
 \vec{l}_2 \\
 \vec{s}_2, \dot{s}
 \end{array}
 \rightarrow
 \left[ \begin{array}{c}
 l_{2x} \\
 \dot{l}_{2y} \\
 l_{2z}
 \end{array} \right]
 =
 \text{CPM } \vec{\omega}_1
 \left[ \begin{array}{c}
 l_{2x} \\
 l_{2y} \\
 l_{2z}
 \end{array} \right]
 +
 \left[ \begin{array}{c}
 s_{2x} \dot{s} \\
 s_{2y} \dot{s} \\
 s_{2z} \dot{s}
 \end{array} \right]
 \rightarrow
 \dot{\vec{l}}_2$$



where

$$CPM\tilde{\omega}_1 = \begin{bmatrix} 0 & -W1(3) & W1(2) \\ W1(3) & 0 & -W1(1) \\ -W1(2) & W1(1) & 0 \end{bmatrix}$$

Discussion: None

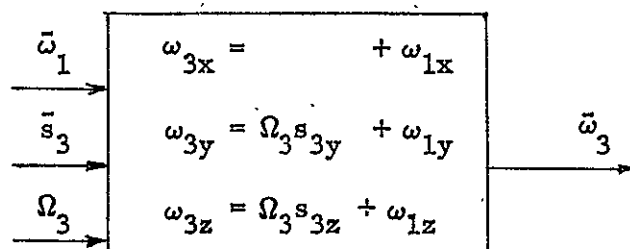
Segment 6

Purpose: To compute the angular velocity of body 3 ( $\bar{\omega}_3$ ).

I/O	Fortran Name	Math Symbol	Definition
I	W1(3)	$\bar{\omega}_1$	Angular velocity of body 1
I	OMEGA3	$\Omega_3$	Angular velocity of body 3 about the hinge line $s_3$
I	s3(3)	$\bar{s}_3$	The hinge line about which body 3 rotates
Ø	W3(3)	$\bar{\omega}_3$	The angular velocity of body 3

Subroutines required: None

Equations programmed:



Discussion: None

Segment 7

Purpose: To compute the derivative of  $\vec{l}_3$ .

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	EL3(3)	$\vec{l}_3$	Vector position of body 3 from hinge line $\vec{s}_3$
I	W3(3)	$\vec{\omega}_3$	Angular velocity of body 3
O	EL3DOT(3)	$\dot{\vec{l}}_3$	Time derivative of $\vec{l}_3$

Subroutines required: None

Equations programmed:

$$\begin{array}{c} \vec{l}_3 \\ \vec{\omega}_3 \end{array} \rightarrow \begin{bmatrix} \dot{l}_{3x} \\ \dot{l}_{3y} \\ \dot{l}_{3z} \end{bmatrix} = \text{CPM} \vec{\omega}_3 \begin{bmatrix} l_{3x} \\ l_{3y} \\ l_{3z} \end{bmatrix} \rightarrow \dot{\vec{l}}_3$$

Discussion: None

Segment 8

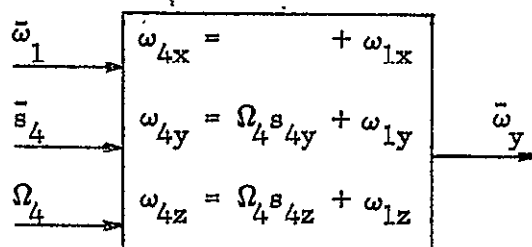
Purpose: To compute the angular velocity of body 4  $\vec{\omega}_4$ .

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	W1(3)	$\vec{\omega}_1$	Angular velocity of body 1
I	OMEGA4	$\Omega_4$	Angular velocity of body 4 about the hinge line $\vec{s}_4$
I	S4(3)	$\vec{s}_4$	The hinge line about which body 4 rotates
Ø	W4(3)	$\vec{\omega}_4$	Angular velocity of body 4

Subroutines required: None

Equations programmed:



Discussion: None

Segment 9

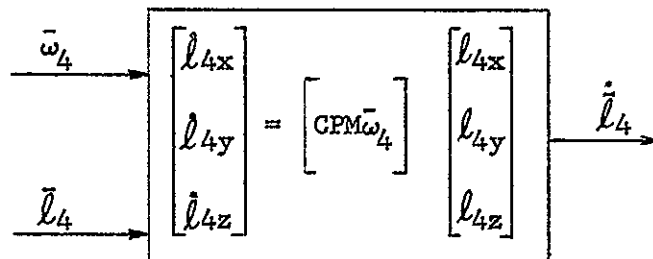
Purpose: To compute the derivative of  $\bar{l}_4$ .

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	EL4(3)	$\bar{l}_4$	Vector position of body 4 from the hinge line $\bar{s}_4$
I	W4(3)	$\bar{\omega}_4$	Angular velocity of body 4
O	EL4DOT(3)	$\dot{\bar{l}}_4$	Time derivative of $\bar{l}_4$

Subroutines required: None

Equations programmed:



Discussion: None

Segment 10

Purpose: To compute the time derivatives of  $\bar{d}_{01}$ ,  $\bar{d}_{13}$ , and  $\bar{d}_{14}$ .

Input/output:

I/O	Fortran Statement	Math Symbol	Definition
I	D01(3)	$\bar{d}_{01}$	Vector distance from the c.m. of body 0 to the hinge line of body 1
I	D13(3)	$\bar{d}_{13}$	Vector distance from the c.m. of body 1 to the hinge line of body 3
I	D14(3)	$\bar{d}_{14}$	Vector distance from the c.m. of body 1 to the hinge line of body 4
I	W1(3)	$\bar{\omega}_1$	Angular velocity of body 1
Ø	D01DOT(3)	$\dot{\bar{d}}_{01}$	Time derivative of $\bar{d}_{01}$
Ø	D13DOT(3)	$\dot{\bar{d}}_{13}$	Time derivative of $\bar{d}_{13}$
Ø	D14DOT(3)	$\dot{\bar{d}}_{14}$	Time derivative of $\bar{d}_{14}$

Subroutines required: None

Equations programmed:

$$\begin{array}{c} \bar{\omega}_0 \\ \bar{d}_{10} \end{array} \rightarrow \left[ \begin{array}{c} \dot{\bar{d}}_{01x} \\ \dot{\bar{d}}_{01y} \\ \dot{\bar{d}}_{01z} \end{array} \right] = \left[ \text{GPM} \bar{\omega}_0 \right] \left[ \begin{array}{c} \bar{d}_{10x} \\ \bar{d}_{10y} \\ \bar{d}_{10z} \end{array} \right] \rightarrow \dot{\bar{d}}_{01} = \bar{\omega}_0 \times \bar{d}_{01}$$

$$\begin{array}{c} \vec{\omega}_1 \\ \vec{d}_{13} \end{array} \rightarrow \left[ \begin{array}{c} \dot{d}_{13x} \\ \dot{d}_{13y} \\ \dot{d}_{13z} \end{array} \right] = \left[ \text{CFM} \vec{\omega}_1 \right] \left[ \begin{array}{c} d_{13x} \\ d_{13y} \\ d_{13z} \end{array} \right] \rightarrow \dot{\vec{d}}_{13} = \vec{\omega}_1 \times \vec{d}_{13}$$

$$\begin{array}{c} \vec{\omega}_1 \\ \vec{d}_{14} \end{array} \rightarrow \left[ \begin{array}{c} \dot{d}_{14x} \\ \dot{d}_{14y} \\ \dot{d}_{14z} \end{array} \right] = \left[ \text{CFM} \vec{\omega}_1 \right] \left[ \begin{array}{c} d_{14x} \\ d_{14y} \\ d_{14z} \end{array} \right] \rightarrow \dot{\vec{d}}_{14} = \vec{\omega}_1 \times \vec{d}_{14}$$

Discussion: None

Segment 11

Purpose: To compute the time derivatives to the center of mass variables  $\bar{r}_1$ ,  $\bar{r}_2$ ,  $\bar{r}_3$  and  $\bar{r}_4$ .

Input/output:

I/O	Fortran Statement	Math Symbol	Definition
I	D01DOT(3)	$\dot{\bar{d}}_{01}$	Time derivatives of $\bar{d}_{01}$
I	EL2DOT(3)	$\dot{\bar{l}}_2$	Time derivative of $\bar{l}_2$
I	D13DOT(3)	$\dot{\bar{d}}_{13}$	Time derivative of $\bar{d}_{13}$
I	EL3DOT(3)	$\dot{\bar{l}}_3$	Time derivative of $\bar{l}_3$
I	D14DOT(3)	$\dot{\bar{d}}_{14}$	Time derivative of $\bar{d}_{14}$
I	EL4DOT(3)	$\dot{\bar{l}}_4$	Time derivative of $\bar{l}_4$
I	R1DOT(3)	$\dot{\bar{r}}_1$	Time derivative of $\bar{r}_1$
I	BOMASS	$m_0$	Mass of body 0
I	B2MASS	$m_2$	Mass of body 2
I	B3MASS	$m_3$	Mass of body 3
I	B4MASS	$m_4$	Mass of body 4
I	TOTMAS	$m$	Mass of composite body (total mass)
I		$A_1$	Coordinate transformation from body 0 to body 1
Ø	R1DOT(3)	$\dot{\bar{r}}_1$	Time derivative of $\bar{r}_1$
Ø	R2DOT(3)	$\dot{\bar{r}}_2$	Time derivative of $\bar{r}_2$
Ø	R3DOT(3)	$\dot{\bar{r}}_3$	Time derivative of $\bar{r}_3$
Ø	R4DOT(3)	$\dot{\bar{r}}_4$	Time derivative of $\bar{r}_4$



Subroutines required: None

Equations programmed:

$$\begin{bmatrix} \dot{r}_{1x} \\ \dot{r}_{1y} \\ \dot{r}_{1z} \end{bmatrix} = \frac{m_0}{m} [A_1] \begin{bmatrix} \dot{d}_{01x} \\ \dot{d}_{01y} \\ \dot{d}_{01z} \end{bmatrix} - \frac{m_2}{m} \begin{bmatrix} \dot{l}_{2x} \\ \dot{l}_{2y} \\ \dot{l}_{2z} \end{bmatrix} - \frac{m_3}{m} \begin{bmatrix} \dot{d}_{13x} + \dot{l}_{3x} \\ \dot{d}_{13y} + \dot{l}_{3y} \\ \dot{d}_{13z} + \dot{l}_{3z} \end{bmatrix} - \frac{m_4}{m} \begin{bmatrix} \dot{d}_{14x} + \dot{l}_{4x} \\ \dot{d}_{14y} + \dot{l}_{4y} \\ \dot{d}_{14z} + \dot{l}_{4z} \end{bmatrix}$$

$$\begin{bmatrix} \dot{r}_{2x} \\ \dot{r}_{2y} \\ \dot{r}_{2z} \end{bmatrix} = \begin{bmatrix} \dot{r}_{1x} \\ \dot{r}_{1y} \\ \dot{r}_{1z} \end{bmatrix} + \begin{bmatrix} \dot{l}_{2x} \\ \dot{l}_{2y} \\ \dot{l}_{2z} \end{bmatrix}$$

$$\begin{bmatrix} \dot{r}_{3x} \\ \dot{r}_{3y} \\ \dot{r}_{3z} \end{bmatrix} = \begin{bmatrix} \dot{r}_{1x} \\ \dot{r}_{1y} \\ \dot{r}_{1z} \end{bmatrix} + \begin{bmatrix} \dot{d}_{13x} + \dot{l}_{3x} \\ \dot{d}_{13y} + \dot{l}_{3y} \\ \dot{d}_{13z} + \dot{l}_{3z} \end{bmatrix}$$

$$\begin{bmatrix} \dot{r}_{4x} \\ \dot{r}_{4y} \\ \dot{r}_{4z} \end{bmatrix} = \begin{bmatrix} \dot{r}_{1x} \\ \dot{r}_{1y} \\ \dot{r}_{1z} \end{bmatrix} + \begin{bmatrix} \dot{d}_{14x} + \dot{l}_{4x} \\ \dot{d}_{14y} + \dot{l}_{4y} \\ \dot{d}_{14z} + \dot{l}_{4z} \end{bmatrix}$$

$\dot{d}_{01}$  (body 0 coordinates)

$\dot{d}_{10}, \dot{d}_{13}, \dot{d}_{14}, \dot{l}_2, \dot{l}_3, \dot{l}_4$ , (body 1 coordinates)

$A_1$

$\dot{r}_1, \dot{r}_2, \dot{r}_3, \dot{r}_4$

(body 1 coords.)

Discussion: None

Segment 12

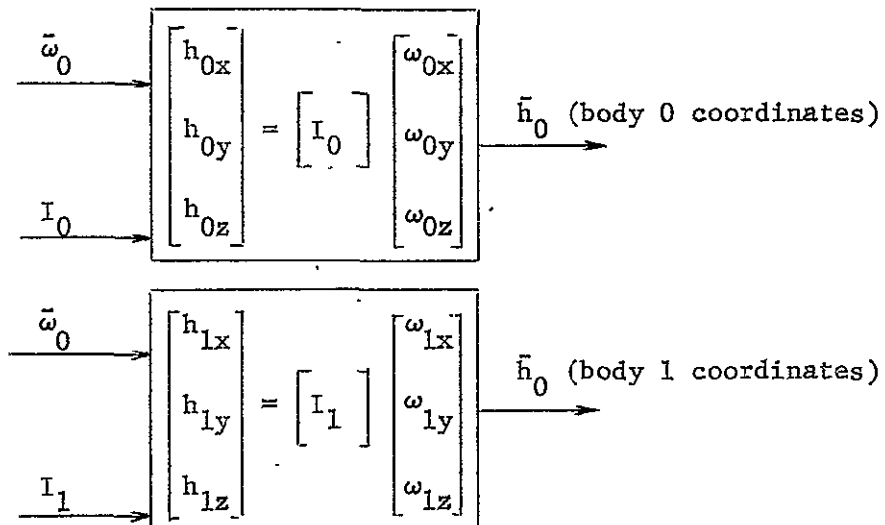
Purpose: To compute the angular momentum of body 0 and body 1.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	W0	$\bar{\omega}_0$	Angular velocity of body 0
I	W1	$\bar{\omega}_1$	Angular velocity of body 1
I	BODY0I	$I_0$	The inertia of body 0
I	BODY1I	$I_1$	The inertia of body 1
O	H0	$\bar{h}_0$	The angular momentum of body 0
O	H1	$\bar{h}_1$	The angular momentum of body 1

Subroutines required: MULT

Equations programmed:



Discussion: None

Segment 13

Purpose: To compute the primed angular momentum of bodies 1, 3 and 4.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	B3MASS	$m_3$	The mass of body 3
I	EL3(3)	$\bar{\ell}_3$	Vector position of body 3 from the hinge line $\bar{s}_3$
I	R3DOT(3)	$\dot{\bar{r}}_3$	The time derivative of $\bar{r}_3$
O	H3PRIM(3)	$\bar{h}_3'$	The primed angular momentum of body 3
I	B4MASS	$m_4$	The mass of body 4
I	EL4(3)	$\bar{\ell}_4$	Vector position of body 4 from the hinge line $\bar{s}_4$
I	R4DOT(3)	$\dot{\bar{r}}_4$	The time derivative of $\bar{r}_4$
O	H4PRIM(3)	$\bar{h}_4'$	The primed angular momentum of body 4
I	H1(3)	$\bar{h}_1$	The angular momentum of body 1
I	H3PRIM(3)	$\bar{h}_3'$	The primed angular momentum of body 3
I	H4PRIM(3)	$\bar{h}_4'$	The primed angular momentum of body 4
I	B2MASS	$m_2$	The mass of body 2
I	EL2(3)	$\bar{\ell}_2$	Vector position of the movable mass
I	R2DOT(3)	$\dot{\bar{r}}_2$	The time derivative of $\bar{r}_2$
I	B3MASS	$m_3$	The mass of body 3

I	R3DOT(3)	$\dot{\bar{\mathbf{r}}}_3$	The time derivative of $\bar{\mathbf{r}}_3$
I	B4MASS	$m_4$	The mass of body 4
I	R4DOT(3)	$\dot{\bar{\mathbf{r}}}_4$	The time derivative of $\bar{\mathbf{r}}_4$
I	D13(3)	$\bar{\mathbf{d}}_{13}$	Vector distance from the c.m. of body 1 to the hinge line of body 3
I	D14(3)	$\bar{\mathbf{d}}_{14}$	Vector distances from the c.m. of body 1 to the hinge line of body 4
0	H1PRIM(3)	$\bar{\mathbf{h}}'_1$	The primed angular momentum of body 1

Subroutines required: None

Equations programmed:

$$\begin{array}{c}
 \begin{array}{c} \bar{\ell}_3, \dot{\bar{\mathbf{r}}}_3 \\ \text{(body 1 coord.)} \end{array} \rightarrow \begin{array}{c} \left[ \begin{array}{c} h'_{3x} \\ h'_{2y} \\ h'_{3z} \end{array} \right] \\ = m_3 \left[ \text{GPM} \bar{\ell}_3 \right] \left[ \begin{array}{c} \dot{\bar{\mathbf{r}}}_{3x} \\ \dot{\bar{\mathbf{r}}}_{3y} \\ \dot{\bar{\mathbf{r}}}_{3z} \end{array} \right] \end{array} \rightarrow \bar{\mathbf{h}}'_3 \text{ (body 1 coords.)} \\
 \\
 \begin{array}{c} \bar{\ell}_4, \dot{\bar{\mathbf{r}}}_4 \\ \text{(body 1 coord.)} \end{array} \rightarrow \begin{array}{c} \left[ \begin{array}{c} h'_{4x} \\ h'_{4y} \\ h'_{4z} \end{array} \right] \\ = m_4 \left[ \text{GPM} \bar{\ell}_4 \right] \left[ \begin{array}{c} \dot{\bar{\mathbf{r}}}_{4x} \\ \dot{\bar{\mathbf{r}}}_{4y} \\ \dot{\bar{\mathbf{r}}}_{4z} \end{array} \right] \end{array} \rightarrow \bar{\mathbf{h}}'_4 \text{ (body 1 coords.)}
 \end{array}$$

$$\begin{bmatrix} \dot{h}'_{1x} \\ \dot{h}'_{1y} \\ \dot{h}'_{1z} \end{bmatrix} = \begin{bmatrix} h_{1x} + h'_{3x} + h'_{4x} \\ h_{1y} + h'_{3y} + h'_{4y} \\ h_{1z} + h'_{3z} + h'_{4z} \end{bmatrix} - m_2 \begin{bmatrix} \text{CPM}(-\bar{\ell}_2) \end{bmatrix} \begin{bmatrix} \dot{r}_{2x} \\ \dot{r}_{2y} \\ \dot{r}_{2z} \end{bmatrix} - m_3 \begin{bmatrix} \text{CPM}(-\bar{\ell}_3) \end{bmatrix} \begin{bmatrix} \dot{r}_{3x} \\ \dot{r}_{3y} \\ \dot{r}_{3z} \end{bmatrix} - m_4 \begin{bmatrix} \text{CPM}(-\bar{d}_{14}) \end{bmatrix} \begin{bmatrix} \dot{r}_{4x} \\ \dot{r}_{4y} \\ \dot{r}_{4z} \end{bmatrix}$$

$\uparrow \quad \bar{h}_1, \bar{h}'_3, \bar{h}'_4, \bar{\ell}_2, \bar{\ell}_3, \dot{\bar{r}}_2, \dot{\bar{r}}_3, \dot{\bar{r}}_4$   
 (body 1 coords.)

$\downarrow \quad \bar{h}'_1$  (body 1 coords.)

Discussion: None

Segment 14

Purpose: To compute the angular momentum of the composite vehicle.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	H0(3)	$\bar{h}_0$	The angular momentum of body 0
I	H1PRIM(3)	$h_1'$	The primed angular momentum of body 1
I	D01(3)	$\bar{d}_{01}$	Vector distance from the c.m. of body 0 to the hinge line of body 1
I		$A_0$	Coordinate transformation from body 1 to body 0
I	B1MASS	$m_1$	Mass of body 1
I	B2MASS	$m_2$	Mass of body 2
I	B3MASS	$m_3$	Mass of body 3
I	B4MASS	$m_4$	Mass of body 4
I	R1DOT(3)	$\dot{\bar{r}}_1$	Time derivative of $\bar{r}_1$
I	R2DOT(3)	$\dot{\bar{r}}_2$	Time derivative of $\bar{r}_2$
I	R3DOT(3)	$\dot{\bar{r}}_3$	Time derivative of $\bar{r}_3$
I	R4DOT(3)	$\dot{\bar{r}}_4$	Time derivative of $\bar{r}_4$
O	H(3)	$\bar{H}$	The angular momentum of the composite vehicle

Subroutines required: None

Equations programmed:

$$\begin{bmatrix} H_x \\ H_y \\ H_z \end{bmatrix} = \begin{bmatrix} h_{0x} \\ h_{0y} \\ h_{0z} \end{bmatrix} + \begin{bmatrix} A_0 \end{bmatrix} \begin{bmatrix} h'_{1x} \\ h'_{1y} \\ h'_{1z} \end{bmatrix} + \begin{bmatrix} \text{CPM}(\vec{d}_{01}) \end{bmatrix} \begin{bmatrix} A_0 \end{bmatrix} \begin{bmatrix} m_1 \ddot{r}_{1x} + m_2 \ddot{r}_{2x} + m_3 \ddot{r}_{3x} \\ m_1 \ddot{r}_{1y} + m_2 \ddot{r}_{2y} + m_3 \ddot{r}_{3y} \\ m_1 \ddot{r}_{1z} + m_2 \ddot{r}_{2z} + m_3 \ddot{r}_{3z} \end{bmatrix}$$

$\vec{h}_0$  (body 0 coords.)

$\vec{h}'_1, \ddot{r}_1, \ddot{r}_2, \ddot{r}_3, \ddot{r}_4$  (body 1 coords.)

$\vec{H}$  (body 0 coords.)

Discussion: None

# Segment 15

Purpose: To compute in body 1 coordinates, the unit vector  $\bar{j}$ . This is done as a matter of computational convenience and is used in setting up the angular momentum derivatives.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	EL2(3)	$\bar{l}_2$	Vector position of the movable mass
I	D13(3)	$\bar{d}_{13}$	Vector distance from the c.m. of body 1 to the hinge line of body 3
I	EL3(3)	$\bar{l}_3$	Vector position of body 3
I	D14(3)	$\bar{d}_{14}$	Vector distance from the c.m. of body 1 to the hinge line of body 4
I	EL4(3)	$\bar{l}_4$	Vector position of body 4
I	BMASS2	$m_2$	Mass of body 2
I	BMASS3	$m_3$	Mass of body 3
I	BMASS4	$m_4$	Mass of body 4
O	AJ1(3)	$\bar{j}_1$	Unit vector defined in body 1

Subroutines required: None

Equations programmed:

$$\begin{array}{l}
 \bar{l}_2, \bar{l}_3, \bar{l}_4 \rightarrow \\
 m_2, m_3, m_4 \rightarrow \\
 \bar{d}_{13}, \bar{d}_{14} \rightarrow
 \end{array}
 \begin{array}{c}
 \begin{bmatrix} j_{1x} \\ j_{1y} \\ j_{1z} \end{bmatrix} = m_2 \begin{bmatrix} l_{2x} \\ l_{2y} \\ l_{2z} \end{bmatrix} + m_3 \begin{bmatrix} d_{13x} + l_{3x} \\ d_{13y} + l_{3y} \\ d_{13z} + l_{3z} \end{bmatrix} + m_4 \begin{bmatrix} d_{14x} + l_{4x} \\ d_{14y} + l_{4y} \\ d_{14z} + l_{4z} \end{bmatrix}
 \end{array}
 \rightarrow \bar{j}_1 \text{ (body 1 coords.)}$$

Discussion: None



Segment 16

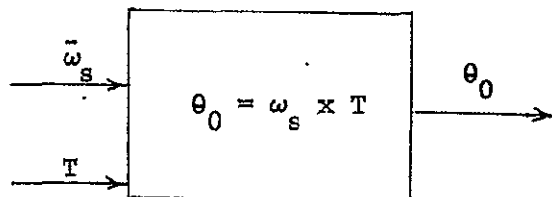
Purpose: To update the orbit angle  $\theta_0$  and to compute the external forces and moments.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	TIME	T	The time in seconds
I	Ws	$\omega_s$	The orbital rate
O	THETO	$\theta_0$	The orbital angular position
O	TQ1G(3)	$TQ_{1G}$	The gravity gradient torques
O	TQ1P(3)	$TQ_{1P}$	The propulsion torques

Subroutines required: GGRAD, PCON

Equations programmed:



Discussion: None

# Segment 17

Purpose: To sum to forces and moments acting on bodies 0 and 1.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	F01(3)	$F_{01}$	Force acting on body 0 due to gravity gradient
I	F11(3)	$F_{11}$	Force acting on body 1 due to gravity gradient
I	TQOG(3)	$TQ_{OG}$	The torque acting on body 0 due to gravity gradient
I	TQOP(3)	$TQ_{OP}$	The torque acting on body 0 due to propulsion forces
I	TQ1G(3)	$TQ_{1G}$	The torque acting on body 1 due to gravity gradient
I	TQ1P(3)	$TQ_{1P}$	The torque acting on body 1 due to propulsion forces
Ø	T0EF(3)	$T_{0eF}$	The summation of the torques acting on body 0
Ø	T1EF(3)	$T_{1eF}$	The summation of the torques acting on body 1

Subroutines required: None

Equations programmed:

Segment 18

Purpose: To calculate the time derivatives of the angular momentum of the composite vehicle.

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	WO(3)	$\bar{\omega}_0$	Angular velocity of body 0
I	H(3)	$\bar{H}$	Angular momentum of the composite body
I	TOTMAS	m	Mass of the composite body
I	BOMASS	$m_0$	Mass of body 0
I	D01(3)	$\bar{d}_{01}$	Vector distance from the c.m. of body 0 to the hinge line of body 1
I	AJ1(3)	$\bar{j}_1$	A vector, defined in body 1 coordinates used only for computational convenience
I	F0(3)	$\bar{F}_0$	Summation of the forces acting on body 0
		$A_0$	Coordinate transformation from body 1 to body 0
I	TOEF(3)	$\bar{T}_{0EF}$	Summation of the torques acting on body 0
I	T1EF(3)	$\bar{T}_{1EF}$	Summation of the torques acting on body 1
O	HDOT(3)	$\frac{dH}{dt}$	The time derivative of H

Subroutines required: None

Equations programmed:

$$\begin{aligned}
 & \begin{bmatrix} \frac{dH_x}{dt} \\ \frac{dH_y}{dt} \\ \frac{dH_z}{dt} \end{bmatrix} + \text{CPM}(\bar{\omega}_0) \begin{bmatrix} H_x \\ H_y \\ H_z \end{bmatrix} = \frac{1}{m} \text{CPM}\{(m_0 - m)\} \begin{bmatrix} \dot{d}_{01x} \\ \dot{d}_{01y} \\ \dot{d}_{01z} \end{bmatrix} - A_0 \begin{bmatrix} \bar{j}_{1x} \\ \bar{j}_{1y} \\ \bar{j}_{1z} \end{bmatrix} \begin{bmatrix} \bar{F}_{0x} \\ \bar{F}_{0y} \\ \bar{F}_{0z} \end{bmatrix} \\
 & + \frac{1}{m} A_0 \text{CPM}\{m_0\} \begin{bmatrix} A_1 \end{bmatrix} \begin{bmatrix} \dot{d}_{01x} \\ \dot{d}_{01y} \\ \dot{d}_{01z} \end{bmatrix} - \begin{bmatrix} \bar{j}_{1x} \\ \bar{j}_{1y} \\ \bar{j}_{1z} \end{bmatrix} \begin{bmatrix} \bar{F}_{1x} \\ \bar{F}_{1y} \\ \bar{F}_{1z} \end{bmatrix} + \begin{bmatrix} \bar{T}_{OEFx} \\ \bar{T}_{OEFy} \\ \bar{T}_{OEFz} \end{bmatrix} + A_0 \begin{bmatrix} \bar{T}_{1EFx} \\ \bar{T}_{1EFy} \\ \bar{T}_{1EFz} \end{bmatrix} \\
 & \begin{array}{l} \bar{\omega}_0, \bar{H}, \bar{F}_0, \bar{T}_{OEF}, \dot{\bar{d}}_{01} \text{ (body 0 coords.)} \\ \bar{j}_1, \bar{F}_1, \bar{T}_{1EF} \text{ (body 1 coords.)} \\ A_1, A_0 \end{array} \quad \begin{array}{l} \frac{d\bar{H}}{dt} \text{ (body 0 coords.)} \\ \text{INTEGRATION SUBROUTINE} \end{array}
 \end{aligned}$$

Discussion: The following vector equation is programmed in this segment:

$$\frac{d\bar{H}}{dt} + \bar{\omega}_0 \times \bar{H} = \left\{ -(m - m_0) \dot{\bar{d}}_{01} - \bar{j}_2 \right\} \times \frac{\bar{F}_0}{m} + \left\{ m_0 \dot{\bar{d}}_{01} - \bar{j}_1 \right\} \times \frac{\bar{F}_0}{m} + \bar{T}_{OEF} + \bar{T}_{1EF}$$

Segment 19

Purpose: To calculate the time derivative of  $\bar{h}_1'$  about the unconstrained axis  $\bar{x}_1$ .

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	W1(3)	$\bar{\omega}_1$	Angular velocity of body 1
I	H1PRIM(3)	$\bar{h}_1$	The primed angular momentum of body 1
I	B2MASS	$m_2$	Mass of body 2
I	EL2DOT(3)	$\dot{\bar{l}}_2$	Time derivative of $\bar{l}_2$
I	R2DOT(3)	$\dot{\bar{r}}_2$	Time derivative of $\bar{r}_2$
I	B3MASS	$m_3$	Mass of body 3
I	D13DOT(3)	$\dot{\bar{d}}_{13}$	Time derivative of $\bar{d}_{13}$
I	EL3DOT(3)	$\dot{\bar{l}}_3$	Time derivative of $\bar{l}_3$
I	R3DOT(3)	$\dot{\bar{r}}_3$	Time derivative of $\bar{r}_3$
I	B4MASS	$m_4$	Mass of body 4
I	D14DOT(3)	$\dot{\bar{d}}_{14}$	Time derivative of $\bar{d}_{14}$
I	EL4DOT(3)	$\dot{\bar{l}}_4$	Time derivative of $\bar{l}_4$
I	R4DOT(3)	$\dot{\bar{r}}_4$	Time derivative of $\bar{r}_4$
I	AJ1(3)	$\bar{j}_1$	A vector, defined in body 1 coordinates, used for computational convenience
I	T1EF(3)	$\bar{T}_{1EF}$	Summation of the torques acting on body 1
I	T01	$\bar{T}_{0 \rightarrow 1}$	The torque acting between bodies 0 and 1
O	H1PDOT(1)	$\dot{\bar{h}}_{1x}'$	Time derivative of $\bar{h}_{1x}'$

Subroutines required: TORK01

Equations programmed:

Unconstrained component along  $\bar{x}_0 = \bar{x}_1$  (axis)

$$\begin{aligned} \frac{dh'_{1x}}{dt} + \omega_{1y} h'_{1z} - \omega_{1z} h'_{1y} = & \dot{r}_{1y} (-m_2 \dot{\ell}_{2z} - m_3 (\dot{d}_{13z} + \dot{\ell}_{3z}) - m_4 (\dot{d}_{14z} + \dot{\ell}_{4z}) \\ & - \dot{r}_{1z} (-m_2 \dot{\ell}_{2y} - m_3 (\dot{d}_{13y} + \dot{\ell}_{3y}) - m_4 (\dot{d}_{14y} + \dot{\ell}_{4y}) \\ & + j_{1y} \left( \frac{F_{0y}}{m} \sin \theta_1 - \frac{F_{0z}}{m} \cos \theta_1 \right) + j_{1z} \left( \frac{F_{0y}}{m} \cos \theta_1 + \frac{F_{0z}}{m} \sin \theta_1 \right) \\ & + j_{1z} \frac{F_{1y}}{m} - j_{1y} \frac{F_{1z}}{m} + T_{1EFx} + T_{(0 \rightarrow 1)x} \end{aligned}$$

$\bar{h}'_1, \bar{\omega}_1, \dot{\bar{r}}_1, \dot{\bar{r}}_2, \dot{\bar{r}}_3, \dot{\bar{r}}_4, \dot{\bar{\ell}}_2, \dot{\bar{\ell}}_3, \dot{\bar{\ell}}_4, \bar{j}_1, \bar{F}_1, \bar{T}_{1EF}, \bar{T}_{(0 \rightarrow 1)x}$   
(body 1 coords.)

$\bar{F}_0$  (body 0 coords.)

$h'_{1x}$ -(body 1 coords.)

Discussion: None

# Segment 2()

Purpose: To calculate the time derivatives of the primed angular momenta about the unconstrained axes  $\bar{s}_3$  and  $\bar{s}_4$ .

Input/output:

I/O	Fortran Name	Math Symbol	Definition
I	H3PRIM(3)	$\bar{h}'_3$	The primed angular momentum of body 3
I	S3(3)	$\bar{s}_3$	The hinge line of body 3
I	W1(3)	$\bar{\omega}_1$	The angular velocity of body 1
I	B3MASS	$m_3$	Mass of body 3
I	EL3DOT(3)	$\dot{\bar{l}}_3$	Time derivative of $\bar{l}_3$
I	R3DOT(3)	$\dot{\bar{r}}_3$	Time derivative of $\bar{r}_3$
I	EL3(3)	$\bar{l}_3$	Vector position of body 3 from the hinge line $\bar{s}_3$
I	B4MASS	$m_3$	Mass of body 4
I	TOTMAS	$m$	Mass of composite vehicle
I	F0(3)	$\bar{F}_0$	Summation of the forces acting on body 0
I	F1(3)	$\bar{F}_1$	Summation of the forces acting on body 1
I	T13	$\bar{T}_{1 \rightarrow 3}$	Torque acting between bodies 1 and 3
Ø	G3DOT $\frac{d}{dt}$	$(\bar{h}'_3 \cdot \bar{s}_3)$	Time derivative of the unconstrained component of $\bar{h}'_3$
I	H4PRIM(3)	$\bar{h}'_4$	The primed angular momentum of body 4

I	S4(3)	$\bar{s}_4$	The hinge line of body 4
I	EL4DOT(3)	$\dot{\bar{l}}_4$	Time derivative of $\bar{l}_4$
I	R4DOT(3)	$\dot{\bar{r}}_4$	Time derivative of $\bar{r}_4$
I	EL4(3)	$\bar{l}_4$	Vector position of body 4 from the hinge line $\bar{s}_4$
I	T14	$\bar{T}_{1 \rightarrow 4}$	Torque acting between bodies 1 and 4
O	G4DOT	$\frac{d}{dt} (\bar{h}_4' \cdot \bar{s}_4)$	Time derivative of the unconstrained component of $\bar{h}_4'$

Subroutines required: TORK13, TORK14



Equations programmed:

$$\begin{aligned}
 & \frac{d}{dt} (\bar{h}'_3 \cdot \bar{s}_3) + s_{3y} (\omega_{1z} h'_{3x} - \omega_{1x} h'_{3z}) + s_{3z} (\omega_{1x} h'_{3y} - \omega_{1y} h'_{3x}) = \\
 & m_3 s_{3y} (\dot{l}_{3z} \dot{x}_{3x} - \dot{l}_{3x} \dot{x}_{3z}) + m_3 s_{3z} (\dot{l}_{3x} \dot{x}_{3y} - \dot{l}_{3y} \dot{x}_{3x}) \\
 & + \frac{m_3}{m} s_{3y} l_{3z} (F_{0x} + F_{1x}) - l_{3x} (-F_{0y} \sin \theta_1 + F_{0z} \cos \theta_1 + F_{1z}) \\
 & + \frac{m_3}{m} s_{3z} l_{3z} (F_{0y} \cos \theta_1 + F_{0z} \sin \theta_1 + F_{1y}) - l_{3y} (F_{0x} + F_{1x}) \\
 & \frac{d(\bar{h}'_4 \cdot \bar{s}_4)}{dt} + s_{4y} (\omega_{1z} h'_{4x} - \omega_{1x} h'_{4z}) + s_{4z} (\omega_{1x} h'_{4y} - \omega_{1y} h'_{4x}) \\
 & = m_4 s_{4y} (\dot{l}_{4z} \dot{x}_{4x} - \dot{l}_{4x} \dot{x}_{4z}) + m_4 s_{4y} (\dot{l}_{4x} \dot{x}_{4y} - \dot{l}_{4y} \dot{x}_{4x}) \\
 & + \frac{m_4}{m} s_{4y} l_{4z} (F_{0x} + F_{1x}) - l_{4x} (-F_{0y} \sin \theta_1 + F_{0z} \cos \theta_1 + F_{1z}) \\
 & + \frac{m_4}{m} s_{4z} l_{4x} (F_{0y} \cos \theta_1 + F_{0z} \sin \theta_1 + F_{1y}) - l_{4y} (F_{0x} + F_{1x}) + T_{1 \rightarrow 4}
 \end{aligned}$$

$\bar{\omega}_1, \bar{h}'_3, \bar{h}'_4, \bar{l}_3, \bar{l}_4, \dot{\bar{l}}_3, \dot{\bar{l}}_4$   
 $\dot{\bar{x}}_3, \dot{\bar{x}}_4, \bar{F}_1, \bar{T}_1, \bar{T}_{1 \rightarrow 4}$   
 (body 1 coords.)

$\bar{F}_0$  (body 0 coords.)

$$\frac{d}{dt} (\bar{h}'_3 \cdot \bar{s}_3) = \frac{d}{dt} (h'_{3y} s_{3y} + h'_{3z} s_{3z})$$

$$\frac{d}{dt} (\bar{h}'_4 \cdot \bar{s}_4) = \frac{d}{dt} (h'_{4y} s_{4y} + h'_{4z} s_{4z})$$

(body 1 coords.)

Discussion: None